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Conflict of interest

Editor of Journal of Biomechanics,

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The authors would like to declare no conflict of interest in the above mentioned submission of manuscript to the Journal of Biomechanics.

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November 27th, 2007.

Cover letter

Editor of Journal of Biomechanics,

REF: Submission of manuscript “Estimating complete ground reaction force with pressure insoles in walking”

The authors would like to declare that this piece of work is neither published nor submitted for consideration of publication elsewhere except as an abstract. The manuscript is submitted as a “Short Communication”. We declare that each author has been involved in the design of the study, interpretation of the data, and writing of the manuscript and that each of the authors has read and concurs with the content in the manuscript. We declare the originality of concept and execution of this paper.

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Title Page

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1 **Estimating the complete ground reaction forces with pressure insoles in walking**

2

3 **Abstract**

4 This study presented a method to estimate the complete ground reaction forces from
5 pressure insoles in walking. Five male subjects performed ten walking trials in a
6 laboratory. The complete ground reaction forces were collected during a right foot
7 stride by a force plate at 1000 Hz. Simultaneous plantar pressure data were collected
8 at 100 Hz by a pressure insole system with 99 sensors covering the whole plantar area.
9 Stepwise linear regressions were performed to individually reconstruct the complete
10 ground reaction forces in three directions from the 99 individual pressure data until
11 redundancy among the predictors occurred. An additional linear regression was
12 performed to reconstruct the vertical ground reaction force by the sum of the value of
13 the 99 pressure sensors. Five other subjects performed the same walking test for
14 validation. Estimated ground reaction forces in three directions were calculated with
15 the developed regression models, and were compared with the real data recorded from
16 force plate. Accuracy was represented by the correlation coefficient and the root mean
17 square error. Results showed very good correlation in anterior-posterior (0.928) and
18 vertical (0.989) directions, and reasonable correlation in medial-lateral direction
19 (0.719). The root mean square error was about 12%, 5% and 28% of the peak
20 recorded value. Future studies should aim to generalize the methods or to establish
21 specific methods to other subjects, patients, motions, footwear, and floor conditions.
22 The method gives an extra option to study an estimation of the complete ground
23 reaction forces in any environment without the constraints from the number and
24 location of force plates.

25

26 **Keywords:** Kinetics, plantar pressure, gait, biomechanics

27

28 **Introduction**

29 Ground reaction forces are often investigated in gait biomechanics studies (Kitaoka et
30 al., 2006). However, the measurement is often restricted by the number and the
31 location of force plates. In attempt to measure vertical and shear ground reaction
32 forces without such restriction, different devices were developed, such as a thin layer
33 of strain gauge transducer (Davis et al., 1998) or piezoelectric copolymer film (Razian
34 et al, 2003), and instrumented shoe with two sensors mounted beneath the forefoot
35 and rearfoot (Liedtke et al., 2007; Schepers et al, 2007). However, these devices were
36 limited to its specific purpose and thus were not readily available for other researchers.
37 For example, although the instrumented shoe with two external mounted sensors
38 beneath the forefoot and rearfoot (Liedtke et al., 2007; Schepers et al, 2007) could
39 measure complete shear and vertical ground reaction force, the external device lifts
40 the shoe sole and separates it from the ground by the two mounting frames. This
41 changes the original interface between shoe-sole and the ground to an interface
42 between the mounting frames and the ground, and could probably alter the friction
43 between the contact interface. Moreover, it may increase the height of the effective
44 sole and also the weight of the sole. For the shoe with an instrumented insole with
45 strain gauge transducer or piezoelectric copolymer film, the high cost of the sensor
46 resulted in the use of a limited number of sensors, and thus an inadequate coverage of
47 the whole plantar region. For example, the complete ground reaction forces could
48 only be measured in the forefoot region with 16 sensors in Davis's device (1998), and
49 at only four selected regions (heel, toe, 1st and 5th metatarsal head) in Razian's device
50 (2003).

51

52 Recently, Forner-Cordero and coworkers (2004) developed a method to calculate

53 complete ground reaction forces during gait by incorporating pressure insole data and
54 kinematics data in a validated calculation algorithm. The kinematics data provided
55 information for the transformation between the insole reference frame and the global
56 reference frame, which facilitated the subsequent calibration of the vertical ground
57 reaction force and the computation of the complete ground reaction force. Although
58 the results were excellent, the method relied on kinematics data from a motion capture
59 system and thus was still not readily applicable in outdoor environment, as it often
60 requires substantial effort in calibrating outdoor environment for kinematics
61 measurement. Moreover, the vision-based motion measurement systems often have a
62 limited measurement volume as dictated by the vision field of the cameras. Another
63 previous study suggested that the plantar pressure distribution was related to the shear
64 ground reaction force (Savelberg and de Lange, 1999). The result suggested a
65 mechanical relation between plantar pressure and shear ground reaction force, which
66 led to the current attempt to develop a method and test the feasibility to estimate the
67 complete ground reaction forces with only pressure insole data during walking in a
68 small group of subjects. As the new method is free from the restrictions of force plate
69 and motion capture system, it is suitable for rapid on-field measurement in all settings,
70 provided that the subsequent future studies to generalize the method on other subject
71 groups are successful.

72

73 **Method**

74 Calibration test

75 Five right-legged male subjects (age = 23.0 ± 3.0 yr, height = 1.72 ± 0.03 m, body
76 mass = 65.1 ± 9.7 kg, foot length = 255-260 mm) wore a pair of cloth sport shoes
77 (Fong et al., 2007) and performed ten trials of walking at their natural cadence on a
78 10-metre walking path in a gait laboratory. The university ethics committee approved

79 the study. In each trial, the subject stepped on a force plate (Advanced Mechanical
80 Technology Inc., USA) located at the middle of the walking path with their right foot.
81 The complete ground reaction forces for the right foot were sampled by the force plate
82 at 1000 Hz. A pair of pressure insoles (Novel Pedar model W, Germany) was inserted
83 in the shoes for the simultaneous measurement of plantar pressure at 100 Hz. There
84 were 99 sensors in each insole, covering the whole plantar area, and recording
85 pressure data with a resolution of 2.50 kPa.

86

87 The force plate data and the plantar pressure data for the right foot were trimmed for
88 one complete stride, from the moment of take off before the foot strike on the force
89 plate, until the next take off from the force plate. The first moment of take off before
90 the foot strike on the force plate was identified by the null plantar pressure value as
91 recorded by the pressure insoles. The second moment of take off from the force plate
92 was identified when the vertical ground reaction force as recorded by the force plate
93 drop beneath 10N. The force plate data were re-sampled to have data point in every
94 0.01s to match the sampling frequency of the pressure data. Data from all trials and all
95 subjects were pooled together for stepwise linear regression analysis to reconstruct the
96 value of the ground reaction force in three directions (anterior-posterior, F_{x_fp} ;
97 medial-lateral, F_{y_fp} ; vertical, F_{z_fp} ; unit = N) by the value of the 99 pressure
98 sensors (P1, P2, ..., P99, unit = kPa). In each stepwise regression analysis, predictors
99 were added to the regression models until the inclusion of the next predictor showed
100 redundancy or multicollinearity, as indicated by a tolerance value of less than 0.20 and
101 a variance-inflation factor value of more than 4. An additional linear regression
102 analysis was conducted to reconstruct the vertical ground reaction force by the sum of
103 the value of the 99 pressure sensors (PSum, unit = kPa).

104

105 Validation test

106 Another group of five right-legged male subjects (age = 23.8 ± 3.3 yr, height = $1.74 \pm$
107 0.03 m, body mass = 65.4 ± 7.3 kg, foot length = 255-260 mm) participated in the
108 validation test. Independent t-tests showed that the two groups of subjects did not
109 differ in age, height and body mass. The subjects performed the walking test with the
110 same procedure with the calibration test. Beside the complete ground reaction forces
111 recorded by the force plate, the estimated ground reaction forces were also calculated
112 by inputting the pressure value of the selected sensor locations to the regression
113 models developed in the calibration test. Correlation coefficient (R) and the root mean
114 square error (RMS error) were computed between the data measured with force plates
115 and estimated from the regression models, for the comparison of accuracy with Forner
116 Cordero's method (2004).

117

118 **Results**

119 Table 1 shows the results of regression analysis, which included the equations to
120 estimate the value of the complete ground reaction forces recorded from the force
121 plate, and the amount of explained variance (Adjusted R^2) of the regression models.
122 Figure 1 shows the locations of the sensors included in each regression model
123 employing individual pressure sensor value as predictors. Four, six and four sensors
124 among the total 99 sensors were required for the estimation of the ground reaction
125 force for anterior-posterior, medial-lateral and vertical directions respectively, as
126 shown in Figure 1. The sum of the value of the 99 pressure sensors (PSum) was also
127 found to be relevant in reconstructing the vertical ground reaction force.

128

129 The accuracy of the estimation was also shown in Table 1, as indicated by the
130 correlation and the RMS error between the real and estimated data. Corresponding

131 results from Forner Cordero's study (2004) are also included for comparison. Figure 2
132 shows the pattern and the absolute error of the real and estimated data of a complete
133 stride trial with an average accuracy among the 50 trials in the validation test. The
134 accuracy of the results was very good in the estimation of ground reaction force in
135 anterior-posterior and vertical directions, as indicated by a very high correlation
136 between the real and estimated data (0.928 and 0.989). The RMS error was 27.41N
137 and 45.79N respectively, which was only about 12% and 5% of their peak values. The
138 estimation in medial-lateral direction was fair, with a correlation value of 0.719
139 between the real and estimated data. The RMS error was 11.71N, which was as much
140 as 28% of the peak value. In general, the pattern and accuracy of the results of this
141 study were similar but slightly inferior to that from Forner Cordero's study (2004), as
142 indicated by lower correlations, greater RMS errors and same deficiency in estimating
143 the ground reaction force in medial-lateral direction.

144

145 The pattern of the estimated data was similar to that of real data, as shown in a
146 selected trial with average accuracy in Figure 2. The solid line shows the pattern of
147 the real ground reaction force data as measured by the force plate (F_{x_fp} , F_{y_fp} ,
148 F_{z_fp}), and the dotted line showed the estimated data calculated from the regression
149 models shown in Table 1 (F_{x_est} , F_{y_est} , F_{z_est} , $F_{z_est_sum}$). At the time right after
150 the foot strike, the estimation of the peaks was found to be very accurate. The
151 estimated values were about 95%-105% of the real data in all three directions.
152 However, the plots of absolute error suggested that the largest error occur right after
153 foot strike and just before take off – this implied that the estimation was even more
154 accurate during the mid-stance period. However, at the period just before take off,
155 relatively larger errors were found in both anterior-posterior and medial-lateral
156 components.

157

158 **Discussion**

159 In the estimation of the vertical force, four critical sensor locations (P1, P18, P71, P74)
160 or the sum of the value of the 99 pressure sensors could both work well with
161 comparable accuracy. The four locations spread around the plantar region, with two at
162 the metatarsal region and two at the rearfoot region. In the estimation of
163 anterior-posterior shear force, the mechanical relation between plantar pressure and
164 shear ground reaction force was somewhat reflected by the position of the essential
165 pressure sensors for the estimation. The locations P13 and P60 contributed negatively
166 to the estimated value – when they were on, especially during the heel strike period
167 and the weight acceptance period by midfoot, the ground reaction force was in a
168 rather backward direction. The locations P90 and P97 around the hallux region
169 contributed positively. They were on, especially at the propulsion and take off period,
170 when the hallux was almost the only contact region of the foot and the ground. The
171 corresponding ground reaction force was in the anterior direction for propulsion. This
172 also reflected the characteristics of heel-toe walking which lead to this unique
173 mechanical relation between plantar pressure and shear ground reaction force in
174 anterior-posterior direction.

175

176 This study presented a feasible method to estimate complete ground reaction forces
177 with pressure insole data during walking, however, the current findings are limited to
178 a small homogenous group of male young subjects only. Future studies should aim to
179 generalize the methods, or to establish specific methods to other subjects, patients,
180 motions, footwear, and floor conditions, etc. Although the method presented in the
181 current study is slightly inferior to that presented by Forner Cordero and coworkers
182 (2004), it does not require a motion capture system for the calculation of complete

183 ground reaction force. Therefore, if the level of accuracy is adequate, or if the inferior
184 accuracy could be tolerated, the current method is readily available for measurement
185 in any environment out of the laboratory. Considering the good and reasonable
186 accuracy and the possible rapid application in any environment, the method presented
187 in this study should give an extra option to study complete ground reaction forces
188 with less constraint from the number and location of force plates. Before the future
189 studies to generalize the methods to other conditions, we suggest performing
190 calibration and measurement on the same group of subject with the same type of
191 shoes. The method presented could be implemented to the original pressure insole
192 system for immediately estimation of the complete ground reaction forces during data
193 collection, and could be useful for real-time analysis for sport biomechanics tests
194 which requires immediate display of data and reports.

195

196 **Conclusion**

197 This study presented a feasible method to estimate complete ground reaction forces
198 with pressure insole data during walking, which eliminates the constraint introduced
199 by number and location of force plates in biomechanics studies. The results were with
200 very good in estimating anterior-posterior and vertical ground reaction force, and with
201 reasonable accuracy in estimating that in medial-lateral direction. The method can
202 serve as an extra option in measuring complete ground reaction forces in any
203 environment out of the laboratory without using force plates.

204

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209

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235

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From: "Journal of Biomechanics" JBM@elsevier.com

Subject: BM-D-07-00858R2 - Editor Decision

Ref.: Ms. No. BM-D-07-00858R2

Estimating complete ground reaction force with pressure insoles in walking

Journal of Biomechanics

Dear Professor Chan,

Thank you for your submission to the Journal of Biomechanics. After considering the enclosed reviews from our referees, I regret to inform you that our referee panel recommends against publication of your manuscript in its current form, although a revised manuscript may be resubmitted and considered after further review.

If you choose to submit a revised manuscript, please provide a list of points of how you have responded to the reviewers' suggestions.

To submit a revision, go to <http://ees.elsevier.com/bm/> and log in as an Author. You will see a menu item called Submission Needing Revision. You will find your submission record there. Please update accordingly and submit your revised manuscript.

We look forward to receiving your revised manuscript.

Yours sincerely,

Dr Rik Huiskes

Editor in Chief

Journal of Biomechanics

Reviewers' comments:

Reviewer #1: The authors have addressed satisfactorily the proposed questions. The manuscript has improved significantly. However, there are still a some minor errors, mostly grammar errors or ambiguous sentences that must be corrected. Please, revise the text for grammatical correctness.

It is used through the text "complete ground reaction force", although in general it is usual to name them as "the complete ground reaction forces".

>>> Revised accordingly.

Line 32: please correct "...including a thin layer..." or even better, "...consisting of a thin layer..."

>>> The paragraph lists some different devices, so it read "including a thin layer of strain gauge transducer (Davis et al., 1998) or piezoelectric copolymer film (Razian et al, 2003), and instrumented shoe with two sensors mounted beneath the forefoot and rearfoot (Liedtke et al., 2007; Schepers et al, 2007)". The term "including" is revised to be "such as" in the revised manuscript.

Line 80: This description is somewhat ambiguous. Were the authors using two force plates? Otherwise, they only measured the complete ground reaction forces during single stance. Please, clarify this point. If the forces measured are not complete (in 3-D but also under both feet) then correct the text.

>>> Only one force plate is used, and the complete ground reaction forces in 3D for only the right foot was recorded and analyzed. The left foot did not step on the same force plate. The sentence is revised as "The complete ground reaction forces for the right foot were sampled by the force plate at 1000 Hz" (Line 81).

In line 86 it is said that the data are trimmed for one complete stride. Is this correct? A stride is defined between two consecutive ground contacts with the same foot. This would imply the need of up to three force plates to record a complete stride. From the explanations provided in the text it seems that the authors only measured the complete forces under one foot. Please, let clear in the text which forces you are referring to.

>>> The first moment of take off before the foot strike on the force plate was identified by the null plantar pressure value as recorded by the pressure insoles. The second moment of take off from the force plate was identified when the vertical ground reaction force as recorded by the force plate drop beneath 10N. This information is added in the revised manuscript (Line 89-93).

Line 172 and line 193 it is said that "This study presented a good feasibility to estimate..." Please, explain better, a good feasibility method to estimate?

>>> Revised accordingly to "a feasible method to estimate...".

Reviewer #2: My comments have been processed adequately

Abstract

This study presented a method to estimate complete ground reaction force from pressure insoles in walking. Five male subjects performed ten walking trials in a laboratory. Complete ground reaction force was collected during a right foot stride by a force plate at 1000 Hz. Simultaneous plantar pressure data were collected at 100 Hz by a pressure insole system with 99 sensors covering the whole plantar area. Stepwise linear regressions were performed to individually reconstruct the complete ground reaction force in three directions from the 99 individual pressure data until redundancy among the predictors occurred. An additional linear regression was performed to reconstruct the vertical ground reaction force by the sum of the value of the 99 pressure sensors. Five other subjects performed the same walking test for validation. Estimated ground reaction forces in three directions were calculated with the developed regression models, and were compared with the real data recorded from force plate. Accuracy was represented by the correlation coefficient and the root mean square error. Results showed very good correlation in anterior-posterior (0.928) and vertical (0.989) directions, and reasonable correlation in medial-lateral direction (0.719). The root mean square error was about 12%, 5% and 28% of the peak recorded value. Future studies should aim to generalize the methods or to establish specific methods to other subjects, patients, motions, footwear, and floor conditions. The method gives an extra option to study complete ground reaction forces in any environment without the constraints from the number and location of force plates.

Figure legends

Figure 1 – Location of the sensors (in right foot) required in the three regression models (in grey).

Figure 2 – Pattern and the absolute error of real and estimated complete ground reaction force data in a selected trial of a complete stride, from the previous take off (time = -0.31s), foot strike (time = 0.00s) to the next take off (time = 0.53s), as shown by the dotted lines.

Figure 1
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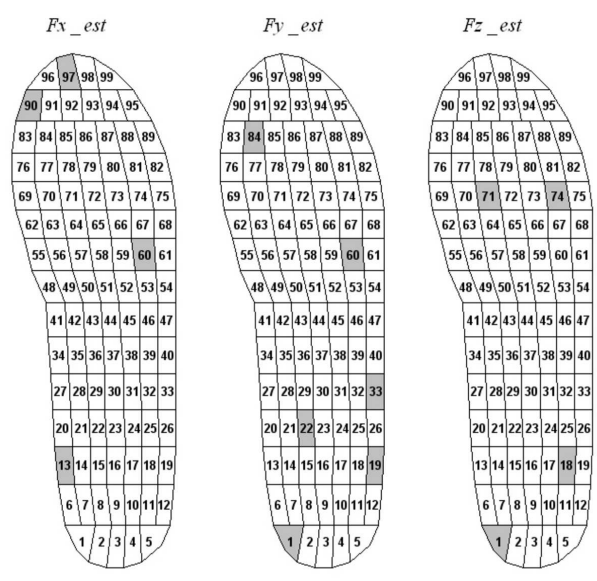


Figure 2

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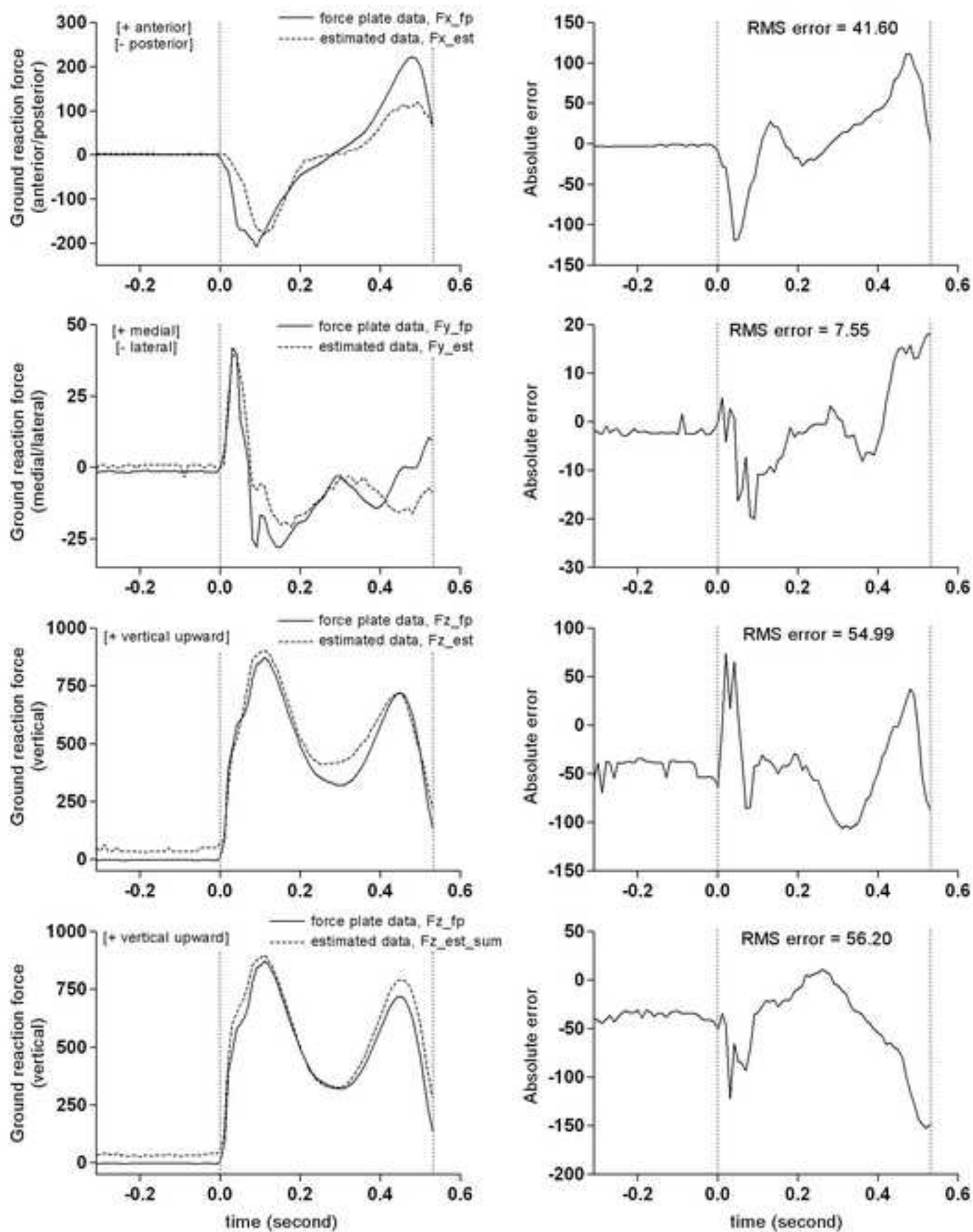


Table 1

Table 1 – Results of regression analysis and the comparison of accuracy with Forner Cordero’s study.

Force direction	Regression models	Adjusted	Accuracy		Forner Cordero’s study	
		R ²	R	RMS Error (N)	R	RMS Error (N)
Anterior-posterior (Fx_fp)	$Fx_est(N) = 1.364 - 32.045 \times (P13) + 4.452 \times (P90) + 4.847 \times (P97) - 2.796 \times P60$	0.904	0.928	27.41	0.977-0.979	7.53-9.15
Medial-lateral (Fy_fp)	$Fy_est(N) = 2.622 - 3.158 \times (P60) - 8.734 \times (P33) - 1.508 \times (P84) - 1.654 \times (P22) + 2.261 \times (P1) - 2.310 \times P19$	0.764	0.719	11.71	0.778-0.818	7.30-7.51
Vertical (Fz_fp)	$Fz_est(N) = -18.938 + 8.001 \times (P74) + 31.446 \times (P18) + 30.836 \times (P71) + 15.150 \times (P1)$	0.975	0.989	45.79	0.995-0.997	27.84-30.13
	$Fz_est_sum(N) = -31.132 + 1.696 \times (PSum)$	0.985	0.992	38.43	0.995-0.997	27.84-30.13

(* Unit: force in N, pressure in kPa. PX is the value of pressure of the sensor number X. PSum is the value of the sum of the pressure values of the 99 sensors.)