



Pilkington Library

Author/Filing Title GORYWODA

Vol. No. Class Mark T

**Please note that fines are charged on ALL
overdue items.**

FOR REFERENCE ONLY

0402509846



 Loughborough University Public Library
Date May 02
Class
Acc No. 040250984

APPENDIX 1. Input Data for Prosthesis F076

F076 : designation of the prosthesis

- 5
- 14
- 18
- 23 : number of the basis-scan
- 11 : last 8 mm step
- 28 : total number of steps
- 73 : number of points per step
- 129 : neck angle in degrees
- 1
- 7
- 110

No.	X	Y	Z	No.	X	Y	Z
✓ 1	3.31	0.00	8.00	2	3.32	.29	8.00
3	3.34	.59	8.00	4	3.27	.88	8.00
5	3.30	1.20	8.00	6	3.36	1.57	8.00
7	3.35	1.93	8.00	8	3.27	2.29	8.00
9	3.13	2.63	8.00	10	2.97	2.97	8.00
11	2.76	3.29	8.00	12	2.52	3.60	8.00
13	2.30	3.98	8.00	14	2.04	4.37	8.00
15	1.71	4.69	8.00	16	1.37	5.13	8.00
17	.97	5.50	8.00	18	.49	5.56	8.00
✓ 19	0.00	5.72	8.00	20	-.49	5.64	8.00
x 21	-.97	5.50	8.00	22	-1.43	5.34	8.00
23	-1.88	5.17	8.00	24	-2.22	4.77	8.00
25	-2.51	4.34	8.00	26	-2.72	3.89	8.00
27	-2.91	3.47	8.00	28	-3.13	3.13	8.00
29	-3.35	2.81	8.00	30	-3.51	2.46	8.00
31	-3.58	2.07	8.00	32	-3.78	1.76	8.00
33	-3.81	1.39	8.00	34	-3.93	1.05	8.00
35	-4.08	.72	8.00	36	-4.07	.36	8.00
✓ 37	-4.16	0.00	8.00	38	-4.28	-.37	8.00
x 39	-4.36	-.77	8.00	40	-4.48	-1.20	8.00
41	-4.42	-1.61	8.00	42	-4.41	-2.06	8.00
43	-4.34	-2.51	8.00	44	-4.22	-2.95	8.00
45	-4.05	-3.39	8.00	46	-3.91	-3.91	8.00
47	-3.72	-4.44	8.00	48	-3.50	-5.01	8.00
49	-3.17	-5.48	8.00	50	-2.79	-5.99	8.00
51	-2.34	-6.44	8.00	52	-1.81	-6.75	8.00
53	-1.24	-7.04	8.00	54	-.61	-7.02	8.00
✓ 55	-0.00	-6.86	8.00	56	.58	-6.67	8.00
λ 57	1.10	-6.23	8.00	58	1.56	-5.81	8.00
59	1.95	-5.35	8.00	60	2.31	-4.94	8.00
61	2.52	-4.36	8.00	62	2.72	-3.89	8.00
63	2.98	-3.55	8.00	64	3.20	-3.20	8.00
65	3.32	-2.78	8.00	66	3.48	-2.44	8.00
67	3.50	-2.02	8.00	68	3.56	-1.66	8.00
69	3.48	-1.27	8.00	70	3.50	-.94	8.00
71	3.45	-.61	8.00	✓ 72	3.38	-.30	8.00
✓ 73	3.31	-0.00	8.00				
✓ 1	3.84	0.00	16.00	2	3.80	.33	16.00
3	3.83	.67	16.00	4	3.77	1.01	16.00
5	3.69	1.34	16.00	6	3.59	1.68	16.00
7	3.55	2.05	16.00	8	3.56	2.50	16.00
9	3.48	2.92	16.00	10	3.27	3.27	16.00

11	3.12	3.72	16.00	12	2.98	4.26	16.00
13	2.73	4.74	16.00	14	2.35	5.05	16.00
15	1.94	5.33	16.00	16	1.51	5.62	16.00
17	1.04	5.88	16.00	18	.52	5.90	16.00
19	0.00	5.86	16.00	20	-.49	5.65	16.00
21	-.97	5.50	16.00	22	-1.43	5.34	16.00
23	-1.88	5.15	16.00	24	-2.31	4.96	16.00
25	-2.67	4.63	16.00	26	-2.96	4.22	16.00
27	-3.22	3.83	16.00	28	-3.46	3.46	16.00
29	-3.71	3.11	16.00	30	-3.78	2.64	16.00
31	-3.97	2.29	16.00	32	-4.11	1.92	16.00
33	-4.22	1.53	16.00	34	-4.37	1.17	16.00
35	-4.36	.77	16.00	36	-4.46	.39	16.00
37	-4.51	0.00	16.00	38	-4.60	-.40	16.00
39	-4.60	-.81	16.00	40	-4.51	-1.21	16.00
41	-4.42	-1.61	16.00	42	-4.41	-2.06	16.00
43	-4.34	-2.51	16.00	44	-4.22	-2.95	16.00
45	-4.05	-3.39	16.00	46	-3.91	-3.91	16.00
47	-3.72	-4.44	16.00	48	-3.51	-5.01	16.00
49	-3.17	-5.48	16.00	50	-2.79	-5.99	16.00
51	-2.34	-6.44	16.00	52	-1.81	-6.75	16.00
53	-1.24	-7.04	16.00	54	-.61	-7.02	16.00
55	-0.00	-6.86	16.00	56	.58	-6.67	16.00
57	1.10	-6.23	16.00	58	1.56	-5.81	16.00
59	1.95	-5.35	16.00	60	2.30	-4.94	16.00
61	2.52	-4.36	16.00	62	2.72	-3.89	16.00
63	2.98	-3.55	16.00	64	3.21	-3.21	16.00
65	3.41	-2.86	16.00	66	3.60	-2.52	16.00
67	3.71	-2.14	16.00	68	3.68	-1.72	16.00
69	3.75	-1.37	16.00	70	3.77	-1.01	16.00
71	3.83	-.68	16.00	72	3.90	-.34	16.00
73	3.84	-0.00	16.00				
1	4.42	0.00	24.00	2	4.50	.39	24.00
3	4.52	.80	24.00	4	4.48	1.20	24.00
5	4.40	1.60	24.00	6	4.40	2.05	24.00
7	4.33	2.50	24.00	8	4.18	2.93	24.00
9	4.11	3.45	24.00	10	3.82	3.82	24.00
11	3.54	4.22	24.00	12	3.24	4.62	24.00
13	2.94	5.09	24.00	14	2.53	5.42	24.00
15	2.02	5.55	24.00	16	1.54	5.73	24.00
17	1.04	5.92	24.00	18	.52	5.91	24.00
19	0.00	5.84	24.00	20	-.52	5.92	24.00
21	-1.05	5.97	24.00	22	-1.56	5.84	24.00
23	-1.97	5.42	24.00	24	-2.36	5.06	24.00
25	-2.74	4.74	24.00	26	-3.12	4.46	24.00
27	-3.43	4.08	24.00	28	-3.70	3.70	24.00
29	-3.81	3.20	24.00	30	-4.01	2.81	24.00
31	-4.10	2.37	24.00	32	-4.12	1.92	24.00
33	-4.21	1.53	24.00	34	-4.37	1.17	24.00
35	-4.36	.77	24.00	36	-4.46	.39	24.00
37	-4.51	0.00	24.00	38	-4.60	-.40	24.00
39	-4.60	-.81	24.00	40	-4.51	-1.21	24.00
41	-4.42	-1.61	24.00	42	-4.41	-2.06	24.00
43	-4.34	-2.51	24.00	44	-4.22	-2.95	24.00
45	-4.05	-3.39	24.00	46	-3.91	-3.91	24.00
47	-3.72	-4.44	24.00	48	-3.51	-5.01	24.00
49	-3.17	-5.48	24.00	50	-2.79	-5.99	24.00
51	-2.34	-6.44	24.00	52	-1.81	-6.75	24.00
53	-1.24	-7.04	24.00	54	-.61	-7.01	24.00
55	-0.00	-6.93	24.00	56	.58	-6.68	24.00
57	1.10	-6.23	24.00	58	1.56	-5.81	24.00

59	1.96	-5.38	24.00
61	2.52	-4.36	24.00
63	3.01	-3.59	24.00
65	3.41	-2.86	24.00
67	3.74	-2.16	24.00
69	3.95	-1.44	24.00
71	4.17	-.74	24.00
73	4.42	-0.00	24.00

60	2.31	-4.95	24.00
62	2.72	-3.88	24.00
64	3.23	-3.23	24.00
66	3.63	-2.54	24.00
68	3.86	-1.80	24.00
70	4.07	-1.09	24.00
72	4.24	-.37	24.00

1	4.49	0.00	32.00
3	4.87	.86	32.00
5	5.02	1.83	32.00
7	4.81	2.78	32.00
9	4.55	3.82	32.00
11	4.08	4.86	32.00
13	3.31	5.73	32.00
15	2.33	6.41	32.00
17	1.19	6.75	32.00
19	0.00	6.77	32.00
21	-1.16	6.59	32.00
23	-2.22	6.11	32.00
25	-3.01	5.21	32.00
27	-3.61	4.30	32.00
29	-3.99	3.35	32.00
31	-4.13	2.38	32.00
33	-4.22	1.54	32.00
35	-4.40	.78	32.00
37	-4.55	0.00	32.00
39	-4.61	-.81	32.00
41	-4.42	-1.61	32.00
43	-4.34	-2.51	32.00
45	-4.05	-3.39	32.00
47	-3.72	-4.44	32.00
49	-3.17	-5.48	32.00
51	-2.34	-6.44	32.00
53	-1.24	-7.04	32.00
55	-0.00	-6.94	32.00
57	1.14	-6.44	32.00
59	1.99	-5.46	32.00
61	2.61	-4.52	32.00
63	3.13	-3.74	32.00
65	3.46	-2.90	32.00
67	3.75	-2.16	32.00
69	4.07	-1.48	32.00
71	4.39	-.77	32.00
73	4.49	-0.00	32.00

2	4.69	.41	32.00
4	4.98	1.33	32.00
6	4.92	2.29	32.00
8	4.69	3.28	32.00
10	4.30	4.30	32.00
12	3.76	5.37	32.00
14	2.83	6.06	32.00
16	1.77	6.61	32.00
18	.60	6.84	32.00
20	-.58	6.68	32.00
22	-1.73	6.44	32.00
24	-2.66	5.70	32.00
26	-3.32	4.74	32.00
28	-3.88	3.88	32.00
30	-4.05	2.84	32.00
32	-4.18	1.95	32.00
34	-4.43	1.19	32.00
36	-4.46	.39	32.00
38	-4.66	-.41	32.00
40	-4.51	-1.21	32.00
42	-4.41	-2.06	32.00
44	-4.22	-2.95	32.00
46	-3.91	-3.91	32.00
48	-3.51	-5.01	32.00
50	-2.79	-5.99	32.00
52	-1.81	-6.75	32.00
54	-.61	-7.01	32.00
56	.58	-6.66	32.00
58	1.61	-6.00	32.00
60	2.32	-4.97	32.00
62	2.89	-4.12	32.00
64	3.38	-3.38	32.00
66	3.65	-2.55	32.00
68	3.87	-1.80	32.00
70	4.17	-1.12	32.00
72	4.40	-.39	32.00

1	5.13	0.00	40.00
3	5.11	.90	40.00
5	5.05	1.84	40.00
7	5.11	2.95	40.00
9	4.86	4.07	40.00
11	4.24	5.05	40.00
13	3.31	5.73	40.00
15	2.33	6.41	40.00
17	1.19	6.75	40.00
19	0.00	6.77	40.00
21	-1.16	6.59	40.00
23	-2.22	6.11	40.00
25	-3.01	5.21	40.00
27	-3.61	4.30	40.00
29	-3.99	3.35	40.00

2	5.17	.45	40.00
4	5.11	1.37	40.00
6	5.14	2.40	40.00
8	4.99	3.49	40.00
10	4.58	4.58	40.00
12	3.79	5.41	40.00
14	2.83	6.06	40.00
16	1.77	6.61	40.00
18	.60	6.84	40.00
20	-.58	6.68	40.00
22	-1.73	6.44	40.00
24	-2.66	5.70	40.00
26	-3.32	4.74	40.00
28	-3.88	3.88	40.00
30	-4.05	2.84	40.00

31	-4.12	2.38	40.00
33	-4.41	1.61	40.00
35	-4.39	.77	40.00
37	-4.55	0.00	40.00
39	-4.61	-.81	40.00
41	-4.42	-1.61	40.00
43	-4.34	-2.51	40.00
45	-4.05	-3.39	40.00
47	-3.72	-4.44	40.00
49	-3.17	-5.49	40.00
51	-2.38	-6.53	40.00
53	-1.25	-7.09	40.00
55	-0.00	-7.04	40.00
57	1.13	-6.43	40.00
59	2.04	-5.61	40.00
61	2.83	-4.90	40.00
63	3.57	-4.25	40.00
65	3.93	-3.30	40.00
67	4.44	-2.57	40.00
69	4.73	-1.72	40.00
71	5.02	-.88	40.00
73	5.13	-0.00	40.00

32	-4.29	2.00	40.00
34	-4.46	1.19	40.00
36	-4.46	.39	40.00
38	-4.66	-.41	40.00
40	-4.51	-1.21	40.00
42	-4.41	-2.06	40.00
44	-4.22	-2.95	40.00
46	-3.91	-3.91	40.00
48	-3.51	-5.01	40.00
50	-2.79	-5.98	40.00
52	-1.83	-6.84	40.00
54	-.62	-7.14	40.00
56	.58	-6.68	40.00
58	1.64	-6.13	40.00
60	2.50	-5.37	40.00
62	3.17	-4.53	40.00
64	3.71	-3.71	40.00
66	4.19	-2.93	40.00
68	4.52	-2.11	40.00
70	4.90	-1.31	40.00
72	5.08	-.44	40.00

1	5.36	0.00	48.00
3	5.60	.99	48.00
5	5.49	2.00	48.00
7	5.32	3.07	48.00
9	4.99	4.18	48.00
11	4.28	5.10	48.00
13	3.44	5.95	48.00
15	2.36	6.48	48.00
17	1.19	6.75	48.00
19	0.00	6.77	48.00
21	-1.16	6.59	48.00
23	-2.22	6.11	48.00
25	-3.01	5.21	48.00
27	-3.61	4.30	48.00
29	-3.99	3.35	48.00
31	-4.12	2.38	48.00
33	-4.41	1.61	48.00
35	-4.39	.77	48.00
37	-4.55	0.00	48.00
39	-4.61	-.81	48.00
41	-4.42	-1.61	48.00
43	-4.34	-2.51	48.00
45	-4.05	-3.39	48.00
47	-3.72	-4.44	48.00
49	-3.17	-5.49	48.00
51	-2.38	-6.53	48.00
53	-1.25	-7.09	48.00
55	-0.00	-7.04	48.00
57	1.14	-6.45	48.00
59	2.06	-5.65	48.00
61	2.87	-4.97	48.00
63	3.57	-4.26	48.00
65	4.14	-3.48	48.00
67	4.45	-2.57	48.00
69	4.72	-1.72	48.00
71	5.13	-.90	48.00
73	5.36	-0.00	48.00

2	5.59	.49	48.00
4	5.47	1.47	48.00
6	5.39	2.51	48.00
8	5.30	3.71	48.00
10	4.63	4.63	48.00
12	3.90	5.56	48.00
14	2.90	6.23	48.00
16	1.77	6.61	48.00
18	.60	6.84	48.00
20	-.58	6.68	48.00
22	-1.73	6.44	48.00
24	-2.66	5.70	48.00
26	-3.32	4.74	48.00
28	-3.88	3.88	48.00
30	-4.05	2.84	48.00
32	-4.29	2.00	48.00
34	-4.46	1.19	48.00
36	-4.46	.39	48.00
38	-4.66	-.41	48.00
40	-4.51	-1.21	48.00
42	-4.41	-2.06	48.00
44	-4.22	-2.95	48.00
46	-3.91	-3.91	48.00
48	-3.51	-5.01	48.00
50	-2.79	-5.98	48.00
52	-1.83	-6.84	48.00
54	-.62	-7.14	48.00
56	.58	-6.67	48.00
58	1.64	-6.13	48.00
60	2.52	-5.41	48.00
62	3.18	-4.54	48.00
64	3.88	-3.88	48.00
66	4.27	-2.99	48.00
68	4.52	-2.11	48.00
70	4.98	-1.33	48.00
72	5.33	-.47	48.00

1	5.73	0.00	56.00
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2	5.79	.51	56.00
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3	5.76	1.02	56.00	4	5.88	1.58	56.00
5	5.89	2.14	56.00	6	5.77	2.69	56.00
7	5.78	3.34	56.00	8	5.65	3.96	56.00
9	5.53	4.64	56.00	10	5.17	5.17	56.00
11	4.75	5.66	56.00	12	4.22	6.03	56.00
13	3.67	6.35	56.00	14	3.06	6.56	56.00
15	2.51	6.89	56.00	16	1.86	6.94	56.00
17	1.27	7.17	56.00	18	.63	7.23	56.00
19	0.00	7.20	56.00	20	-.63	7.17	56.00
21	-1.22	6.91	56.00	22	-1.75	6.54	56.00
23	-2.23	6.12	56.00	24	-2.66	5.70	56.00
25	-3.01	5.21	56.00	26	-3.32	4.74	56.00
27	-3.61	4.30	56.00	28	-3.88	3.88	56.00
29	-3.99	3.35	56.00	30	-4.05	2.84	56.00
31	-4.12	2.38	56.00	32	-4.29	2.00	56.00
33	-4.41	1.61	56.00	34	-4.46	1.19	56.00
35	-4.39	.77	56.00	36	-4.46	.39	56.00
37	-4.55	0.00	56.00	38	-4.66	-.41	56.00
39	-4.61	-.81	56.00	40	-4.51	-1.21	56.00
41	-4.42	-1.61	56.00	42	-4.41	-2.06	56.00
43	-4.34	-2.51	56.00	44	-4.22	-2.95	56.00
45	-4.05	-3.39	56.00	46	-3.91	-3.91	56.00
47	-3.72	-4.44	56.00	48	-3.51	-5.01	56.00
49	-3.17	-5.49	56.00	50	-2.79	-5.98	56.00
51	-2.38	-6.53	56.00	52	-1.83	-6.84	56.00
53	-1.25	-7.09	56.00	54	-.62	-7.14	56.00
55	-0.00	-7.03	56.00	56	.59	-6.69	56.00
57	1.15	-6.50	56.00	58	1.69	-6.30	56.00
59	2.13	-5.85	56.00	60	2.61	-5.59	56.00
61	3.02	-5.23	56.00	62	3.41	-4.87	56.00
63	3.74	-4.45	56.00	64	4.03	-4.03	56.00
65	4.31	-3.61	56.00	66	4.61	-3.23	56.00
67	4.67	-2.70	56.00	68	4.93	-2.30	56.00
69	5.09	-1.85	56.00	70	5.24	-1.40	56.00
71	5.39	-.95	56.00	72	5.59	-.49	56.00
73	5.73	-0.00	56.00				

1	6.60	0.00	64.00	2	6.75	.59	64.00
3	6.95	1.23	64.00	4	6.84	1.83	64.00
5	6.71	2.44	64.00	6	6.65	3.10	64.00
7	6.46	3.73	64.00	8	6.24	4.37	64.00
9	5.79	4.86	64.00	10	5.30	5.30	64.00
11	4.77	5.68	64.00	12	4.22	6.03	64.00
13	3.67	6.36	64.00	14	3.06	6.56	64.00
15	2.51	6.89	64.00	16	1.86	6.94	64.00
17	1.27	7.17	64.00	18	.63	7.23	64.00
19	0.00	7.20	64.00	20	-.63	7.17	64.00
21	-1.22	6.91	64.00	22	-1.75	6.54	64.00
23	-2.23	6.12	64.00	24	-2.66	5.70	64.00
25	-3.01	5.21	64.00	26	-3.32	4.74	64.00
27	-3.61	4.30	64.00	28	-3.88	3.88	64.00
29	-4.05	3.40	64.00	30	-4.06	2.84	64.00
31	-4.12	2.38	64.00	32	-4.28	2.00	64.00
33	-4.44	1.62	64.00	34	-4.58	1.23	64.00
35	-4.63	.82	64.00	36	-4.70	.41	64.00
37	-4.68	0.00	64.00	38	-4.67	-.41	64.00
39	-4.61	-.81	64.00	40	-4.51	-1.21	64.00
41	-4.42	-1.61	64.00	42	-4.41	-2.06	64.00
43	-4.34	-2.51	64.00	44	-4.22	-2.95	64.00
45	-4.05	-3.39	64.00	46	-3.91	-3.91	64.00
47	-3.72	-4.44	64.00	48	-3.51	-5.01	64.00
49	-3.17	-5.48	64.00	50	-2.79	-5.98	64.00

51	-2.37	-6.52	64.00	52	-1.89	-7.07	64.00
53	-1.29	-7.34	64.00	54	-.66	-7.49	64.00
55	-0.00	-7.30	64.00	56	.63	-7.15	64.00
57	1.24	-7.03	64.00	58	1.79	-6.69	64.00
59	2.30	-6.32	64.00	60	2.82	-6.04	64.00
61	3.28	-5.67	64.00	62	3.73	-5.33	64.00
63	4.22	-5.03	64.00	64	4.58	-4.58	64.00
65	4.89	-4.10	64.00	66	5.20	-3.64	64.00
67	5.51	-3.18	64.00	68	5.83	-2.72	64.00
69	6.21	-2.26	64.00	70	6.29	-1.68	64.00
71	6.38	-1.13	64.00	72	6.49	-.57	64.00
73	6.60	-0.00	64.00				

1	7.29	0.00	72.00	2	7.15	.63	72.00
3	7.20	1.27	72.00	4	7.30	1.96	72.00
5	7.21	2.62	72.00	6	7.07	3.30	72.00
7	6.78	3.91	72.00	8	6.28	4.40	72.00
9	5.85	4.91	72.00	10	5.31	5.31	72.00
11	4.77	5.68	72.00	12	4.22	6.03	72.00
13	3.67	6.36	72.00	14	3.06	6.56	72.00
15	2.51	6.89	72.00	16	1.86	6.94	72.00
17	1.27	7.17	72.00	18	.63	7.23	72.00
19	0.00	7.21	72.00	20	-.63	7.16	72.00
21	-1.25	7.08	72.00	22	-1.80	6.73	72.00
23	-2.32	6.38	72.00	24	-2.73	5.85	72.00
25	-3.19	5.52	72.00	26	-3.55	5.07	72.00
27	-3.71	4.42	72.00	28	-3.98	3.98	72.00
29	-4.15	3.48	72.00	30	-4.29	3.00	72.00
31	-4.45	2.57	72.00	32	-4.49	2.09	72.00
33	-4.58	1.67	72.00	34	-4.60	1.23	72.00
35	-4.62	.82	72.00	36	-4.70	.41	72.00
37	-4.68	0.00	72.00	38	-4.67	-.41	72.00
39	-4.61	-.81	72.00	40	-4.51	-1.21	72.00
41	-4.42	-1.61	72.00	42	-4.41	-2.06	72.00
43	-4.34	-2.51	72.00	44	-4.15	-2.95	72.00
45	-4.05	-3.39	72.00	46	-3.91	-3.91	72.00
47	-3.72	-4.44	72.00	48	-3.51	-5.01	72.00
49	-3.17	-5.48	72.00	50	-2.79	-5.98	72.00
51	-2.37	-6.52	72.00	52	-1.89	-7.07	72.00
53	-1.29	-7.34	72.00	54	-.66	-7.55	72.00
55	-0.00	-7.54	72.00	56	.64	-7.29	72.00
57	1.25	-7.09	72.00	58	1.80	-6.70	72.00
59	2.30	-6.32	72.00	60	2.82	-6.04	72.00
61	3.29	-5.69	72.00	62	3.83	-5.47	72.00
63	4.29	-5.12	72.00	64	4.64	-4.64	72.00
65	5.13	-4.30	72.00	66	5.55	-3.88	72.00
67	5.86	-3.39	72.00	68	6.16	-2.87	72.00
69	6.43	-2.34	72.00	70	6.70	-1.79	72.00
71	6.92	-1.22	72.00	72	7.23	-.63	72.00
73	7.29	-0.00	72.00				

1	8.23	0.00	80.00	2	8.21	.72	80.00
3	8.33	1.47	80.00	4	8.09	2.17	80.00
5	7.72	2.81	80.00	6	7.40	3.45	80.00
7	7.07	4.08	80.00	8	6.62	4.64	80.00
9	5.90	4.95	80.00	10	5.31	5.31	80.00
11	4.77	5.68	80.00	12	4.22	6.03	80.00
13	3.67	6.36	80.00	14	3.06	6.56	80.00
15	2.51	6.89	80.00	16	1.86	6.94	80.00
17	1.27	7.17	80.00	18	.63	7.23	80.00
19	0.00	7.20	80.00	20	-.63	7.18	80.00
21	-1.25	7.08	80.00	22	-1.80	6.73	80.00

23	-2.38	6.55	80.00
25	-3.20	5.55	80.00
27	-3.72	4.43	80.00
29	-4.17	3.50	80.00
31	-4.46	2.58	80.00
33	-4.60	1.67	80.00
35	-4.62	.82	80.00
37	-4.68	0.00	80.00
39	-4.61	-.81	80.00
41	-4.42	-1.61	80.00
43	-4.34	-2.51	80.00
45	-4.05	-3.39	80.00
47	-3.72	-4.44	80.00
49	-3.17	-5.48	80.00
51	-2.37	-6.52	80.00
53	-1.32	-7.50	80.00
55	-0.00	-7.93	80.00
57	1.31	-7.41	80.00
59	2.44	-6.71	80.00
61	3.57	-6.19	80.00
63	4.63	-5.52	80.00
65	5.44	-4.57	80.00
67	6.47	-3.73	80.00
69	7.45	-2.71	80.00
71	8.14	-1.44	80.00
73	8.23	-0.00	80.00

24	-2.84	6.09	80.00
26	-3.56	5.09	80.00
28	-3.98	3.98	80.00
30	-4.38	3.07	80.00
32	-4.56	2.13	80.00
34	-4.60	1.23	80.00
36	-4.70	.41	80.00
38	-4.67	-.41	80.00
40	-4.51	-1.21	80.00
42	-4.41	-2.06	80.00
44	-4.22	-2.95	80.00
46	-3.91	-3.91	80.00
48	-3.51	-5.01	80.00
50	-2.79	-5.98	80.00
52	-1.89	-7.06	80.00
54	-.67	-7.69	80.00
56	.68	-7.78	80.00
58	1.88	-7.03	80.00
60	3.00	-6.44	80.00
62	4.09	-5.84	80.00
64	5.03	-5.03	80.00
66	5.96	-4.18	80.00
68	6.99	-3.26	80.00
70	7.91	-2.12	80.00
72	8.27	-.72	80.00

1	8.68	0.00	88.00
3	8.66	1.53	88.00
5	8.02	2.92	88.00
7	7.21	4.16	88.00
9	5.90	4.95	88.00
11	4.77	5.68	88.00
13	3.67	6.36	88.00
15	2.51	6.89	88.00
17	1.27	7.18	88.00
19	0.00	7.33	88.00
21	-1.26	7.17	88.00
23	-2.44	6.71	88.00
25	-3.35	5.80	88.00
27	-4.01	4.78	88.00
29	-4.44	3.72	88.00
31	-4.66	2.69	88.00
33	-4.71	1.72	88.00
35	-4.80	.85	88.00
37	-4.68	0.00	88.00
39	-4.62	-.82	88.00
41	-4.42	-1.61	88.00
43	-4.34	-2.51	88.00
45	-4.05	-3.39	88.00
47	-3.74	-4.45	88.00
49	-3.34	-5.78	88.00
51	-2.59	-7.11	88.00
53	-1.41	-8.02	88.00
55	-0.00	-8.18	88.00
57	1.31	-7.41	88.00
59	2.44	-6.71	88.00
61	3.57	-6.19	88.00
63	4.63	-5.52	88.00
65	5.44	-4.56	88.00
67	6.46	-3.73	88.00
69	7.72	-2.81	88.00

2	8.80	.77	88.00
4	8.39	2.25	88.00
6	7.67	3.58	88.00
8	6.64	4.65	88.00
10	5.31	5.31	88.00
12	4.22	6.03	88.00
14	3.06	6.56	88.00
16	1.86	6.94	88.00
18	.63	7.22	88.00
20	-.64	7.31	88.00
22	-1.88	7.00	88.00
24	-2.89	6.19	88.00
26	-3.71	5.30	88.00
28	-4.34	4.34	88.00
30	-4.62	3.24	88.00
32	-4.67	2.18	88.00
34	-4.74	1.27	88.00
36	-4.78	.42	88.00
38	-4.69	-.41	88.00
40	-4.51	-1.21	88.00
42	-4.41	-2.06	88.00
44	-4.22	-2.95	88.00
46	-3.91	-3.91	88.00
48	-3.55	-5.08	88.00
50	-3.04	-6.51	88.00
52	-2.06	-7.67	88.00
54	-.71	-8.17	88.00
56	.68	-7.81	88.00
58	1.88	-7.03	88.00
60	3.00	-6.44	88.00
62	4.09	-5.84	88.00
64	5.03	-5.03	88.00
66	5.96	-4.18	88.00
68	7.13	-3.33	88.00
70	8.19	-2.19	88.00

71	8.43	-1.49	88.00	72	8.58	-.75	88.00
73	8.68	-0.00	88.00				
1	9.21	0.00	92.00	2	9.35	.82	92.00
3	9.20	1.62	92.00	4	8.68	2.32	92.00
5	8.42	3.07	92.00	6	7.98	3.72	92.00
7	7.34	4.24	92.00	8	6.65	4.66	92.00
9	5.90	4.95	92.00	10	5.31	5.31	92.00
11	4.77	5.68	92.00	12	4.22	6.03	92.00
13	3.67	6.36	92.00	14	3.06	6.56	92.00
15	2.51	6.89	92.00	16	1.86	6.94	92.00
17	1.27	7.18	92.00	18	.63	7.22	92.00
19	0.00	7.33	92.00	20	-.64	7.31	92.00
21	-1.26	7.17	92.00	22	-1.88	7.00	92.00
23	-2.44	6.71	92.00	24	-2.89	6.19	92.00
25	-3.35	5.80	92.00	26	-3.71	5.30	92.00
27	-4.01	4.78	92.00	28	-4.34	4.34	92.00
29	-4.44	3.72	92.00	30	-4.62	3.24	92.00
31	-4.66	2.69	92.00	32	-4.67	2.18	92.00
33	-4.71	1.72	92.00	34	-4.74	1.27	92.00
35	-4.80	.85	92.00	36	-4.78	.42	92.00
37	-4.68	0.00	92.00	38	-4.69	-.41	92.00
39	-4.62	-.82	92.00	40	-4.51	-1.21	92.00
41	-4.42	-1.61	92.00	42	-4.41	-2.06	92.00
43	-4.34	-2.51	92.00	44	-4.22	-2.95	92.00
45	-4.05	-3.39	92.00	46	-3.91	-3.91	92.00
47	-3.74	-4.45	92.00	48	-3.55	-5.08	92.00
49	-3.34	-5.78	92.00	50	-3.04	-6.51	92.00
51	-2.59	-7.11	92.00	52	-2.06	-7.67	92.00
53	-1.41	-8.02	92.00	54	-.71	-8.17	92.00
55	-0.00	-8.18	92.00	56	.68	-7.81	92.00
57	1.31	-7.41	92.00	58	1.88	-7.03	92.00
59	2.44	-6.71	92.00	60	3.00	-6.44	92.00
61	3.57	-6.19	92.00	62	4.09	-5.84	92.00
63	4.63	-5.52	92.00	64	5.03	-5.03	92.00
65	5.44	-4.56	92.00	66	5.96	-4.18	92.00
67	6.46	-3.73	92.00	68	7.13	-3.33	92.00
69	7.72	-2.81	92.00	70	8.18	-2.19	92.00
71	8.62	-1.52	92.00	72	8.80	-.77	92.00
73	9.21	-0.00	92.00				
1	10.30	0.00	96.00	2	10.57	.92	96.00
3	10.55	1.86	96.00	4	9.90	2.65	96.00
5	9.41	3.42	96.00	6	8.86	4.13	96.00
7	7.98	4.61	96.00	8	7.26	5.08	96.00
9	6.48	5.44	96.00	10	5.68	5.68	96.00
11	5.02	5.98	96.00	12	4.35	6.22	96.00
13	3.79	6.57	96.00	14	3.13	6.72	96.00
15	2.51	6.91	96.00	16	1.86	6.94	96.00
17	1.27	7.18	96.00	18	.63	7.21	96.00
19	0.00	7.49	96.00	20	-.67	7.64	96.00
21	-1.34	7.62	96.00	22	-2.04	7.61	96.00
23	-2.66	7.31	96.00	24	-3.22	6.90	96.00
25	-3.54	6.13	96.00	26	-3.88	5.54	96.00
27	-4.15	4.95	96.00	28	-4.38	4.38	96.00
29	-4.46	3.75	96.00	30	-4.62	3.23	96.00
31	-4.78	2.76	96.00	32	-4.89	2.28	96.00
33	-4.79	1.74	96.00	34	-4.82	1.29	96.00
35	-4.86	.86	96.00	36	-4.97	.44	96.00
37	-4.97	0.00	96.00	38	-4.91	-.43	96.00
39	-4.80	-.8	96.00	40	-4.83	-1.29	96.00
41	-4.78	-1.74	96.00	42	-4.60	-2.14	96.00

43	-4.45	-2.57	96.00
45	-4.04	-3.39	96.00
47	-3.78	-4.51	96.00
49	-3.33	-5.77	96.00
51	-2.60	-7.14	96.00
53	-1.41	-8.02	96.00
55	-0.00	-8.18	96.00
57	1.31	-7.41	96.00
59	2.44	-6.71	96.00
61	3.57	-6.19	96.00
63	4.63	-5.52	96.00
65	5.44	-4.56	96.00
67	6.46	-3.73	96.00
69	7.71	-2.81	96.00
71	9.12	-1.61	96.00
73	10.30	-0.00	96.00

44	-4.23	-2.96	96.00
46	-3.91	-3.91	96.00
48	-3.57	-5.09	96.00
50	-3.09	-6.63	96.00
52	-2.05	-7.67	96.00
54	-.71	-8.17	96.00
56	.68	-7.81	96.00
58	1.88	-7.03	96.00
60	3.00	-6.44	96.00
62	4.09	-5.84	96.00
64	5.03	-5.03	96.00
66	5.96	-4.18	96.00
68	7.13	-3.33	96.00
70	8.28	-2.22	96.00
72	9.85	-.86	96.00

1	10.40	0.00	100.00
3	10.61	1.87	100.00
5	9.65	3.51	100.00
7	8.14	4.70	100.00
9	6.65	5.58	100.00
11	5.40	6.44	100.00
13	4.02	6.97	100.00
15	2.79	7.67	100.00
17	1.40	7.92	100.00
19	0.00	7.87	100.00
21	-1.38	7.81	100.00
23	-2.73	7.50	100.00
25	-3.91	6.77	100.00
27	-4.74	5.65	100.00
29	-5.20	4.36	100.00
31	-5.38	3.11	100.00
33	-5.23	1.90	100.00
35	-5.20	.92	100.00
37	-5.03	0.00	100.00
39	-5.10	-.90	100.00
41	-4.93	-1.79	100.00
43	-4.82	-2.78	100.00
45	-4.44	-3.73	100.00
47	-4.14	-4.94	100.00
49	-3.82	-6.61	100.00
51	-2.82	-7.74	100.00
53	-1.49	-8.43	100.00
55	-0.00	-8.26	100.00
57	1.32	-7.50	100.00
59	2.44	-6.71	100.00
61	3.57	-6.19	100.00
63	4.63	-5.52	100.00
65	5.44	-4.56	100.00
67	6.46	-3.73	100.00
69	7.71	-2.81	100.00
71	9.12	-1.61	100.00
73	10.40	-0.00	100.00

2	10.76	.94	100.00
4	10.14	2.72	100.00
6	9.05	4.22	100.00
8	7.33	5.13	100.00
10	6.01	6.01	100.00
12	4.71	6.73	100.00
14	3.38	7.25	100.00
16	2.10	7.83	100.00
18	.69	7.93	100.00
20	-.69	7.83	100.00
22	-2.10	7.83	100.00
24	-3.38	7.25	100.00
26	-4.33	6.18	100.00
28	-4.99	4.99	100.00
30	-5.31	3.71	100.00
32	-5.24	2.44	100.00
34	-5.33	1.43	100.00
36	-5.07	.44	100.00
38	-5.04	-.44	100.00
40	-5.03	-1.35	100.00
42	-4.90	-2.29	100.00
44	-4.69	-3.28	100.00
46	-4.29	-4.29	100.00
48	-4.00	-5.71	100.00
50	-3.36	-7.22	100.00
52	-2.20	-8.22	100.00
54	-.75	-8.62	100.00
56	.68	-7.79	100.00
58	1.89	-7.05	100.00
60	3.00	-6.44	100.00
62	4.09	-5.84	100.00
64	5.03	-5.03	100.00
66	5.96	-4.18	100.00
68	7.13	-3.33	100.00
70	8.28	-2.22	100.00
72	9.89	-.87	100.00

1	10.92	0.00	104.00
3	11.20	1.98	104.00
5	10.31	3.75	104.00
7	8.74	5.05	104.00
9	7.26	6.09	104.00
11	5.58	6.65	104.00
13	4.27	7.39	104.00

2	11.36	.99	104.00
4	10.97	2.94	104.00
6	9.56	4.46	104.00
8	7.96	5.58	104.00
10	6.36	6.36	104.00
12	4.95	7.07	104.00
14	3.51	7.54	104.00

15	2.81	7.71	104.00	16	2.10	7.82	104.00
17	1.41	7.98	104.00	18	.71	8.15	104.00
19	0.00	8.30	104.00	20	-.74	8.43	104.00
21	-1.51	8.54	104.00	22	-2.24	8.34	104.00
23	-3.00	8.24	104.00	24	-3.62	7.77	104.00
25	-4.20	7.27	104.00	26	-4.70	6.71	104.00
27	-5.00	5.96	104.00	28	-5.28	5.28	104.00
29	-5.31	4.45	104.00	30	-5.35	3.75	104.00
31	-5.39	3.11	104.00	32	-5.45	2.54	104.00
33	-5.49	2.00	104.00	34	-5.48	1.47	104.00
35	-5.69	1.00	104.00	36	-5.70	.50	104.00
37	-5.72	0.00	104.00	38	-5.71	-.50	104.00
39	-5.58	-.98	104.00	40	-5.48	-1.47	104.00
41	-5.54	-2.02	104.00	42	-5.53	-2.58	104.00
43	-5.54	-3.20	104.00	44	-5.43	-3.80	104.00
45	-5.29	-4.43	104.00	46	-5.09	-5.09	104.00
47	-4.90	-5.84	104.00	48	-4.64	-6.30	104.00
49	-4.22	-7.32	104.00	50	-3.79	-8.13	104.00
51	-3.20	-8.80	104.00	52	-2.43	-9.08	104.00
53	-1.60	-9.10	104.00	54	-.77	-8.77	104.00
55	-0.00	-8.25	104.00	56	.68	-7.79	104.00
57	1.32	-7.50	104.00	58	1.89	-7.05	104.00
59	2.44	-6.71	104.00	60	3.00	-6.44	104.00
61	3.57	-6.18	104.00	62	4.15	-5.92	104.00
63	4.80	-5.72	104.00	64	5.36	-5.36	104.00
65	5.88	-4.93	104.00	66	6.53	-4.57	104.00
67	7.07	-4.08	104.00	68	7.59	-3.54	104.00
69	8.27	-3.01	104.00	70	9.00	-2.41	104.00
71	9.85	-1.74	104.00	72	10.41	-.91	104.00
73	10.92	-0.00	104.00				
1	11.82	0.00	108.00	2	11.95	1.05	108.00
3	11.67	2.06	108.00	4	11.27	3.02	108.00
5	10.73	3.91	108.00	6	10.12	4.72	108.00
7	9.28	5.36	108.00	8	8.37	5.86	108.00
9	7.50	6.29	108.00	10	6.66	6.66	108.00
11	5.92	7.06	108.00	12	5.20	7.43	108.00
13	4.47	7.75	108.00	14	3.80	8.15	108.00
15	3.06	8.42	108.00	16	2.28	8.50	108.00
17	1.51	8.55	108.00	18	.77	8.77	108.00
19	0.00	9.03	108.00	20	-.80	9.10	108.00
21	-1.63	9.26	108.00	22	-2.48	9.27	108.00
23	-3.28	9.00	108.00	24	-3.93	8.43	108.00
25	-4.53	7.84	108.00	26	-5.01	7.16	108.00
27	-5.44	6.49	108.00	28	-5.77	5.77	108.00
29	-6.09	5.11	108.00	30	-6.18	4.33	108.00
31	-6.30	3.64	108.00	32	-6.27	2.92	108.00
33	-6.16	2.24	108.00	34	-6.10	1.64	108.00
35	-6.12	1.08	108.00	36	-6.09	.53	108.00
37	-5.96	0.00	108.00	38	-5.86	-.51	108.00
39	-5.83	-1.03	108.00	40	-5.95	-1.59	108.00
41	-5.90	-2.15	108.00	42	-5.79	-2.70	108.00
43	-5.72	-3.30	108.00	44	-5.62	-3.94	108.00
45	-5.63	-4.72	108.00	46	-5.54	-5.54	108.00
47	-5.39	-6.43	108.00	48	-5.01	-7.16	108.00
49	-4.52	-7.82	108.00	50	-3.98	-8.54	108.00
51	-3.26	-8.95	108.00	52	-2.44	-9.10	108.00
53	-1.60	-9.10	108.00	54	-.77	-8.77	108.00
55	-0.00	-8.25	108.00	56	.68	-7.79	108.00
57	1.32	-7.50	108.00	58	1.89	-7.05	108.00
59	2.44	-6.71	108.00	60	3.00	-6.44	108.00
61	3.57	-6.18	108.00	62	4.15	-5.92	108.00

63	4.80	-5.72	108.00	64	5.36	-5.36	108.00
65	5.88	-4.93	108.00	66	6.53	-4.57	108.00
67	7.07	-4.08	108.00	68	7.59	-3.54	108.00
69	8.26	-3.01	108.00	70	9.18	-2.46	108.00
71	10.30	-1.82	108.00	72	11.10	-.97	108.00
73	11.82	-0.00	108.00				

1	12.25	0.00	112.00	2	12.94	1.13	112.00
3	12.50	2.20	112.00	4	11.68	3.13	112.00
5	10.96	3.99	112.00	6	10.37	4.84	112.00
7	9.64	5.57	112.00	8	8.90	6.23	112.00
9	7.93	6.65	112.00	10	7.13	7.13	112.00
11	6.17	7.36	112.00	12	5.40	7.71	112.00
13	4.70	8.14	112.00	14	3.89	8.35	112.00
15	3.07	8.45	112.00	16	2.34	8.74	112.00
17	1.58	8.95	112.00	18	.80	9.14	112.00
19	0.00	9.34	112.00	20	-.84	9.58	112.00
21	-1.67	9.45	112.00	22	-2.52	9.40	112.00
23	-3.45	9.47	112.00	24	-4.38	9.38	112.00
25	-5.13	8.88	112.00	26	-5.91	8.45	112.00
27	-6.58	7.85	112.00	28	-7.14	7.14	112.00
29	-7.68	6.44	112.00	30	-7.97	5.58	112.00
31	-8.19	4.73	112.00	32	-8.31	3.87	112.00
33	-8.27	3.01	112.00	34	-8.28	2.22	112.00
35	-8.30	1.46	112.00	36	-8.19	.72	112.00
37	-8.19	0.00	112.00	38	-7.92	-.69	112.00
39	-7.81	-1.38	112.00	40	-7.57	-2.03	112.00
41	-7.45	-2.71	112.00	42	-7.39	-3.44	112.00
43	-7.09	-4.10	112.00	44	-7.01	-4.91	112.00
45	-6.66	-5.59	112.00	46	-6.31	-6.31	112.00
47	-5.86	-6.99	112.00	48	-5.37	-7.67	112.00
49	-4.76	-8.24	112.00	50	-4.06	-8.72	112.00
51	-3.29	-9.05	112.00	52	-2.45	-9.15	112.00
53	-1.61	-9.10	112.00	54	-.77	-8.77	112.00
55	-0.00	-8.25	112.00	56	.68	-7.79	112.00
57	1.32	-7.49	112.00	58	1.89	-7.05	112.00
59	2.44	-6.71	112.00	60	3.00	-6.44	112.00
61	3.57	-6.18	112.00	62	4.15	-5.92	112.00
63	4.80	-5.72	112.00	64	5.36	-5.36	112.00
65	5.88	-4.93	112.00	66	6.53	-4.57	112.00
67	7.08	-4.08	112.00	68	7.59	-3.54	112.00
69	8.26	-3.01	112.00	70	9.18	-2.46	112.00
71	10.29	-1.81	112.00	72	11.27	-.99	112.00
73	12.25	-0.00	112.00				

1	14.06	0.00	116.00	2	14.22	1.24	116.00
3	13.71	2.42	116.00	4	13.21	3.54	116.00
5	12.36	4.50	116.00	6	11.61	5.42	116.00
7	10.65	6.15	116.00	8	9.51	6.66	116.00
9	8.60	7.22	116.00	10	7.79	7.79	116.00
11	6.89	8.22	116.00	12	6.00	8.57	116.00
13	5.14	8.91	116.00	14	4.25	9.11	116.00
15	3.41	9.38	116.00	16	2.52	9.42	116.00
17	1.69	9.60	116.00	18	.86	9.86	116.00
19	0.00	10.08	116.00	20	-.89	10.21	116.00
21	-1.82	10.35	116.00	22	-2.82	10.54	116.00
23	-3.90	10.71	116.00	24	-5.07	10.87	116.00
25	-6.11	10.58	116.00	26	-7.03	10.03	116.00
27	-7.82	9.32	116.00	28	-8.22	8.22	116.00
29	-8.73	7.33	116.00	30	-9.16	6.41	116.00
31	-9.49	5.48	116.00	32	-9.65	4.50	116.00
33	-9.88	3.60	116.00	34	-9.88	2.65	116.00

35	-10.23	1.80	116.00
37	-10.14	0.00	116.00
39	-9.53	-1.68	116.00
41	-8.93	-3.25	116.00
43	-8.33	-4.81	116.00
45	-7.70	-6.46	116.00
47	-6.95	-8.28	116.00
49	-5.70	-9.87	116.00
51	-3.77	-10.37	116.00
53	-1.65	-9.36	116.00
55	-0.00	-8.33	116.00
57	1.33	-7.52	116.00
59	2.44	-6.71	116.00
61	3.57	-6.18	116.00
63	4.79	-5.71	116.00
65	6.04	-5.07	116.00
67	7.61	-4.40	116.00
69	9.68	-3.52	116.00
71	11.80	-2.08	116.00
73	14.06	-0.00	116.00

36	-10.29	.90	116.00
38	-9.85	-.86	116.00
40	-9.23	-2.47	116.00
42	-8.63	-4.02	116.00
44	-8.02	-5.62	116.00
46	-7.36	-7.36	116.00
48	-6.43	-9.18	116.00
50	-4.79	-10.28	116.00
52	-2.70	-10.06	116.00
56	-.77	-8.77	116.00
56	.70	-7.95	116.00
58	1.89	-7.05	116.00
60	3.00	-6.44	116.00
62	4.15	-5.92	116.00
64	5.48	-5.48	116.00
66	6.72	-4.71	116.00
68	8.55	-3.99	116.00
70	10.71	-2.87	116.00
72	13.04	-1.14	116.00

1	16.57	0.00	120.00
3	15.52	2.74	120.00
5	13.08	4.76	120.00
7	10.89	6.29	120.00
9	8.85	7.43	120.00
11	6.91	8.24	120.00
13	5.21	9.02	120.00
15	3.46	9.49	120.00
17	1.77	10.07	120.00
19	0.00	10.70	120.00
21	-2.00	11.34	120.00
23	-4.35	11.96	120.00
25	-6.95	12.04	120.00
27	-8.78	10.47	120.00
29	-10.26	8.61	120.00
31	-11.41	6.59	120.00
33	-11.87	4.32	120.00
35	-11.26	1.99	120.00
37	-10.50	0.00	120.00
39	-9.83	-1.73	120.00
41	-9.21	-3.35	120.00
43	-8.59	-4.96	120.00
45	-7.94	-6.66	120.00
47	-7.06	-8.41	120.00
49	-5.58	-9.67	120.00
51	-3.67	-10.08	120.00
53	-1.65	-9.34	120.00
55	-0.00	-8.35	120.00
57	1.33	-7.52	120.00
59	2.44	-6.71	120.00
61	3.57	-6.18	120.00
63	4.79	-5.71	120.00
65	6.04	-5.07	120.00
67	7.61	-4.39	120.00
69	9.99	-3.64	120.00
71	14.21	-2.51	120.00
73	16.57	-0.00	120.00

2	16.06	1.41	120.00
4	14.27	3.82	120.00
6	11.93	5.56	120.00
8	9.87	6.91	120.00
10	7.95	7.95	120.00
12	6.00	8.56	120.00
14	4.39	9.42	120.00
16	2.58	9.63	120.00
18	.90	10.34	120.00
20	-.95	10.91	120.00
22	-3.16	11.79	120.00
24	-5.63	12.07	120.00
26	-7.97	11.38	120.00
28	-9.46	9.46	120.00
30	-10.78	7.55	120.00
32	-11.82	5.51	120.00
34	-11.67	3.13	120.00
36	-10.86	.95	120.00
38	-10.16	-.89	120.00
40	-9.52	-2.55	120.00
42	-8.90	-4.15	120.00
44	-8.27	-5.79	120.00
46	-7.54	-7.54	120.00
48	-6.40	-9.14	120.00
50	-4.66	-10.00	120.00
52	-2.66	-9.94	120.00
54	-.78	-8.86	120.00
56	.70	-7.94	120.00
58	1.89	-7.05	120.00
60	3.00	-6.44	120.00
62	4.15	-5.92	120.00
64	5.48	-5.48	120.00
66	6.72	-4.71	120.00
68	8.69	-4.05	120.00
70	11.59	-3.11	120.00
72	15.94	-1.39	120.00

1	18.67	0.00	124.00
3	17.93	3.16	124.00
5	15.71	5.72	124.00

2	18.55	1.62	124.00
4	17.04	4.57	124.00
6	14.21	6.63	124.00

7	12.71	7.34	124.00	8	11.29	7.91	124.00
9	9.91	8.32	124.00	10	8.44	8.44	124.00
11	7.48	8.92	124.00	12	6.51	9.30	124.00
13	5.56	9.63	124.00	14	4.63	9.92	124.00
15	3.71	10.19	124.00	16	2.81	10.47	124.00
17	1.87	10.61	124.00	18	.96	10.95	124.00
19	0.00	11.23	124.00	20	-.98	11.18	124.00
21	-2.04	11.56	124.00	22	-3.16	11.81	124.00
23	-4.42	12.15	124.00	24	-5.84	12.53	124.00
25	-7.23	12.53	124.00	26	-8.61	12.29	124.00
27	-9.85	11.74	124.00	28	-10.88	10.88	124.00
29	-11.65	9.78	124.00	30	-12.10	8.47	124.00
31	-12.18	7.03	124.00	32	-11.96	5.58	124.00
33	-11.46	4.17	124.00	34	-10.98	2.94	124.00
35	-10.57	1.86	124.00	36	-10.20	.89	124.00
37	-9.85	0.00	124.00	38	-9.53	-.83	124.00
39	-9.23	-1.63	124.00	40	-8.94	-2.39	124.00
41	-8.65	-3.15	124.00	42	-8.36	-3.90	124.00
43	-8.07	-4.66	124.00	44	-7.77	-5.44	124.00
45	-7.42	-6.23	124.00	46	-7.00	-7.00	124.00
47	-6.46	-7.69	124.00	48	-5.80	-8.28	124.00
49	-5.05	-8.75	124.00	50	-4.23	-9.07	124.00
51	-3.37	-9.25	124.00	52	-2.48	-9.27	124.00
53	-1.61	-9.13	124.00	54	-.77	-8.85	124.00
55	-0.00	-8.44	124.00	56	.70	-7.96	124.00
57	1.33	-7.52	124.00	58	1.89	-7.05	124.00
59	2.44	-6.71	124.00	60	3.00	-6.44	124.00
61	3.57	-6.18	124.00	62	4.15	-5.92	124.00
63	4.79	-5.71	124.00	64	5.48	-5.48	124.00
65	6.04	-5.07	124.00	66	6.72	-4.71	124.00
67	7.61	-4.39	124.00	68	8.69	-4.05	124.00
69	9.99	-3.64	124.00	70	11.58	-3.10	124.00
71	14.63	-2.58	124.00	72	17.36	-1.52	124.00
73	18.67	-0.00	124.00				

1	20.78	0.00	128.00	2	21.21	1.86	128.00
3	20.42	3.60	128.00	4	19.68	5.27	128.00
5	18.25	6.64	128.00	6	16.46	7.67	128.00
7	14.37	8.29	128.00	8	12.64	8.85	128.00
9	11.04	9.26	128.00	10	9.71	9.71	128.00
11	8.28	9.86	128.00	12	7.11	10.15	128.00
13	6.05	10.49	128.00	14	5.08	10.89	128.00
15	4.03	11.07	128.00	16	3.00	11.19	128.00
17	2.04	11.59	128.00	18	1.02	11.63	128.00
19	0.00	11.75	128.00	20	-1.06	12.13	128.00
21	-2.18	12.35	128.00	22	-3.39	12.66	128.00
23	-4.69	12.89	128.00	24	-6.08	13.03	128.00
25	-7.45	12.91	128.00	26	-8.71	12.44	128.00
27	-9.78	11.66	128.00	28	-10.62	10.62	128.00
29	-11.17	9.37	128.00	30	-11.33	7.94	128.00
31	-11.19	6.46	128.00	32	-10.70	4.99	128.00
33	-10.21	3.72	128.00	34	-9.79	2.62	128.00
35	-9.42	1.66	128.00	36	-9.09	.80	128.00
37	-8.78	0.00	128.00	38	-8.50	-.74	128.00
39	-8.23	-1.45	128.00	40	-7.96	-2.13	128.00
41	-7.71	-2.80	128.00	42	-7.45	-3.47	128.00
43	-7.19	-4.15	128.00	44	-6.92	-4.85	128.00
45	-6.62	-5.55	128.00	46	-6.25	-6.25	128.00
47	-5.78	-6.88	128.00	48	-5.21	-7.44	128.00
49	-4.56	-7.90	128.00	50	-3.85	-8.25	128.00
51	-3.09	-8.48	128.00	52	-2.30	-8.59	128.00
53	-1.51	-8.58	128.00	54	-.74	-8.44	128.00

55	-0.00	-8.18	128.00
57	1.29	-7.34	128.00
59	2.44	-6.72	128.00
61	3.57	-6.18	128.00
63	4.79	-5.71	128.00
65	6.04	-5.07	128.00
67	7.61	-4.39	128.00
69	9.99	-3.64	128.00
71	14.59	-2.57	128.00
73	20.78	-0.00	128.00

56	.68	-7.81	128.00
58	1.88	-7.02	128.00
60	3.00	-6.44	128.00
62	4.15	-5.92	128.00
64	5.48	-5.48	128.00
66	6.72	-4.71	128.00
68	8.69	-4.05	128.00
70	11.59	-3.11	128.00
72	18.62	-1.63	128.00

1	24.35	0.00	132.00
3	23.81	4.20	132.00
5	20.33	7.40	132.00
7	15.91	9.18	132.00
9	12.05	10.11	132.00
11	9.17	10.93	132.00
13	6.55	11.34	132.00
15	4.40	12.10	132.00
17	2.27	12.85	132.00
19	0.00	13.23	132.00
21	-2.43	13.79	132.00
23	-5.17	14.20	132.00
25	-7.74	13.40	132.00
27	-9.70	11.56	132.00
29	-10.67	8.95	132.00
31	-10.42	6.01	132.00
33	-9.46	3.44	132.00
35	-8.73	1.54	132.00
37	-8.14	0.00	132.00
39	-7.62	-1.34	132.00
41	-7.14	-2.60	132.00
43	-6.66	-3.85	132.00
45	-6.13	-5.15	132.00
47	-5.42	-6.45	132.00
49	-4.37	-7.57	132.00
51	-3.06	-8.40	132.00
53	-1.56	-8.86	132.00
55	-0.00	-8.92	132.00
57	1.52	-8.62	132.00
59	2.91	-7.99	132.00
61	4.36	-7.55	132.00
63	5.88	-7.01	132.00
65	7.82	-6.56	132.00
67	10.09	-5.82	132.00
69	13.23	-4.82	132.00
71	19.01	-3.35	132.00
73	24.35	-0.00	132.00

2	24.23	2.12	132.00
4	22.51	6.03	132.00
6	17.98	8.38	132.00
8	13.67	9.57	132.00
10	10.67	10.67	132.00
12	7.80	11.14	132.00
14	5.46	11.70	132.00
16	3.35	12.51	132.00
18	1.14	13.04	132.00
20	-1.17	13.39	132.00
22	-3.79	14.16	132.00
24	-6.50	13.94	132.00
26	-8.82	12.59	132.00
28	-10.33	10.33	132.00
30	-10.66	7.46	132.00
32	-9.92	4.63	132.00
34	-9.08	2.43	132.00
36	-8.42	.74	132.00
38	-7.88	-.69	132.00
40	-7.38	-1.98	132.00
42	-6.90	-3.22	132.00
44	-6.42	-4.49	132.00
46	-5.81	-5.81	132.00
48	-4.93	-7.04	132.00
50	-3.74	-8.03	132.00
52	-2.33	-8.68	132.00
54	-.78	-8.94	132.00
56	.77	-8.80	132.00
58	2.22	-8.29	132.00
60	3.63	-7.78	132.00
62	5.09	-7.28	132.00
64	6.79	-6.79	132.00
66	8.94	-6.26	132.00
68	11.40	-5.32	132.00
70	15.23	-4.08	132.00
72	22.77	-1.99	132.00

1	27.92	0.00	136.00
3	26.96	4.75	136.00
5	22.79	8.30	136.00
7	17.89	10.33	136.00
9	14.06	11.80	136.00
11	10.60	12.64	136.00
13	7.59	13.14	136.00
15	4.94	13.57	136.00
17	2.53	14.33	136.00
19	0.00	14.60	136.00
21	-2.64	14.96	136.00
23	-5.30	14.56	136.00
25	-7.63	13.21	136.00

2	27.87	2.44	136.00
4	25.28	6.77	136.00
6	20.27	9.45	136.00
8	15.97	11.18	136.00
10	12.10	12.10	136.00
12	9.04	12.91	136.00
14	6.21	13.33	136.00
16	3.74	13.98	136.00
18	1.26	14.39	136.00
20	-1.30	14.91	136.00
22	-3.99	14.88	136.00
24	-6.53	14.01	136.00
26	-8.56	12.22	136.00

27	-9.29	11.07	136.00
29	-10.01	8.40	136.00
31	-9.72	5.61	136.00
33	-8.84	3.22	136.00
35	-8.16	1.44	136.00
37	-7.61	0.00	136.00
39	-7.12	-1.26	136.00
41	-6.67	-2.43	136.00
43	-6.23	-3.59	136.00
45	-5.70	-4.78	136.00
47	-4.95	-5.90	136.00
49	-3.97	-6.88	136.00
51	-2.79	-7.68	136.00
53	-1.45	-8.22	136.00
55	-0.00	-8.48	136.00
57	1.49	-8.42	136.00
59	2.91	-8.00	136.00
61	4.36	-7.55	136.00
63	5.88	-7.01	136.00
65	7.82	-6.56	136.00
67	10.09	-5.82	136.00
69	13.26	-4.83	136.00
71	21.90	-3.86	136.00
73	27.92	-0.00	136.00

28	-9.78	9.78	136.00
30	-9.93	6.95	136.00
32	-9.27	4.32	136.00
34	-8.48	2.27	136.00
36	-7.87	.69	136.00
38	-7.36	-.64	136.00
40	-6.90	-1.85	136.00
42	-6.45	-3.01	136.00
44	-5.98	-4.19	136.00
46	-5.36	-5.36	136.00
48	-4.49	-6.41	136.00
50	-3.41	-7.31	136.00
52	-2.14	-7.98	136.00
54	-.73	-8.39	136.00
56	.74	-8.49	136.00
58	2.22	-8.28	136.00
60	3.63	-7.78	136.00
62	5.09	-7.28	136.00
64	6.79	-6.79	136.00
66	8.94	-6.26	136.00
68	11.40	-5.31	136.00
70	16.01	-4.29	136.00
72	26.22	-2.29	136.00

1	34.50	-0.00	140.00
3	34.21	6.04	140.00
5	26.63	9.69	140.00
7	19.32	11.16	140.00
9	14.49	12.16	140.00
11	10.84	12.92	140.00
13	7.82	13.55	140.00
15	5.14	14.11	140.00
17	2.58	14.64	140.00
19	0.00	15.18	140.00
21	-2.73	15.49	140.00
23	-5.39	14.79	140.00
25	-7.57	13.11	140.00
27	-8.96	10.67	140.00
29	-9.26	7.77	140.00
31	-8.40	4.85	140.00
33	-7.60	2.76	140.00
35	-7.01	1.24	140.00
37	-6.53	0.00	140.00
39	-6.12	-1.08	140.00
41	-5.73	-2.09	140.00
43	-5.35	-3.09	140.00
45	-4.94	-4.15	140.00
47	-4.41	-5.26	140.00
49	-3.64	-6.31	140.00
51	-2.64	-7.25	140.00
53	-1.41	-8.00	140.00
55	-0.00	-8.50	140.00
57	1.53	-8.68	140.00
59	3.10	-8.53	140.00
61	4.76	-8.24	140.00
63	6.65	-7.92	140.00
65	8.96	-7.52	140.00
67	12.09	-6.98	140.00
69	16.90	-6.15	140.00
71	26.11	-4.60	140.00
73	34.50	-0.00	140.00

2	35.12	3.07	140.00
4	31.37	8.40	140.00
6	22.50	10.50	140.00
8	16.71	11.70	140.00
10	12.57	12.56	140.00
12	9.28	13.25	140.00
14	6.45	13.84	140.00
16	3.85	14.38	140.00
18	1.31	14.91	140.00
20	-1.35	15.44	140.00
22	-4.09	15.27	140.00
24	-6.56	14.06	140.00
26	-8.38	11.97	140.00
28	-9.26	9.26	140.00
30	-8.91	6.24	140.00
32	-7.96	3.71	140.00
34	-7.28	1.95	140.00
36	-6.76	.59	140.00
38	-6.32	-.55	140.00
40	-5.92	-1.59	140.00
42	-5.54	-2.59	140.00
44	-5.15	-3.61	140.00
46	-4.70	-4.70	140.00
48	-4.06	-5.79	140.00
50	-3.17	-6.80	140.00
52	-2.05	-7.65	140.00
54	-.72	-8.28	140.00
56	.76	-8.63	140.00
58	2.32	-8.65	140.00
60	3.91	-8.39	140.00
62	5.66	-8.09	140.00
64	7.73	-7.73	140.00
66	10.39	-7.27	140.00
68	14.19	-6.62	140.00
70	20.57	-5.51	140.00
72	31.97	-2.80	140.00

1	46.45	0.00	144.00	2	45.76	4.00	144.00
3	44.38	7.83	144.00	4	41.38	11.09	144.00
5	34.14	12.43	144.00	6	27.71	12.92	144.00
7	23.05	13.31	144.00	8	19.45	13.61	144.00
9	16.52	13.86	144.00	10	14.07	14.07	144.00
11	11.96	14.25	144.00	12	10.09	14.40	144.00
13	8.40	14.55	144.00	14	6.85	14.68	144.00
15	5.39	14.80	144.00	16	3.99	14.92	144.00
17	2.65	15.03	144.00	18	1.32	15.14	144.00
19	-0.00	15.26	144.00	20	-1.35	15.35	144.00
21	-2.69	15.25	144.00	22	-3.99	14.89	144.00
23	-5.20	14.29	144.00	24	-6.28	13.46	144.00
25	-7.18	12.43	144.00	26	-7.87	11.24	144.00
27	-8.32	9.91	144.00	28	-8.49	8.49	144.00
29	-8.36	7.02	144.00	30	-7.91	5.54	144.00
31	-7.43	4.29	144.00	32	-7.04	3.28	144.00
33	-6.72	2.45	144.00	34	-6.45	1.73	144.00
35	-6.20	1.09	144.00	36	-5.98	.52	144.00
37	-5.78	0.00	144.00	38	-5.60	-.49	144.00
39	-5.42	-.96	144.00	40	-5.24	-1.40	144.00
41	-5.08	-1.85	144.00	42	-4.91	-2.29	144.00
43	-4.74	-2.73	144.00	44	-4.56	-3.19	144.00
45	-4.37	-3.67	144.00	46	-4.18	-4.18	144.00
47	-3.96	-4.71	144.00	48	-3.68	-5.25	144.00
49	-3.34	-5.78	144.00	50	-2.94	-6.30	144.00
51	-2.47	-6.80	144.00	52	-1.95	-7.26	144.00
53	-1.35	-7.68	144.00	54	-.70	-8.04	144.00
55	-0.00	-8.34	144.00	56	.75	-8.57	144.00
57	1.53	-8.71	144.00	58	2.35	-8.76	144.00
59	3.18	-8.73	144.00	60	4.04	-8.66	144.00
61	4.96	-8.60	144.00	62	5.97	-8.52	144.00
63	7.08	-8.44	144.00	64	8.35	-8.35	144.00
65	9.82	-8.24	144.00	66	11.58	-8.11	144.00
67	13.78	-7.95	144.00	68	16.60	-7.75	144.00
69	20.50	-7.46	144.00	70	26.25	-7.03	144.00
71	36.61	-6.46	144.00	72	44.22	-3.86	144.00
73	46.45	0.00	144.00				

1	52.39	-.01	148.00	2	50.90	4.46	148.00
3	49.31	8.70	148.00	4	46.68	12.51	148.00
5	38.50	14.02	148.00	6	30.73	14.33	148.00
7	25.20	14.55	148.00	8	21.01	14.72	148.00
9	17.69	14.85	148.00	10	14.96	14.95	148.00
11	12.62	15.05	148.00	12	10.59	15.13	148.00
13	8.77	15.20	148.00	14	7.12	15.26	148.00
15	5.58	15.33	148.00	16	4.12	15.38	148.00
17	2.72	15.44	148.00	18	1.36	15.49	148.00
19	-0.00	15.55	148.00	20	-1.35	15.50	148.00
21	-2.68	15.21	148.00	22	-3.93	14.66	148.00
23	-5.05	13.88	148.00	24	-6.01	12.88	148.00
25	-6.75	11.70	148.00	26	-7.26	10.37	148.00
27	-7.49	8.93	148.00	28	-7.40	7.40	148.00
29	-6.95	5.83	148.00	30	-6.45	4.51	148.00
31	-6.06	3.50	148.00	32	-5.74	2.68	148.00
33	-5.48	1.99	148.00	34	-5.25	1.41	148.00
35	-5.06	.89	148.00	36	-4.88	.43	148.00
37	-4.71	0.00	148.00	38	-4.56	-.40	148.00
39	-4.41	-.78	148.00	40	-4.27	-1.14	148.00
41	-4.14	-1.51	148.00	42	-4.00	-1.86	148.00
43	-3.86	-2.23	148.00	44	-3.71	-2.60	148.00
45	-3.56	-2.99	148.00	46	-3.41	-3.41	148.00

47	-3.23	-3.85	148.00
49	-2.83	-4.90	148.00
51	-2.22	-6.09	148.00
53	-1.28	-7.25	148.00
55	0.00	-8.26	148.00
57	1.58	-8.98	148.00
59	3.38	-9.29	148.00
61	5.34	-9.26	148.00
63	7.72	-9.20	148.00
65	10.87	-9.12	148.00
67	15.58	-9.00	148.00
69	24.13	-8.78	148.00
71	46.19	-8.14	148.00
73	52.39	-.01	148.00

48	-3.04	-4.35	148.00
50	-2.56	-5.49	148.00
52	-1.79	-6.68	148.00
54	-.68	-7.78	148.00
56	.76	-8.66	148.00
58	2.46	-9.19	148.00
60	4.33	-9.28	148.00
62	6.46	-9.23	148.00
64	9.16	-9.16	148.00
66	12.94	-9.06	148.00
68	19.11	-8.91	148.00
70	31.99	-8.57	148.00
72	51.71	-4.53	148.00

1	56.66	.01	152.00
3	53.38	9.41	152.00
5	39.63	14.42	152.00
7	25.64	14.81	152.00
9	17.96	15.08	152.00
11	12.80	15.26	152.00
13	8.89	15.40	152.00
15	5.65	15.51	152.00
17	2.75	15.61	152.00
19	-0.00	15.66	152.00
21	-2.63	14.93	152.00
23	-4.81	13.22	152.00
25	-6.18	10.70	152.00
27	-6.39	7.62	152.00
29	-5.37	4.51	152.00
31	-4.68	2.70	152.00
33	-4.23	1.54	152.00
35	-3.91	.69	152.00
37	-3.64	0.00	152.00
39	-3.41	-.60	152.00
41	-3.20	-1.16	152.00
43	-2.98	-1.72	152.00
45	-2.75	-2.31	152.00
47	-2.50	-2.98	152.00
49	-2.19	-3.79	152.00
51	-1.77	-4.87	152.00
53	-1.12	-6.37	152.00
55	-0.00	-7.87	152.00
57	1.60	-9.10	152.00
59	3.58	-9.83	152.00
61	5.74	-9.95	152.00
63	8.26	-9.84	152.00
65	11.57	-9.70	152.00
67	16.45	-9.50	152.00
69	25.10	-9.14	152.00
71	48.10	-8.49	152.00
73	56.66	.01	152.00

2	55.03	4.82	152.00
4	49.63	13.30	152.00
6	31.32	14.61	152.00
8	21.35	14.96	152.00
10	15.18	15.17	152.00
12	10.74	15.33	152.00
14	7.21	15.45	152.00
16	4.17	15.56	152.00
18	1.37	15.66	152.00
20	-1.35	15.43	152.00
22	-3.80	14.19	152.00
24	-5.62	12.04	152.00
26	-6.45	9.22	152.00
28	-5.90	5.90	152.00
30	-4.98	3.49	152.00
32	-4.44	2.07	152.00
34	-4.06	1.09	152.00
36	-3.77	.33	152.00
38	-3.52	-.31	152.00
40	-3.30	-.88	152.00
42	-3.09	-1.44	152.00
44	-2.87	-2.01	152.00
46	-2.63	-2.63	152.00
48	-2.35	-3.36	152.00
50	-2.00	-4.28	152.00
52	-1.50	-5.59	152.00
54	-.62	-7.14	152.00
56	.75	-8.53	152.00
58	2.55	-9.53	152.00
60	4.65	-9.96	152.00
62	6.93	-9.90	152.00
64	9.78	-9.78	152.00
66	13.73	-9.61	152.00
68	20.05	-9.35	152.00
70	32.79	-8.79	152.00
72	55.50	-4.85	152.00

1	61.98	-0.00	156.00
3	58.41	10.30	156.00
5	41.10	14.95	156.00
7	26.30	15.19	156.00
9	18.33	15.38	156.00
11	13.02	15.52	156.00
13	9.01	15.61	156.00
15	5.71	15.70	156.00
17	2.78	15.77	156.00

2	60.08	5.26	156.00
4	52.58	14.08	156.00
6	32.25	15.04	156.00
8	21.84	15.30	156.00
10	15.46	15.46	156.00
12	10.90	15.57	156.00
14	7.30	15.66	156.00
16	4.21	15.73	156.00
18	1.38	15.80	156.00

19	0.00	15.67	156.00	20	-1.34	15.27	156.00
21	-2.57	14.61	156.00	22	-3.67	13.69	156.00
23	-4.57	12.55	156.00	24	-5.23	11.22	156.00
25	-5.60	9.70	156.00	26	-5.62	8.03	156.00
27	-5.12	6.10	156.00	28	-4.52	4.52	156.00
29	-4.11	3.45	156.00	30	-3.81	2.67	156.00
31	-3.58	2.07	156.00	32	-3.39	1.58	156.00
33	-3.24	1.18	156.00	34	-3.10	.83	156.00
35	-2.99	.53	156.00	36	-2.88	.25	156.00
37	-2.79	0.00	156.00	38	-2.69	-.24	156.00
39	-2.61	-.46	156.00	40	-2.53	-.68	156.00
41	-2.44	-.89	156.00	42	-2.36	-1.10	156.00
43	-2.28	-1.32	156.00	44	-2.19	-1.54	156.00
45	-2.11	-1.77	156.00	46	-2.01	-2.01	156.00
47	-1.91	-2.28	156.00	48	-1.80	-2.57	156.00
49	-1.67	-2.90	156.00	50	-1.53	-3.28	156.00
51	-1.36	-3.72	156.00	52	-1.14	-4.27	156.00
53	-.88	-4.97	156.00	54	-.51	-5.87	156.00
55	-0.00	-6.79	156.00	56	.67	-7.64	156.00
57	1.48	-8.40	156.00	58	2.42	-9.03	156.00
59	3.46	-9.50	156.00	60	4.57	-9.81	156.00
61	5.73	-9.91	156.00	62	6.93	-9.89	156.00
63	8.26	-9.84	156.00	64	9.80	-9.79	156.00
65	11.60	-9.73	156.00	66	13.80	-9.66	156.00
67	16.58	-9.57	156.00	68	20.27	-9.45	156.00
69	25.49	-9.28	156.00	70	33.56	-8.99	156.00
71	49.72	-8.77	156.00	72	60.28	-5.27	156.00
73	61.98	-0.00	156.00				

Coordinates of the centre of the head of the prosthesis (x,y,z)

40.70 3.98 161.00

APPENDIX 2. FEM-model. Programs PROEM and COSCF

Program PROEM

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C MESH GENERATOR FOR FEM STRESS ANALYSIS WITH PAPEC OF EMBEDDED
C PROSTHESIS WITH SMOOTH SHAPE
C
  PROGRAM PROEM
  CHARACTER NAME*10
  INTEGER STEP,L1,L2,CCD,UEB,NPPS,NSCH
  INTEGER I,J,K,ISHOR,IDIV,NSTEP,NSEMB,NBLOCK
  INTEGER NRNOD,NSTEM,NTOP,NEMBE,LEV,LESS
  REAL FORCE
  DIMENSION POINTS(30,73,3),RKMP(3),CKMP(3),SKMP(73,3)
  DIMENSION NSCN(5),CMID(30,3),GEM(6,10,3)
C
C NAME: NEAME OF THE FILE CONTAINING THE GEOMETRY OF THE PROSTHESIS
C STEP, L1, L2, UEB: PARAMETERS
C CCD: NECK ANGLE
C NSCH: NUMBER OF STEPS (CONTOURS) OF THE PROSTHESIS
C NPPS: NUMBER OF POINTS PER STEP (CONTOUR)
C I,J,K: POINTERS
C ISHOR: NUMBER OF POINTS PER CONTOUR FOR FEM MODEL
C IDIV: NUMBER OF DIVISIONS OF THE SECTION ITO ELEMENTS
C   IDIV=2 => ONE LAYER OF BRICK + ONE LAYER OF WEDGE ELEMENTS
C   IDIV=3 => TWO LAYERS OF BRICK + ONE LAYER OF WEDGE ELEMENTS
C NSTEP: POINTER FOR NUMBER OF STEPS
C NSEMB: NUMBER OF STEPS IN THE EMBEDDING
C LEV: NUMBER OF THE CONTOUR AT EMBEDDING LEVEL
C LESS: LAST CONTOUR TO BE MEDELLED INSTEPAD OF THE BASIC-CONTOUR
C NRNOD: TOTAL NUMBER OF NODES AND POINTER FOR THE NODE NUMBERS
C NSTEM: NUMBER OF THE LAST NODE OF THE STEM
C NTOP: NUMBER OF THE LAST NODE OF THE TOP (NECK)
C NEMBE: NUMBER OF THE LAST NODE OF THE EMBEDDING
C NBLOCK: POINTER ON NUMBER OF PAFBLOCKS
C FORCE: VALUE OF THE LOAD IN DIN-TEST
C POINTS: ARRAY CONTAINING THE COORDINATES OF THE GEOMETRY POINTS
C NSCN(4): NUMBER OF THE BASIC STEP
C NSCN(5): NUMBER OF THE LAST 8MM-PART
C RKMP: ARRAY CONTAINING THE MIDPOINT OF PROSTHESIS HEAD
C CKMP: ARRAY CONTAINING POINT ON THE NECK AXIS 25MM FROM RKMP
C SKMP: ARRAY CONTAINING POINTS OF THE NECK (FOUR IN EACH LEVEL)
C CMID: ARRAY CONTAINING THE COORDINATES OF THE CENTRE POINT OF
C   EACH CONTOUR (CALCULATED IN SUBROUTINE SECT)
C
C
C READ INPUT FILE
C
  CALL READAT(POINTS,NSCN,RKMP,STEP,L1,L2,UEB,CCD,NSCH,NPPS,NAME)
C
C CALCULATE CENTRE POINTS AN REDEFINE COORDINATES OF THE POINTS
C OF THE CONTOURS
C
  CALL SECT(POINTS,NPPS,NSCN(4),CMID)
C
C SET VALUES OF PARAMETERS
C
  J=0
  LESS=4
C LESS IS ALSO USED IN SUBROUTINE DEFEMBE
```

```
NSCN(4)=NSCN(4)-LESS
ISHOR=24
IDIV=2
FORCE=-1.0
C
C OPEN OUTPUT FILE
C
  OPEN(12,FILE='PROEM.DAT')
C
C WRITE TITLE
C
  WRITE(12,1)'TITLE FEM-APPROX PROT ',NAME
C
C WRITE CONTROL MODULE
C
  WRITE(12,1)'CONTROL'
  WRITE(12,1)'FULL.CONTROL'
  WRITE(12,1)'REDUCED OUTPUT'
  WRITE(12,1)'STRESS'
  WRITE(12,1)'PHASE=1,2,4,6,7,9'
  WRITE(12,1)'CONTROL.END'
C
C WRITE NODES
C
  WRITE(12,1)'NODES'
  WRITE(12,1)'NODE.NUMBER X Y Z '
1  FORMAT(80A)
C
C DEFINE NODES OF THE STEM
C
  CALL DEFSTE(POINTS,NSCN(4),NSCN(5),NPPS,ISHOR,CMID,J,NRNOD,NSTEM
+,NSTEP,IDIV)
C
C DEFINE NODES OF THE NECK (TOP)
C
  CALL DEFTOP(RKMP,CKMP,SKMP,NPPS,CCD,NRNOD,ISHOR,J,IDIV,NTOP)
C
C DEFINE NODES OF THE EMBEDDING
C
  CALL DEFEMB(POINTS,NSCN(4),NSCN(5),NPPS,ISHOR,CMID,
+J,NRNOD,NEMBE,NSEMB,LEV,IDIV,LESS)
C
C WRITE PAFBLOCKS (ELEMENTS)
C
  WRITE(12,1)'PAFBLOCKS'
  WRITE(12,1)'BLOCK.NUMBER TYPE ELEMENT.TYPE PROPERTIES
+ N1 N2 N5 TOPOLOGY'
  NBLOCK=0
C
C DEFINE PAFBLOCKS OF THE STEM AND THE NECK
C
  CALL PROTE(NBLOCK,NSTEM,NSTEP,NRNOD,ISHOR,IDIV)
C
C DEFINE PAFBLOCKS OF THE EMBEDDING
C
  CALL EMBE(NBLOCK,NEMBE,NSEMB,NRNOD,ISHOR,NTOP,IDIV)
C
C DEFINE MESH AND REFERENCE SPACING LIST
C
  WRITE(12,1)'MESH'
  WRITE(12,1)'REFERENCE SPACING.LIST'
  WRITE(12,1)'1 1'
```



```
DIMENSION RKMP(3)
INTEGER STEP,NSCH,NPPS,CCD,L1,L2,UEB,I,J,K
C
C THIS SUBROUTINE READS THE INPUT FILE
C
PRINT*,'ENTER THE NAME OF THE INPUT-FILE NAME '
PRINT*,'                               (UP TO 10 CHARACTERS)'
READ(*,7) NAME
7  FORMAT(A10)
OPEN(10,FILE=NAME,STATUS='OLD')
C
C READ PARAMETERS
C
READ(10,*) STEP
DO 100 I=1,5
  READ(10,*) NSCN(I)
100 CONTINUE
READ(10,*) NSCH
READ(10,*) NPPS
READ(10,*) CCD
READ(10,*) L1
READ(10,*) L2
READ(10,*) UEB
C
C READ THE COORDINATES OF POINTS
C
DO 110 I=1,NSCH
  DO 120 J=1,NPPS
    DO 130 K=1,3
      READ(10,*) POINTS(I,J,K)
130  CONTINUE
120  CONTINUE
110  CONTINUE
C
C READ THE COORDINATES OF THE CENTRE OF THE HEAD
C
DO 140 I=1,3
  READ(10,*) RKMP(I)
140 CONTINUE
C
PRINT*,'DATA SUCESSFULLY READ'
C
CLOSE(10)
RETURN
END
C
C END READAT
C
C
C
SUBROUTINE SECT(POINTS,NPPS,NSCN4,CMID)
INTEGER I,J,K,L,OFFSET,NSCN4
REAL PI,X,X1,X2,Y,Y1,Y2,A1,A2,B1,B2,D1,D2,W,ALPHA
DIMENSION POINTS(30,73,3),SEC(0:72,3),CMID(30,3),WEIG(73)
C
C THIS SUBROUTINE CALCULATES 'CENTRES' OF THE SECTIONS
C AND NEW POINTS AROUND THESE
C
C CMID: COORDINATES OF THE CENTRE POINTS
C
DO 100 I=1,NSCN4
  DO 110 J=1,NPPS
```

```
DO 120 K=1,3
  SEC(J-1,K)=POINTS(I,J,K)
120 CONTINUE
110 CONTINUE
C
C COMPUTING WEIGHTS
C
  W=0.0
  DO 130 J=0,NPPS-1
    D1=SQRT((SEC(J,1)-SEC(MOD(J+1,NPPS-1),1))**2+(SEC(J,2)-
+ SEC(MOD(J+1,NPPS-1),2))**2)
    D2=SQRT((SEC(J,1)-SEC(MOD(J+NPPS-2,NPPS-1),1))**2+(SEC(J,2)-
+ SEC(MOD(J+NPPS-2,NPPS-1),2))**2)
    WEIG(J+1)=(D1+D2)/2
    W=W+WEIG(J+1)
130 CONTINUE
C
C CALCULATE THE COORDINATES OF THE CENTRE POINTS
C
  DO 140 K=1,3
    CMID(I,K)=0.0
140 CONTINUE
  DO 145 J=1,NPPS
    CMID(I,1)=WEIG(J)*SEC(J-1,1)+CMID(I,1)
    CMID(I,2)=WEIG(J)*SEC(J-1,2)+CMID(I,2)
145 CONTINUE
  CMID(I,1)=CMID(I,1)/W
  CMID(I,2)=CMID(I,2)/W
  CMID(I,3)=SEC(1,3)
C
C FIND NEW POINTS ON THE CONTOUR IN ALPHA DEGREES STEPS
C AROUND CMIDS STARTING WITH THE POINT NO. 1
C
  PI=4*ATAN(1.0)
  ALPHA=2*PI/(NPPS-1)
  SEC(0,1)=POINTS(I,1,1)
  SEC(0,2)=POINTS(I,1,2)
  K=1
  DO 210 J=0,NPPS-2
    X1=SEC(J,1)-CMID(I,1)
    Y1=SEC(J,2)-CMID(I,2)
    D1=SQRT(X1**2+Y1**2)
99  X2=POINTS(I,MOD(K,NPPS)+1,1)-CMID(I,1)
    Y2=POINTS(I,MOD(K,NPPS)+1,2)-CMID(I,2)
    D2=SQRT(X2**2+Y2**2)
    IF(((X1*X2+Y1*Y2)/(D1*D2)).GT.(COS(ALPHA)))THEN
      K=K+1
      GOTO 99
    END IF
    X=X1*COS(ALPHA)-Y1*SIN(ALPHA)
    Y=X1*SIN(ALPHA)+Y1*COS(ALPHA)
    X=X+CMID(I,1)
    Y=Y+CMID(I,2)
C
  IF((ABS(X-CMID(I,1)).GT.1E-12))THEN
    A1=(Y-CMID(I,2))/(X-CMID(I,1))
    B1=Y-A1*X
    IF((ABS(POINTS(I,MOD(K,NPPS)+1,1)-SEC(J,1)).GT.1E-12))THEN
      A2=(POINTS(I,MOD(K,NPPS)+1,2)-SEC(J,2))/(POINTS(I,MOD(K,NPPS)+
+ 1,1)-SEC(J,1))
      B2=POINTS(I,MOD(K,NPPS)+1,2)-A2*POINTS(I,MOD(K,NPPS)+1,1)
      SEC(J+1,1)=(B2-B1)/(A1-A2)
```

```

SEC(J+1,2)=A1*SEC(J+1,1)+B1
ELSE
  A2=0.0
  B2=POINTS(I,MOD(K,NPPS)+1,2)
  SEC(J+1,1)=(B2-B1)/A1
  SEC(J+1,2)=B2
END IF
ELSE
  A1=0.0
  B1=Y
  IF((ABS(POINTS(I,MOD(K,NPPS)+1,1)-SEC(J,1)).GT.1E-12)) THEN
A2=(POINTS(I,MOD(K,NPPS)+1,2)-SEC(J,2))/(POINTS(I,MOD(K,NPPS)+
+ 1,1)-SEC(J,1))
  B2=POINTS(I,MOD(K,NPPS)+1,2)-A2*POINTS(I,MOD(K,NPPS)+1,1)
  SEC(J+1,1)=(B1-B2)/A2
  SEC(J+1,2)=B1
ELSE
  SEC(J+1,1)=POINTS(I,MOD(K,NPPS)+1,1)
  SEC(J+1,2)=POINTS(I,MOD(K,NPPS)+1,2)
END IF
END IF
210 CONTINUE
C
C CALCULATE OFFSET, I.E., THE NUMBER OF THE POINT, THE Y COORDINATE
C OF WHICH IS CLOSEST OF THE Y-COORDINATE OF THE CENTRE POINT
C
  L=IFIX((PI/4/ALPHA))
  OFFSET=0
  D1=ABS(CMID(I,2)-SEC(0,2))
  DO 205 J=-L,L
    Y=SEC(MOD(NPPS+L,NPPS),2)
    D2=ABS(CMID(I,2)-Y)
    IF(D2.LT.D1) THEN
      OFFSET=MOD(NPPS+L,NPPS)
    ENDIF
205 CONTINUE
C
C WRITE THE COORDINATES OF NEW POINTS
C
  DO 220 J=1,NPPS
    DO 230 K=1,2
      POINTS(I,J,K)=SEC(MOD(J-1+OFFSET,NPPS),K)
230 CONTINUE
220 CONTINUE
100 CONTINUE
C
  RETURN
END
C
C END SECT
C
C
C
C
  SUBROUTINE DEFSTE(POINTS,NSCN4,NSCN5,NPPS,ISHOR,CMID,J
+,NRNOD,NSTEM,NSTEP,IDIV)
  INTEGER NSCN4,NSCN5,ISHOR,NPPS,J,NRNOD,NSTEM
  INTEGER I,K,L,M,NSTEP,IDIV,INT
  REAL PI
  DIMENSION POINTS(30,73,3),CMID(30,3)
  DIMENSION ARRAY(3)
C
C THIS SUBROUTINE DEFINES NODES OF THE STEM.

```

```
C
  PI=ATAN(1.0)*4
  INT=(NPPS-1)/ISHOR
  NRNOD=0
C
C INT IS THE INTERVAL USED IN ORDER TO PICK OUT THE POINTS
C
C DEFINE ZERO LEVEL
C
  WRITE(12,2)'C DEFINE POINTS ON ZERO LEVEL'
  DO 100 I=0, IDIV-1
    WRITE(12,2)'C STEM SECTION'
    DO 110 K=0, ISHOR-1
      ARRAY(1)=POINTS(1, MOD(K*INT+J, NPPS-2)+1, 1)
      ARRAY(2)=POINTS(1, MOD(K*INT+J, NPPS-2)+1, 2)
      ARRAY(3)=0.0
      ARRAY(1)=ARRAY(1)-(ARRAY(1)-CMID(1,1))/IDIV*I
      ARRAY(2)=ARRAY(2)-(ARRAY(2)-CMID(1,2))/IDIV*I
      NRNOD=NRNOD+1
      WRITE(12,1)NRNOD, (ARRAY(L), L=1, 3)
1     FORMAT(15, 1X, E15.7, 1X, E15.7, 1X, E15.7)
110   CONTINUE
2     FORMAT(80A)
100   CONTINUE
C
  NRNOD=NRNOD+1
  WRITE(12,2)'C MIDPOINT ZERO LEVEL'
  WRITE(12,1)NRNOD, CMID(1,1), CMID(1,2), 0.0
C
  WRITE(12,2)'C BETWEEN SECTIONS AT Z=4 MM'
  DO 111 K=0, ISHOR-1
    IF((MOD(K,2)).EQ.1)GOTO 111
    ARRAY(1)=POINTS(1, MOD(K*INT+J, NPPS-2)+1, 1)
    ARRAY(2)=POINTS(1, MOD(K*INT+J, NPPS-2)+1, 2)
    ARRAY(1)=(ARRAY(1)+POINTS(2, MOD(K*INT+J, NPPS-2)+1, 1))/2
    ARRAY(2)=(ARRAY(2)+POINTS(2, MOD(K*INT+J, NPPS-2)+1, 2))/2
    ARRAY(3)=4.0
    NRNOD=NRNOD+1
    WRITE(12,1)NRNOD, (ARRAY(L), L=1, 3)
111   CONTINUE
C
C DEFINE REST OF THE STEM
C
  NSTEP=0
  DO 115 M=1, NSCN4
    IF(M.GT.NSCN5)THEN
      IF(MOD(M-NSCN5, 2).GT.0)GOTO 114
    ENDIF
    NSTEP=NSTEP+1
  DO 120 I=0, IDIV-1
    WRITE(12,2)'C STEM SECTION ', NSTEP*8, ' MM'
    DO 130 K=0, ISHOR-1
      ARRAY(1)=POINTS(M, MOD(K*INT+J, NPPS-2)+1, 1)
      ARRAY(2)=POINTS(M, MOD(K*INT+J, NPPS-2)+1, 2)
      ARRAY(3)=POINTS(M, 1, 3)
      ARRAY(1)=ARRAY(1)-(ARRAY(1)-CMID(M,1))/IDIV*I
      ARRAY(2)=ARRAY(2)-(ARRAY(2)-CMID(M,2))/IDIV*I
      NRNOD=NRNOD+1
      WRITE(12,1)NRNOD, (ARRAY(L), L=1, 3)
130   CONTINUE
120   CONTINUE
C
```

```
NRNOD=NRNOD+1
WRITE(12,2)'C MIDPOINT'
WRITE(12,1)NRNOD,CMID(M,1),CMID(M,2),CMID(M,3)
C
WRITE(12,2)'C BETWEEN SECTIONS', NSTEP*8+4,' MM'
DO 125 K=0,ISHOR-1
  IF(((MOD(K,2)).EQ.1).OR.(M.GE.(NSCN4-1)))GOTO 125
  ARRAY(1)=POINTS(M,MOD(K*INT+J,NPPS-2)+1,1)
  ARRAY(2)=POINTS(M,MOD(K*INT+J,NPPS-2)+1,2)
  ARRAY(1)=(ARRAY(1)+POINTS(M+1,MOD(K*INT+J,NPPS-2)+1,1))/2
  ARRAY(2)=(ARRAY(2)+POINTS(M+1,MOD(K*INT+J,NPPS-2)+1,2))/2
  ARRAY(3)=POINTS(M,1,3)+4.0
  NRNOD=NRNOD+1
  WRITE(12,1)NRNOD,(ARRAY(L),L=1,3)
125  CONTINUE
114  CONTINUE
115  CONTINUE
C
  WRITE(12,2)'C END STEM'
  NSTEM=NRNOD
C
  RETURN
  END
C
C END DEFSTE
C
C
C
C
  SUBROUTINE DEFTOP(RKMP,CKMP,SKMP,NPPS,CCD,NRNOD,ISHOR,JJ,
+IDIV,NTOP)
  INTEGER NPPS,CCD,NRNOD,ISHOR,IDIV,NTOP
  INTEGER I,J,JJ,K,L,LEN
  REAL PI,R
  DIMENSION RKMP(3),CKMP(3),SKMP(73,3)
C
C THIS SUBROUTINE DEFINES NODES OF THE NECK PART.
C THE NECK PART IS A SIMPLIFIED STANDARD. IN ORDER TO HAVE A
C SIMPLER MODEL, THE NECK IS SHORTENED ALONG THE NECK AXIS BY
C THE VALUE OF LEN.
C HERE:
C LEN= 25MM
C LEN IS ALSO USED IN SUBROUTINE DEFLOAD IN ORDER TO DEFINE
C THE LOADS
C THE DIAMETER OF THE NECK IS SET TO 2R= 16 MM
C
  LEN=25
  R=8
  J=0
C
C CALCULATE THE CENTRE NODE ALONG THE NECK AXIS AND BY
C LEN DISTANT FROM THE CENTRE OF THE HEAD OF THE PROSTHESIS
C
  PI=4*ATAN(1.0)
  IF(RKMP(1).GT.0.0)THEN
    CKMP(1)=RKMP(1)-LEN*COS((CCD-90)*PI/180)
  ELSE
    CKMP(1)=RKMP(1)+LEN*COS((CCD-90)*PI/180)
  END IF
  CKMP(2)=RKMP(2)
  CKMP(3)=RKMP(3)-LEN*SIN((CCD-90)*PI/180)
C
C CALCULATE NODES AROUND CKMP
```

```
C
WRITE(12,2)'C DEFINE TOP PART'
DO 90 K=0, IDIV-1
  WRITE(12,2)'C TOP SECTION'
  DO 100 I=0, ISHOR-1
    SKMP(I+1,1)=CKMP(1)+R*COS(I*2*PI/ISHOR+J*2*PI/(NPPS-1))
    SKMP(I+1,2)=CKMP(2)+R*SIN(I*2*PI/ISHOR+J*2*PI/(NPPS-1))
    SKMP(I+1,3)=CKMP(3)
    SKMP(I+1,1)=SKMP(I+1,1)-(SKMP(I+1,1)-CKMP(1))/IDIV*K
    SKMP(I+1,2)=SKMP(I+1,2)-(SKMP(I+1,2)-CKMP(2))/IDIV*K
    NRNOD=NRNOD+1
    WRITE(12,1)NRNOD,(SKMP(I+1,L),L=1,3)
1   FORMAT(I5,3(1X,E15.7))
100  CONTINUE
2   FORMAT(80A)
90   CONTINUE
WRITE(12,2)'C MIDPOINT TOP'
C
NRNOD=NRNOD+1
WRITE(12,1)NRNOD,(CKMP(L),L=1,3)
C
WRITE(12,2)'C END TOP'
NTOP=NRNOD
C
RETURN
END
C
C END DEFTOP
C
C
C
SUBROUTINE DEFEMB(POINTS,NSCN4,NSCN5,NPPS,ISHOR,CMID,J
+,NRNOD,NEMBE,NSEMB,LEV,IDIV,LESS)
INTEGER NSCN4,NSCN5,ISHOR,NPPS,J,NRNOD,NEMBE,LESS,IDIV
INTEGER I,K,L,M,LEV,HIGH,NSEMB,INT
REAL PI,DICK,ALPHA
DIMENSION POINTS(30,73,3),CMID(30,3)
DIMENSION ARRAY(3)
C
C THIS SUBROUTINE DEFINES NODES OF THE EMBEDDING.
C
PI=ATAN(1.0)*4
ALPHA=2*PI/(NPPS-1)
INT=(NPPS-1)/ISHOR
C
C INT IS THE INTERVAL REQUIRED FOR PICKING OUT THE POINTS
C
C DICK IS THE THICKNESS OF THE EMBEDDING
C
DICK=20
C
C CALCULATE THE EMBEDDING LEVEL: LEV
C
HIGH=NSCN5*8+(NSCN4+LESS-NSCN5)*4-50
IF((NSCN5*8).GT.HIGH)THEN
  LEV=HIGH/8-1
ELSE
  LEV=NSCN5+(HIGH-NSCN5*8)/4-1
END IF
LEV=LEV+2
C
C DEFINE LOWER PART OF THE EMBEDDING AROUND THE TIP OF THE PROSTHESIS
```

```
C
WRITE(12,2)'C DEFINE DISTAL PART OF THE EMBEDDING'
2  FORMAT(80A)
DO 90 M=0,1
  WRITE(12,2)'C DISTAL SECTION EMBEDDING SURFACE'
  DO 110 K=0,ISHOR-1
    ARRAY(3)=0.0+(M-1)*8
    ARRAY(1)=DICK*COS(MOD(K*INT+J,NPPS-2)*ALPHA)
    ARRAY(2)=DICK*SIN(MOD(K*INT+J,NPPS-2)*ALPHA)
    NRNOD=NRNOD+1
    WRITE(12,1)NRNOD,(ARRAY(L),L=1,3)
1  FORMAT(15,1X,E15.7,1X,E15.7,1X,E15.7)
110 CONTINUE
DO 111 I=0,IDIV-1
  WRITE(12,2)'C EMBEDDING SECTION'
  DO 112 K=0,ISHOR-1
    ARRAY(1)=POINTS(1,MOD(K*INT+J,NPPS-2)+1,1)
    ARRAY(2)=POINTS(1,MOD(K*INT+J,NPPS-2)+1,2)
    ARRAY(3)=0.0+(M-1)*8
    ARRAY(1)=ARRAY(1)-(ARRAY(1)-CMID(1,1))/IDIV*I
    ARRAY(2)=ARRAY(2)-(ARRAY(2)-CMID(1,2))/IDIV*I
    NRNOD=NRNOD+1
    WRITE(12,1)NRNOD,(ARRAY(L),L=1,3)
112 CONTINUE
111 CONTINUE
  WRITE(12,2)'C MIDPOINT'
  NRNOD=NRNOD+1
  WRITE(12,1)NRNOD,CMID(1,1),CMID(1,2),ARRAY(3)
90 CONTINUE
C
C
C DEFINE ZERO LEVEL
C
DO 120 I=0,1
  WRITE(12,2)'C EMBEDDING SECTION '
  DO 130 K=0,ISHOR-1
    ARRAY(1)=POINTS(1,MOD(K*INT+J,NPPS-2)+1,1)
    ARRAY(2)=POINTS(1,MOD(K*INT+J,NPPS-2)+1,2)
    ARRAY(3)=0.0
    ARRAY(1)=ARRAY(1)*I+DICK*COS(MOD(K*INT+J,NPPS-2)*ALPHA)*(1-I)
    ARRAY(2)=ARRAY(2)*I+DICK*SIN(MOD(K*INT+J,NPPS-2)*ALPHA)*(1-I)
    NRNOD=NRNOD+1
    WRITE(12,1)NRNOD,(ARRAY(L),L=1,3)
130 CONTINUE
120 CONTINUE
  WRITE(12,2)'C BETWEEN'
  DO 135 K=0,ISHOR-1
    IF((MOD(K,2)).EQ.1) GOTO 135
    ARRAY(1)=POINTS(1,MOD(K*INT+J,NPPS-2)+1,1)
    ARRAY(2)=POINTS(1,MOD(K*INT+J,NPPS-2)+1,2)
    ARRAY(1)=(ARRAY(1)+POINTS(2,MOD(K*INT+J,NPPS-2)+1,1))/2
    ARRAY(2)=(ARRAY(2)+POINTS(2,MOD(K*INT+J,NPPS-2)+1,2))/2
    ARRAY(3)=4.0
    NRNOD=NRNOD+1
    WRITE(12,1)NRNOD,(ARRAY(L),L=1,3)
135 CONTINUE
C
C
C DEFINE REMAINING NODES OF THE EMBEDDING
C
NSEMB=1
DO 115 M=1,LEV
```



```
N1=1
N2=1
N5=1
DO 110 K=1,NSTEP+1
  WRITE(12,2)'C STEM '
2  FORMAT(80A)
  MID=K*(IDIV*ISHOR+1)+(K-1)*ISHOR/2
  INT=(K-1)*(IDIV*ISHOR+ISHOR/2+1)
  IF(K.EQ.(NSTEP+1))THEN
    WRITE(12,2)'C '
C
C DIVISION OF THE NECK PART
C
  N5=4
  END IF
  DO 120 J=1,IDIV
    IF(J.EQ.IDIV)THEN
      TYP=4
C
C WEDGE ELEMENT
C
      ETYP=37210
      DO 130 I=0,ISHOR/2-1
        EL(1)=MID
        EL(2)=INT+1+I*2
        EL(3)=INT+1+MOD((I+1)*2,ISHOR)
        EL(4)=EL(1)+IDIV*ISHOR+1+ISHOR/2
        EL(5)=EL(2)+IDIV*ISHOR+1+ISHOR/2
        EL(6)=EL(3)+IDIV*ISHOR+1+ISHOR/2
        EL(7)=0
        EL(8)=EL(2)+1
        EL(9)=0
        EL(10)=0
        EL(11)=0
        EL(12)=0
        EL(13)=0
        EL(14)=EL(8)+IDIV*ISHOR+1+ISHOR/2
        EL(15)=0
        IF(K.EQ.(NSTEP+1))THEN
          EL(4)=EL(4)-ISHOR/2
          EL(5)=EL(5)-ISHOR/2
          EL(6)=EL(6)-ISHOR/2
          EL(14)=EL(14)-ISHOR/2
        END IF
        NBLOCK=NBLOCK+1
        WRITE(12,1)NBLOCK,TYP,ETYP,PROP,N1,N2,N5,(EL(L),L=1,15)
130  CONTINUE
      ELSE
        WRITE(12,2)'C '
        TYP=1
C
C BRICK ELEMENT
C
      ETYP=37110
      DO 140 I=0,ISHOR/2-1
        EL(1)=1+I*2+INT
        EL(2)=INT+1+MOD((I+1)*2,ISHOR)
        EL(3)=EL(1)+IDIV*ISHOR+1+ISHOR/2
        EL(4)=EL(2)+IDIV*ISHOR+1+ISHOR/2
        EL(5)=EL(1)+ISHOR
        EL(6)=EL(2)+ISHOR
        EL(7)=EL(5)+IDIV*ISHOR+1+ISHOR/2
```

```
EL(8)=EL(6)+IDIV*ISHOR+1+ISHOR/2
EL(9)=EL(1)+1
EL(12)=EL(3)+1
EL(17)=EL(5)+1
EL(20)=EL(7)+1
EL(10)=0
EL(11)=0
EL(13)=0
EL(14)=0
EL(15)=0
EL(16)=0
EL(18)=0
EL(19)=0
IF(J.EQ.1)THEN
  EL(10)=MID+I+1
  EL(11)=MID+MOD(I+1,ISHOR/2)+1
ENDIF
IF(K.EQ.(NSTEP+1))THEN
  EL(3)=EL(3)-ISHOR/2
  EL(4)=EL(4)-ISHOR/2
  EL(7)=EL(7)-ISHOR/2
  EL(8)=EL(8)-ISHOR/2
  EL(10)=0
  EL(11)=0
  EL(12)=EL(12)-ISHOR/2
  EL(20)=EL(20)-ISHOR/2
END IF
NBLOCK=NBLOCK+1
WRITE(12,1)NBLOCK,TYP,ETYP,PROP,N1,N2,N5,(EL(L),L=1,20)
1  FORMAT(7(I6,1X)/*',10(I5,1X)/*',10(I5,1X))
140 CONTINUE
END IF
  INT=INT+ISHOR
120 CONTINUE
110 CONTINUE
C
  RETURN
  END
C
C
C END PROTE
C
C
C
C
SUBROUTINE EMBE(NBLOCK,NEMBE,NSEMB,NRNOD,ISHOR,NTOP,IDIV)
INTEGER I,J,K,L,NBLOCK,NEMBE,NSEMB,NRNOD,ISHOR,NTOP,IDIV
INTEGER INT,MID,TYP,N1,N2,N5,PROP,EL
INTEGER*4 ETYP
DIMENSION EL(20)
C
C THIS SUBROUTINE DEFINES PAFBLOCKS (ELEMENTS) OF THE EMBEDDING
C
  DO 100 I=1,20
    EL(I)=0
100 CONTINUE
C
C PROPERTY 21 = PMMA
C
  PROP=21
  N1=1
C
C N2=2 OR N2 =1. IF THE DISTAL PART OF
```

```
C THE EMBEDDING (JUST BELOW THE STEM) IS MODELLED, N2=1. IF
C THE EMBEDDING AROUND THE STEM IS MODELLED, N2=2
C
      N5=1
C
      WRITE(12,2)'C EMBEDDING SECTION'
2      FORMAT(80A)
      MID=ISHOR*(IDIV+1)+NTOP+1
      INT=NTOP
      DO 77 J=1, IDIV+1
      WRITE(12,2)'C EMBEDDING'
      IF(J.EQ.(IDIV+1)) THEN
        TYP=4
        N2=1
        ETYP=37210
        DO 78 I=0, ISHOR/2-1
          EL(1)=MID
          EL(2)=INT+1+I*2
          EL(3)=INT+1+MOD((I+1)*2, ISHOR)
          EL(4)=EL(1)+(IDIV+1)*ISHOR+1
          EL(5)=EL(2)+(IDIV+1)*ISHOR+1
          EL(6)=EL(3)+(IDIV+1)*ISHOR+1
          EL(7)=0
          EL(8)=EL(2)+1
          EL(9)=0
          EL(10)=0
          EL(11)=0
          EL(12)=0
          EL(13)=0
          EL(14)=EL(8)+(IDIV+1)*ISHOR+1
          EL(15)=0
          NBLOCK=NBLOCK+1
78      WRITE(12,1)NBLOCK, TYP, ETYP, PROP, N1, N2, N5, (EL(L), L=1, 15)
        CONTINUE
        ELSE
          TYP=1
          N2=2
          ETYP=37110
          DO 79 I=0, ISHOR/2-1
            EL(1)=1+I*2+INT
            EL(2)=INT+1+MOD((I+1)*2, ISHOR)
            EL(3)=EL(1)+(IDIV+1)*ISHOR+1
            EL(4)=EL(2)+(IDIV+1)*ISHOR+1
            EL(5)=EL(1)+ISHOR
            EL(6)=EL(2)+ISHOR
            EL(7)=EL(5)+(IDIV+1)*ISHOR+1
            EL(8)=EL(6)+(IDIV+1)*ISHOR+1
            EL(9)=EL(1)+1
            EL(12)=EL(3)+1
            EL(17)=EL(5)+1
            EL(20)=EL(7)+1
            EL(10)=0
            EL(11)=0
            EL(13)=0
            EL(14)=0
            EL(15)=0
            EL(16)=0
            EL(18)=0
            EL(19)=0
            NBLOCK=NBLOCK+1
1      WRITE(12,1)NBLOCK, TYP, ETYP, PROP, N1, N2, N5, (EL(L), L=1, 20)
      FORMAT(7(I6,1X)/* ',10(I5,1X)/* ',10(I5,1X))
```

```
79  CONTINUE
    END IF
    INT=INT+ISHOR
77  CONTINUE
C
DO 110 K=1,NSEMB-1
  WRITE(12,2)'C EMBEDDING SECTION'
  TYP=1
  N2=2
  ETYP=37110
  INT=NTOP+2*ISHOR*(IDIV+1)+2+(K-1)*(2*ISHOR+ISHOR/2)
DO 140 I=0,ISHOR/2-1
  EL(1)=1+I*2+INT
  EL(2)=INT+1+MOD((I+1)*2,ISHOR)
  EL(3)=EL(1)+2*ISHOR+ISHOR/2
  EL(4)=EL(2)+2*ISHOR+ISHOR/2
  EL(5)=EL(1)+ISHOR
  EL(6)=EL(2)+ISHOR
  EL(7)=EL(5)+2*ISHOR+ISHOR/2
  EL(8)=EL(6)+2*ISHOR+ISHOR/2
  EL(9)=EL(1)+1
  EL(12)=EL(3)+1
  EL(17)=EL(5)+1
  EL(20)=EL(7)+1
  EL(10)=0
  EL(11)=0
  EL(13)=0
  EL(14)=0
  EL(15)=0
  EL(16)=0
  EL(18)=INT+2*ISHOR+I+1
  EL(19)=INT+2*ISHOR+MOD(I+1,ISHOR/2)+1
NBLOCK=NBLOCK+1
WRITE(12,1)NBLOCK,TYP,ETYP,PROP,N1,N2,N5,(EL(L),L=1,20)
140 CONTINUE
110 CONTINUE
C
  RETURN
  END
```

C
C
C

```
SUBROUTINE BOND(NRNOD,NSTEM,ISHOR,IDIV,NTOP,NSEMB)
INTEGER NRNOD,NSTEM,I,J,NSEMB,ISHOR,IDIV,NTOP,L1,L2
```

C
C
C

THIS SUBROUTINE DEFINES CONSTRAINTS ON THE EMBEDDING

```
DO 100 I=NTOP+1,NTOP+ISHOR*(IDIV+1)+1
  WRITE(12,2)I,0
100 CONTINUE
  WRITE(12,1)'C'
  FORMAT(80A)
DO 105 I=NTOP+ISHOR*(IDIV+1)+2,NTOP+ISHOR*(IDIV+1)+1+ISHOR
  WRITE(12,2)I,0
105 CONTINUE
  WRITE(12,1)'C'
  L1=NTOP+2*ISHOR*(IDIV+1)+2
  L2=2*ISHOR+ISHOR/2
DO 110 I=1,NSEMB
  WRITE(12,1)'C'
```

```
      DO 120 J=L1+1,L1+ISHOR
      WRITE(12,2)J,0
2     FORMAT(2(I6,1X))
120   CONTINUE
      L1=L1+L2
110   CONTINUE
      RETURN
      END
```

```
C
C END BOND
C
C
C
C
```

```
      SUBROUTINE DEFLOD(FORCE,CCD,NTOP,ISHOR,IDIV,RKMP,CKMP)
      INTEGER NTOP,CCD,ISHOR,IDIV
      REAL FORCE,PI,LEN,M1,M2,FX,FZ
      DIMENSION RKMP(3),CKMP(3)
```

```
C
C THIS SUBROUTINE CALCULATES THE LOADS ON THE PROSTHESIS
C
C LEN IS THE AMOUNT BY WHICH THE NECK WAS SHORTENED
C IN THE MODEL. LEN WAS ALSO USED IN SUBROUTINE DEFTOP
C WHERE IT WAS SPECIFIED AS LEN=25 MM
C
```

```
      LEN=25
      PI=4*ATAN(1.0)
```

```
C
C (PI/18) = 10 DEGREES => TILT OF THE PROSTHESIS IN DIN-TEST
C
```

```
      FX=FORCE*SIN(PI/18)
      IF(RKMP(1).LT.0.0)THEN
      FX=-FX
      END IF
```

```
C
C CALCULATE LOADS WHICH RESULTS FROM THE SHORTENING OF THE NECK
C
```

```
      M1=FORCE*(RKMP(1)-CKMP(1))*COS(PI/18)
      M2=FORCE*(RKMP(3)-CKMP(3))*SIN(PI/18)
      M1=M1-M2
      FZ=M1/16
      WRITE(12,2)NTOP,3,FORCE*COS(PI/18)
      WRITE(12,2)NTOP,1,FX
      WRITE(12,2)NTOP-IDIV*ISHOR,3,FZ
      WRITE(12,2)NTOP-IDIV*ISHOR+ISHOR/2,3,-FZ
2     FORMAT(I6,1X,I6,1X,E15.7)
      RETURN
      END
```

```
C
C
C
C
```

```
      SUBROUTINE GAPS(NTOP,ISHOR,NSEMB,IDIV)
      INTEGER NTOP,ISHOR,NSEMB,IDIV
      INTEGER I,J,K,N1,N2
      K=0
```

```
C
C THIS SUBROUTINE SPECIFIES GAPS ELEMENTS ON THE EMBEDDING/
C PROSTHESIS INTERFACE AS AN OPTION TO THE CONTINUOUS
C INTERFACE CONDITIONS ASSUMED IN FEM-ANALYSIS.
```

```
C
C (COMMENTED OUT IN THE MAIN PROGRAM)
```

```
C
WRITE(12,1)'GAPS'
WRITE(12,1)'N1 N2 AXIS.NUMB DIRE TYPE'
1  FORMAT(80A)
   DO 100 I=1,NSEMB
     DO 110 J=1,ISHOR
       N1=NTOP+J+I*2*ISHOR+ISHOR+K
       N2=J+(I-1)*(IDIV*ISHOR+1)+K
       WRITE(12,2)N1,N2,1,1,1
2      FORMAT(5(I5,1X))
110   CONTINUE
      DO 120 J=1,ISHOR/2
        IF(I.EQ.NSEMB)GOTO 120
        N1=NTOP+(I+1)*2*ISHOR+J+K
        N2=I*(IDIV*ISHOR+1)+J+K
        WRITE(12,2)N1,N2,1,1,1
120   CONTINUE
      K=K+ISHOR/2
100   CONTINUE
      RETURN
      END
C
C END GAPS
```

Program COSCF

C THIS PROGRAMM ENABLES THE ESTIMATION OF THE STRESS CONCENTRATION
C FACTORS IN ONE STEP OF THE PROSTHESIS

C

```
PROGRAM COSCF
CHARACTER NAME*10
INTEGER STEP,L1,L2,CCD,UEB,NPPS,NSCH
INTEGER NST,ISHOR,NN0,NN1,NN2,NN3
REAL RAD,XP,YP,ZP
DIMENSION NSCN(5)
DIMENSION X(73,30),Y(73,30),Z(73,30)
DIMENSION XBAR(30),YBAR(30)
DIMENSION XT(73,30),YT(73,30)
```

C

```
C NST: NUMBER OF STEP TO MODELLED
C NN0,NN1,NN2,NN3: TOTAL NUMBER OF NODES IN EACH MODEL
C XP,YP,ZP: COORDINATES OF THE CENTRE OF THE HEAD OF THE PROSTHESIS
C RAD: VALUE OF THE TRANSITION RADIUS
C X,Y,Z: ARRAYS CONTAINING THE COORDINATES OF POINTS
C OF THE PROSTHESIS
C XBAR, YBAR: COORDINATES OF POINTS OF GRAVITY (CENTROIDS) OF
C EACH SECTION (CALCULATED IN SUBROUTINE SECT)
C XT,YT: CHANGED COORDINATES OF POINTS OF THE PROSTHESIS
C AROUND CENTROIDS (SUBROUTINE SECT)
```

C

```
RAD=2.0
ISHOR=24
NN0=0
NN1=0
NN2=0
NN3=0
```

C

C READ INPUT FILE

C

```
CALL READAT(X,Y,Z,NSCN,XP,YP,ZP,STEP,L1,L2,UEB,CCD,NSCH,
+NPPS,NAME)
```

C

C CALCULATE CENTROIDS AND NEW POINT COORDINATE AROUND CENTROIDS

C

```
CALL SECT(X,Y,Z,NPPS,NSCN(4),XBAR,YBAR,XT,YT)
```

C

```
PRINT*, 'NUMBER OF THE STEP TO BE MODELLED ?'
READ(*,*)NST
```

C

```
OPEN(3, FILE='COSF0.DAT')
OPEN(4, FILE='COSF1.DAT')
OPEN(5, FILE='COSF2.DAT')
OPEN(6, FILE='COSF3.DAT')
```

C

C DEFINE NODES (GEOMETRIES) OF THE MODELS

C

```
CALL GEOM0(XT,YT,NAME,NST,RAD,ISHOR,NPPS,NN0)
CALL GEOM1(XT,YT,NAME,NST,RAD,ISHOR,NPPS,NN1)
CALL GEOM2(XT,YT,NAME,NST,RAD,ISHOR,NPPS,NN2)
CALL GEOM3(XT,YT,NAME,NST,RAD,ISHOR,NPPS,NN3)
```

C

C DEFINE PAFBLOCKS (ELEMENTS)

C

```
CALL PABLO0(ISHOR)
CALL PABLO1(ISHOR)
CALL PABLO2(ISHOR)
```

```
      CALL PABLO3(ISHOR)
C
C DEFINE RESTRAINTS
C
      CALL RES0(ISHOR,NN0)
      CALL RES1(ISHOR,NN1)
      CALL RES2(ISHOR,NN2)
      CALL RES3(ISHOR,NN3)
C
C DEFINE LOADS
C
      CALL LOA0(XT,YT,NST,XP,ISHOR,NPPS)
      CALL LOA1(XT,YT,NST,XP,ISHOR,NPPS)
      CALL LOA2(XT,YT,NST,XP,ISHOR,NPPS)
      CALL LOA3(XT,YT,NST,XP,ISHOR,NPPS)
C
C
C
      STOP
      END
C
C
      SUBROUTINE READAT(X,Y,Z,NSCN,XP,YP,ZP,STEP,L1,L2,UEB,CCD,NSCH,
+NPPS,NAME)
      CHARACTER NAME*10
      DIMENSION X(73,30),Y(73,30),Z(73,30)
      DIMENSION NSCN(5)
      INTEGER STEP,NSCH,NPPS,CCD,L1,L2,UEB,I,J,K
      REAL XP,YP,ZP
C
C THIS SUBROUTINE READS THE INPUT FILE
C
      PRINT*, 'NAME OF THE DATA FILE'
      READ(*,55)NAME
55     FORMAT(A10)
      OPEN(2,FILE=NAME,STATUS='OLD')
      READ(2,*)STEP
C     PRINT*,STEP
      DO 100 I=1,5
        READ(2,*) NSCN(I)
C     PRINT*,NSCN(I)
100    CONTINUE
      READ(2,*) NSCH
      READ(2,*) NPPS
      READ(2,*) CCD
      READ(2,*) L1
      READ(2,*) L2
      READ(2,*) UEB
      DO 110 I=1,NSCH
        DO 120 J=1,NPPS
          READ(2,*)X(J,I)
          READ(2,*)Y(J,I)
          READ(2,*)Z(J,I)
130    CONTINUE
120    CONTINUE
110    CONTINUE
      READ(2,*)XP
      READ(2,*)YP
      READ(2,*)ZP
      CLOSE(10)
      RETURN
      END
```

```

C
C END READAT
C
C
C
C
SUBROUTINE SECT(X,Y,Z,NPPS,NSCN4,XBAR,YBAR,XT,YT)
INTEGER I,J,K,NSCN4,M,II,IQADR
REAL B,DELX,H1,H2,YMIN,YMAX
REAL PI,X3,X1,X2,Y3,Y1,Y2,A1,A2,B1,B2,D1,D2,ALPHA
DIMENSION A(30,3),AX(30,3),AY(30,3),XMAX(4,30),IPOINT(4,30)
DIMENSION X(73,30),Y(73,30),Z(73,30),SEC(0:72,3),CMID(30,3)
DIMENSION XBAR(30),YBAR(30),XT(73,30),YT(73,30)

C
C THIS SUBROUTINE CALCULATES THE CENTROIDS OF EACH SECTION
C AND NEW COORDINATES OF POINT AROUND THE CENTROIDS
C
C CALCULATION OF THE CENTROIDES FOR EACH CONTOUR
C
C FIND MAXIMUM X FOR EACH QUADRANT OF THE CONTOUR
C
      IQADR=(NPPS-1)/4
      DO 10 M=1,NSCN4
        I=0
        DO 11 II=1,4
          XMAX(II,M)=0.
          DO 12 J=1,IQADR
            I=I+1
            IF(ABS(X(I,M)).GT.ABS(XMAX(II,M)))THEN
              XMAX(II,M)=X(I,M)
              IPOINT(II,M)=I
            END IF
          12 CONTINUE
        11 CONTINUE
      10 CONTINUE
C
C LOOP ON NUMBER OF STEPS
C
      DO 20 M=1,NSCN4
C
C LOOP ON NUMBER OF POINTS AROUND PERIPHERY OF STEP
C
C CALCULATION OF STRIP PROPERTIES
C
      DO 21 I=1,NPPS-1
        DELX=ABS(X(I+1,M)-X(I,M))
        B=DELX
C
C 'NEGATIVE' AREAS OF CROSS-SECTION
C
      IF(I.LT.(IQADR+1))THEN
        IF((X(I,M).LT.XMAX(1,M)).AND.(I.LT.IPOINT(1,M)))THEN
          B=-DELX
        END IF
      END IF
      IF((I.GT.(IQADR+1)).AND.(I.LT.(2*IQADR+1)))THEN
        IF((ABS(X(I,M)).LT.ABS(XMAX(2,M))).AND.(I.GT.IPOINT(2,M)))
+ THEN
          B=-DELX
        END IF
      END IF
      IF((I.GT.(2*IQADR+1)).AND.(I.LT.(3*IQADR+1)))THEN
        IF((ABS(X(I,M)).LT.ABS(XMAX(3,M))).AND.(I.LT.IPOINT(3,M)))

```

```
+ THEN
  B=-DELX
  END IF
  END IF
  IF(I.GT.(IQADR*3))THEN
    IF((X(I,M).LT.XMAX(4,M)).AND.(I.GT.IPOINT(4,M)))THEN
      B=-DELX
      END IF
    END IF
    IF((ABS(Y(I,M)).LT.ABS(Y(I+1,M))) THEN
      YMIN=Y(I,M)
      YMAX=Y(I+1,M)
    ELSE
      YMIN=Y(I+1,M)
      YMAX=Y(I,M)
    END IF
    H1=ABS(YMIN)
    H2=ABS(YMAX)
    X1=(X(I,M)+X(I+1,M))/2.
    Y1=YMIN/2.
    Y2=YMAX/2.
    A1=B*H1
    A2=B*H2
    X2=X1

C
C CALCULATION OF STEP PROPERTIES, I.E., AREAS AND SECOND MOMENTS
C OF AREAS
C
  A(M,1)=A(M,1)+A1
  A(M,2)=A(M,2)+A2
  AX(M,1)=AX(M,1)+A1*X1
  AX(M,2)=AX(M,2)+A2*X2
  AY(M,1)=AY(M,1)+A1*Y1
  AY(M,2)=AY(M,2)+A2*Y2
21 CONTINUE
C
C AVERAGE MAX AND MIN PROPERTIES
C
  A(M,3)=(A(M,1)+A(M,2))/2.
  AX(M,3)=(AX(M,1)+AX(M,2))/2.
  AY(M,3)=(AY(M,1)+AY(M,2))/2.
C
C CENTROID COORDINATES OF STEP M
C
  XBAR(M)=AX(M,3)/A(M,3)
  YBAR(M)=AY(M,3)/A(M,3)
C
20 CONTINUE
C
C CALCULATE NEW POINTS ON THE CONTOUR IN ALPHA DEGREE STEPS
C AROUND CMIDS STARTING WITH THE POINT NO. 1
C
  PI=4*ATAN(1.0)
  ALPHA=2*PI/(NPPS-1)
  DO 100 I=1,NSCN4
    CMID(I,1)=XBAR(I)
    CMID(I,2)=YBAR(I)
    SEC(0,1)=X(1,I)
    SEC(0,2)=Y(1,I)
  K=1
  DO 210 J=0,NPPS-2
    X1=SEC(J,1)-CMID(I,1)
```

```

Y1=SEC(J,2)-CMID(I,2)
D1=SQRT(X1**2+Y1**2)
99 X2=X(MOD(K,NPPS)+1,I)-CMID(I,1)
Y2=Y(MOD(K,NPPS)+1,I)-CMID(I,2)
D2=SQRT(X2**2+Y2**2)
IF(((X1*X2+Y1*Y2)/(D1*D2)).GT.(COS(ALPHA)))THEN
  K=K+1
  GOTO 99
END IF
X3=X1*COS(PI/36)-Y1*SIN(ALPHA)
Y3=X1*SIN(PI/36)+Y1*COS(ALPHA)
X3=X3+CMID(I,1)
Y3=Y3+CMID(I,2)
IF((ABS(X3-CMID(I,1)).GT.1E-12))THEN
  A1=(Y3-CMID(I,2))/(X3-CMID(I,1))
  B1=Y3-A1*X3
  IF((ABS(X(MOD(K,NPPS)+1,I)-SEC(J,1)).GT.1E-12))THEN
    A2=(Y(MOD(K,NPPS)+1,I)-SEC(J,2))/(X(MOD(K,NPPS)+1,I)
+   -SEC(J,1))
    B2=Y(MOD(K,NPPS)+1,I)-A2*X(MOD(K,NPPS)+1,I)
    SEC(J+1,1)=(B2-B1)/(A1-A2)
    SEC(J+1,2)=A1*SEC(J+1,1)+B1
  ELSE
    A2=0.0
    B2=Y(MOD(K,NPPS)+1,I)
    SEC(J+1,1)=(B2-B1)/A1
    SEC(J+1,2)=B2
  END IF
ELSE
  A1=0.0
  B1=Y3
  IF((ABS(X(MOD(K,NPPS)+1,I)-SEC(J,1)).GT.1E-12))THEN
    A2=(Y(MOD(K,NPPS)+1,I)-SEC(J,2))/(X(MOD(K,NPPS)+1,I)
+   -SEC(J,1))
    B2=Y(MOD(K,NPPS)+1,I)-A2*X(MOD(K,NPPS)+1,I)
    SEC(J+1,1)=(B1-B2)/A2
    SEC(J+1,2)=B1
  ELSE
    SEC(J+1,1)=X(MOD(K,NPPS)+1,I)
    SEC(J+1,2)=Y(MOD(K,NPPS)+1,I)
  END IF
END IF
210 CONTINUE
C
C WRITE NEW POINTS
C
  DO 220 J=1,NPPS
    X(J,I)=SEC(J-1,1)
    Y(J,I)=SEC(J-1,2)
220 CONTINUE
100 CONTINUE
C
C POINT COORDINATES ABOUT CENTROIDS
C
  DO 300 M=1,NSCN4
    DO 310 I=1,NPPS
      XT(I,M)=X(I,M)-XBAR(M)
      YT(I,M)=Y(I,M)-YBAR(M)
310 CONTINUE
300 CONTINUE
C
C

```

```
      RETURN
      END
C
C END SECT
C
      SUBROUTINE GEOM0(XT,YT,NAME,NST,RAD,ISHOR,NPPS,NN0)
      CHARACTER NAME*10
      INTEGER I,J,K,NST,INT,NN0
      REAL PI,RAD,X,Y
      DIMENSION XT(73,30),YT(73,30)
C
C THIS SUBROUTINE DEFINES NODES FOR A 'SMOOTH' STEP
C
      PI=4.0*ATAN(1.0)
      INT=(NPPS-1)/ISHOR
      WRITE(3,1)'TITLE COSF0 - STEP PROT ',NAME
      WRITE(3,3)'C STEP NUMBER ',NST
3     FORMAT(A14,I6)
      WRITE(3,1)'CONTROL'
      WRITE(3,1)'FULL.CONTROL'
      WRITE(3,1)'PHASE=1,2,4,6,7,9'
      WRITE(3,1)'CLEAR.FILES'
      WRITE(3,1)'CONTROL.END'
C
      WRITE(3,1)'NODES'
      WRITE(3,1)'NODE.NUMB X Y Z'
1     FORMAT(80A)
C
      J=0
      WRITE(3,1)'C C FIRST CONTOUR, EDGE'
      DO 10 I=1,ISHOR
          J=J+1
          K=1+(I-1)*INT
          X=XT(K,NST)
          Y=YT(K,NST)
          WRITE(3,2)J,X,Y,0.0
2     FORMAT(I5,1X,E15.7,1X,E15.7,1X,E15.7)
10    CONTINUE
C
      WRITE(3,1)'C FIRST CONTOUR , INSIDE'
      DO 20 I=1,ISHOR
          J=J+1
          K=1+(I-1)*INT
          X=XT(K,NST)/2
          Y=YT(K,NST)/2
          WRITE(3,2)J,X,Y,0.0
20    CONTINUE
      WRITE(3,1)'C MIDPOINT'
      J=J+1
      WRITE(3,2)J,0.0,0.0,0.0
C
C
      WRITE(3,1)'C SECOND CONTOUR, EDGE'
      DO 30 I=1,ISHOR
          J=J+1
          K=1+(I-1)*INT
          X=XT(K,NST)
          Y=YT(K,NST)
          WRITE(3,2)J,X,Y,16.0
30    CONTINUE
      WRITE(3,1)'C SECOND CONTOUR, INSIDE'
      DO 40 I=1,ISHOR
```

```
J=J+1
K=1+(I-1)*INT
X=XT(K,NST)/2
Y=YT(K,NST)/2
WRITE(3,2)J,X,Y,16.0
40 CONTINUE
WRITE(3,1)'C SECOND CONTOUR, MIDPOINT'
J=J+1
WRITE(3,2)J,0.0,0.0,16.0
C
NN0=J
C
C
C
RETURN
END
C
C END GEOM0
C
C
SUBROUTINE PABLO0(ISHOR)
INTEGER I,J,K,ISHOR
INTEGER N1,N2,N5,EL,TYP,PROP
INTEGER*4 ETYP
DIMENSION EL(20)
C
C THIS SUBROUTINE DEFINES PAFBLOCKS (ELEMENTS) FOR THE SMOOTH STEP
C
WRITE(3,1)'PAFBLOCCKS'
WRITE(3,1)'BLOCK.NUMB TYPE ELEM.TYPE PROP N1 N2 N5 TOPO'
1 FORMAT(80A)
C
WRITE(3,1)'C FIRST OUTSIDE'
J=0
N1=1
N2=1
N5=5
ETYP=37110
TYP=1
PROP=20
DO 10 I=1,ISHOR/2
EL(1)=1+(I-1)*2
EL(2)=1+MOD(I*2,ISHOR)
EL(3)=2*ISHOR+1+EL(1)
EL(4)=2*ISHOR+1+EL(2)
EL(5)=ISHOR+EL(1)
EL(6)=ISHOR+EL(2)
EL(7)=ISHOR+EL(3)
EL(8)=ISHOR+EL(4)
EL(9)=EL(1)+1
EL(10)=0
EL(11)=0
EL(12)=EL(3)+1
EL(13)=0
EL(14)=0
EL(15)=0
EL(16)=0
EL(17)=EL(5)+1
EL(18)=0
EL(19)=0
EL(20)=EL(7)+1
C
```

```
      J=J+1
      WRITE(3,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,20)
2     FORMAT(7(I6,1X)/'* ',10(I5,1X)/'* ',10(I5,1X))
10    CONTINUE
C
```

```
      WRITE(3,1)'C FIRST INSIDE'
      ETYP=37210
      TYP=4
      DO 20 I=1,ISHOR/2
        EL(1)=2*ISHOR+1
        EL(2)=ISHOR+1+(I-1)*2
        EL(3)=ISHOR+1+MOD(I*2,ISHOR)
        EL(4)=EL(1)+2*ISHOR+1
        EL(5)=EL(2)+2*ISHOR+1
        EL(6)=EL(3)+2*ISHOR+1
        EL(7)=0
        EL(8)=EL(2)+1
        EL(9)=0
        EL(10)=0
        EL(11)=0
        EL(12)=0
        EL(13)=0
        EL(14)=EL(5)+1
        EL(15)=0
```

```
C
      J=J+1
      WRITE(3,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,15)
20    CONTINUE
```

```
C
C
C
C
```

```
      WRITE(3,1)'MESH'
      WRITE(3,1)'REFE SPAC.LIST'
      WRITE(3,1)'1 1'
      WRITE(3,1)'2 2'
      WRITE(3,1)'3 3'
      WRITE(3,1)'4 4'
      WRITE(3,1)'5 5'
      WRITE(3,1)'6 6'
      WRITE(3,1)'7 7'
      WRITE(3,1)'8 8'
      WRITE(3,1)'C '
      WRITE(3,1)'MATERIAL'
      WRITE(3,1)'MATE.NUMB E NU'
      WRITE(3,1)'20 110000 0.35'
```

```
C
C
```

```
      RETURN
      END
```

```
C
C END PABLO0
C
```

```
      SUBROUTINE RES0(ISHOR,NN0)
      INTEGER I,ISHOR,NN0
```

```
C
C THIS SUBROUTINE WRITES RESTRAINTS OF THE SMOOTH STEP
C
```

```
      WRITE(3,1)'RESTRAINTS'
      WRITE(3,1)'NODE.NUMB DIRECTION'
1     FORMAT(80A)
```

```
C
```

```
      DO 10 I=NN0-2*ISHOR,NN0
```

```
      WRITE(3,2)I,0
2      FORMAT(I6,1X,I6)
10     CONTINUE
C
      RETURN
      END
C
C END RES0
C
      SUBROUTINE LOA0(XT,YT,NST,XP,ISHOR,NPPS)
      INTEGER NST,ISHOR,NPPS,I
      REAL D1,D2,F1,F2,XP
      DIMENSION XT(73,30),YT(73,30)
C
C THIS SUBROUTINE CALCULATES LOADS FOR SMOOTH STEP
C
      D1=SQRT((XT(1,NST))**2+(YT(1,NST))**2)
      D2=SQRT((XT((NPPS-1)/2+1,NST))**2+(YT((NPPS-1)/2+1,NST))**2)
      F1=-0.5/D1
      F2=0.5/D2
      IF(XP.LE.0.0)THEN
          F1=-F1
          F2=-F2
      END IF
C
      WRITE(3,1)'LOADS'
      WRITE(3,1)'NODE.NUMB DIRE.OF.LOAD VALU.OF.LOAD'
1      FORMAT(80A)
C
      WRITE(3,2)1,3,F1
      I=(NPPS-1)/2+1
      WRITE(3,2)I,3,F2
C
2      FORMAT(I6,1X,I6,1X,E15.7)
C
      WRITE(3,1)'END.OF.DATA'
      RETURN
      END
C
C END LOA0
C
      SUBROUTINE GEOM1(XT,YT,NAME,NST,RAD,ISHOR,NPPS,NN1)
      CHARACTER NAME*10
      INTEGER I,J,K,NST,NPPS,ISHOR,INT,NN1
      REAL PI,RAD,AL,X,Y,Z
      DIMENSION XT(73,30),YT(73,30)
C
C THIS SUBROUTINE DEFINES NODES FOR STEP WITH 1/3 OF TRANSITION
C RADIUS
C
      PI=4.0*ATAN(1.0)
      INT=(NPPS-1)/ISHOR
      WRITE(4,1)'TITLE COSF1 - STEP PROT ',NAME
      WRITE(4,3)'C STEP NUMBER ',NST
3      FORMAT(A14,I6)
      WRITE(4,1)'CONTROL'
      WRITE(4,1)'FULL.CONTROL'
      WRITE(4,1)'PHASE=1,2,4,6,7,9'
      WRITE(4,1)'CLEAR.FILES'
      WRITE(4,1)'CONTROL.END'
C
      WRITE(4,1)'NODES'
```

```
WRITE(4,1)'NODE.NUMB X Y Z'
1
C
FORMAT(80A)
J=0
WRITE(4,1)'C C FIRST CONTOUR, EDGE'
DO 10 I=1,ISHOR
  J=J+1
  K=1+(I-1)*INT
  X=XT(K,NST)
  Y=YT(K,NST)
  WRITE(4,2)J,X,Y,0.0
2
10
C
FORMAT(I5,1X,E15.7,1X,E15.7,1X,E15.7)
CONTINUE
WRITE(4,1)'C FIRST CONTOUR , INSIDE'
DO 20 I=1,ISHOR
  J=J+1
  K=1+(I-1)*INT
  X=XT(K,NST)/2
  Y=YT(K,NST)/2
  WRITE(4,2)J,X,Y,0.0
20
CONTINUE
WRITE(4,1)'C MIDPOINT'
J=J+1
WRITE(4,2)J,0.0,0.0,0.0
C
C
WRITE(4,1)'C SECOND CONTOUR, EDGE'
DO 30 I=1,ISHOR
  J=J+1
  K=1+(I-1)*INT
  X=XT(K,NST)
  Y=YT(K,NST)
  WRITE(4,2)J,X,Y,8.0
30
CONTINUE
WRITE(4,1)'C SECOND CONTOUR, INSIDE'
DO 40 I=1,ISHOR
  J=J+1
  K=1+(I-1)*INT
  X=XT(K,NST)/2
  Y=YT(K,NST)/2
  WRITE(4,2)J,X,Y,8.0
40
CONTINUE
WRITE(4,1)'C SECOND CONTOUR, MIDPOINT'
J=J+1
WRITE(4,2)J,0.0,0.0,8.0
C
C
WRITE(4,1)'C THIRD CONTOUR, STEP'
C
AL=XT(1,NST)/SQRT(XT(1,NST)**2+YT(1,NST)**2)
IF (AL.GE.1.0) THEN
  AL=0.0
ELSE
  AL=ACOS(AL)
END IF
C
DO 50 I=1,ISHOR
  J=J+1
  K=1+(I-1)*INT
  X=XT(K,NST)+RAD*(1-COS(PI/6))*COS((I-1)*PI/12+AL)
  Y=YT(K,NST)+RAD*(1-COS(PI/6))*SIN((I-1)*PI/12+AL)
```

```
Z=8.0+RAD*SIN(PI/6)
WRITE(4,2)J,X,Y,Z
50 CONTINUE
WRITE(4,1)'C THIRD CONTOUR, INSIDE'
DO 60 I=1,ISHOR
  J=J+1
  K=1+(I-1)*INT
  X=(XT(K,NST)+RAD*(1-COS(PI/6))*COS((I-1)*PI/12+AL))/2
  Y=(YT(K,NST)+RAD*(1-COS(PI/6))*SIN((I-1)*PI/12+AL))/2
  Z=8.0+RAD*SIN(PI/6)
  WRITE(4,2)J,X,Y,Z
60 CONTINUE
WRITE(4,1)'C THIRD CONTOUR, MIDPOINT'
J=J+1
WRITE(4,2)J,0.0,0.0,8.0+RAD*SIN(PI/6)
C
C
WRITE(4,1)'C FOURTH CONTOUR, EDGE'
DO 70 I=1,ISHOR
  J=J+1
  K=1+(I-1)*INT
  X=XT(K,NST)+RAD*(1-COS(PI/6))*COS((I-1)*PI/12+AL)
  Y=YT(K,NST)+RAD*(1-COS(PI/6))*SIN((I-1)*PI/12+AL)
  Z=16.0+RAD*SIN(PI/6)
  WRITE(4,2)J,X,Y,Z
70 CONTINUE
WRITE(4,1)'C FOURTH CONTOUR, INSIDE'
DO 80 I=1,ISHOR
  J=J+1
  K=1+(I-1)*INT
  X=(XT(K,NST)+RAD*(1-COS(PI/6))*COS((I-1)*PI/12+AL))/2
  Y=(YT(K,NST)+RAD*(1-COS(PI/6))*SIN((I-1)*PI/12+AL))/2
  Z=16.0+RAD*SIN(PI/6)
  WRITE(4,2)J,X,Y,Z
80 CONTINUE
WRITE(4,1)'C FOURTH CONTOUR, MIDPOINT'
J=J+1
WRITE(4,2)J,0.0,0.0,16.0+RAD*SIN(PI/6)
C
NN1=J
C
RETURN
END
C
C END GEOM1
C
C
SUBROUTINE PABLO1(ISHOR)
INTEGER I,J,K,ISHOR
INTEGER N1,N2,N5,EL,TYP,PROP
INTEGER*4 ETYP
DIMENSION EL(20)
C
C THIS SUBROUTINE DEFINES PAFBLOCKS (ELEMENTS) FOR STEP WITH
C 1/3 OF THE TRANSITION RADIUS
C
WRITE(4,1)'PAFBLOCKCS'
WRITE(4,1)'BLOCK.NUMB TYPE ELEM.TYPE PROP N1 N2 N5 TOPO'
1 FORMAT(80A)
C
WRITE(4,1)'C FIRST OUTSIDE'
J=0
```

```
N1=1
N2=1
N5=5
ETYP=37110
TYP=1
PROP=20
DO 10 I=1, ISHOR/2
  EL(1)=1+(I-1)*2
  EL(2)=1+MOD(I*2, ISHOR)
  EL(3)=2*ISHOR+1+EL(1)
  EL(4)=2*ISHOR+1+EL(2)
  EL(5)=ISHOR+EL(1)
  EL(6)=ISHOR+EL(2)
  EL(7)=ISHOR+EL(3)
  EL(8)=ISHOR+EL(4)
  EL(9)=EL(1)+1
  EL(10)=0
  EL(11)=0
  EL(12)=EL(3)+1
  EL(13)=0
  EL(14)=0
  EL(15)=0
  EL(16)=0
  EL(17)=EL(5)+1
  EL(18)=0
  EL(19)=0
  EL(20)=EL(7)+1
C
  J=J+1
  WRITE(4,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,20)
2  FORMAT(7(I6,1X)/* ',10(I5,1X)/* ',10(I5,1X))
10 CONTINUE
C
WRITE(4,1)'C FIRST INSIDE'
ETYP=37210
TYP=4
DO 20 I=1, ISHOR/2
  EL(1)=2*ISHOR+1
  EL(2)=ISHOR+1+(I-1)*2
  EL(3)=ISHOR+1+MOD(I*2, ISHOR)
  EL(4)=EL(1)+2*ISHOR+1
  EL(5)=EL(2)+2*ISHOR+1
  EL(6)=EL(3)+2*ISHOR+1
  EL(7)=0
  EL(8)=EL(2)+1
  EL(9)=0
  EL(10)=0
  EL(11)=0
  EL(12)=0
  EL(13)=0
  EL(14)=EL(5)+1
  EL(15)=0
C
  J=J+1
  WRITE(4,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,15)
20 CONTINUE
C
C
WRITE(4,1)'C SECOND OUTSIDE'
N5=1
ETYP=37110
TYP=1
```

```
DO 30 I=1,ISHOR/2
  EL(1)=1+(I-1)*2+2*ISHOR+1
  EL(2)=1+MOD(I*2,ISHOR)+2*ISHOR+1
  EL(3)=2*ISHOR+1+EL(1)
  EL(4)=2*ISHOR+1+EL(2)
  EL(5)=ISHOR+EL(1)
  EL(6)=ISHOR+EL(2)
  EL(7)=ISHOR+EL(3)
  EL(8)=ISHOR+EL(4)
  EL(9)=EL(1)+1
  EL(10)=0
  EL(11)=0
  EL(12)=EL(3)+1
  EL(13)=0
  EL(14)=0
  EL(15)=0
  EL(16)=0
  EL(17)=EL(5)+1
  EL(18)=0
  EL(19)=0
  EL(20)=EL(7)+1
```

C

```
  J=J+1
  WRITE(4,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,20)
30 CONTINUE
  WRITE(4,1)'C SECOND INSIDE'
  ETYP=37210
  TYP=4
```

```
DO 40 I=1,ISHOR/2
  EL(1)=2*(2*ISHOR+1)
  EL(2)=ISHOR+1+(I-1)*2+2*ISHOR+1
  EL(3)=ISHOR+1+MOD(I*2,ISHOR)+2*ISHOR+1
  EL(4)=EL(1)+2*ISHOR+1
  EL(5)=EL(2)+2*ISHOR+1
  EL(6)=EL(3)+2*ISHOR+1
  EL(7)=0
  EL(8)=EL(2)+1
  EL(9)=0
  EL(10)=0
  EL(11)=0
  EL(12)=0
  EL(13)=0
  EL(14)=EL(5)+1
  EL(15)=0
```

C

```
  J=J+1
  WRITE(4,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,15)
40 CONTINUE
```

C

```
  WRITE(4,1)'C THIRD OUTSIDE'
  N5=5
  ETYP=37110
  TYP=1
DO 50 I=1,ISHOR/2
  EL(1)=1+(I-1)*2+2*(2*ISHOR+1)
  EL(2)=1+MOD(I*2,ISHOR)+2*(2*ISHOR+1)
  EL(3)=2*ISHOR+1+EL(1)
  EL(4)=2*ISHOR+1+EL(2)
  EL(5)=ISHOR+EL(1)
  EL(6)=ISHOR+EL(2)
  EL(7)=ISHOR+EL(3)
  EL(8)=ISHOR+EL(4)
```

```
EL(9)=EL(1)+1
EL(10)=0
EL(11)=0
EL(12)=EL(3)+1
EL(13)=0
EL(14)=0
EL(15)=0
EL(16)=0
EL(17)=EL(5)+1
EL(18)=0
EL(19)=0
EL(20)=EL(7)+1
```

C

```
J=J+1
WRITE(4,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,20)
50 CONTINUE
WRITE(4,1)'C THIRD INSIDE'
ETYP=37210
TYP=4
DO 60 I=1,ISHOR/2
  EL(1)=3*(2*ISHOR+1)
  EL(2)=ISHOR+1+(I-1)*2+2*(2*ISHOR+1)
  EL(3)=ISHOR+1+MOD(I*2,ISHOR)+2*(2*ISHOR+1)
  EL(4)=EL(1)+2*ISHOR+1
  EL(5)=EL(2)+2*ISHOR+1
  EL(6)=EL(3)+2*ISHOR+1
  EL(7)=0
  EL(8)=EL(2)+1
  EL(9)=0
  EL(10)=0
  EL(11)=0
  EL(12)=0
  EL(13)=0
  EL(14)=EL(5)+1
  EL(15)=0
```

C

```
J=J+1
WRITE(4,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,15)
60 CONTINUE
```

C

```
WRITE(4,1)'MESH'
WRITE(4,1)'REFE SPAC.LIST'
WRITE(4,1)'1 1'
WRITE(4,1)'2 2'
WRITE(4,1)'3 3'
WRITE(4,1)'4 4'
WRITE(4,1)'5 5'
WRITE(4,1)'6 6'
WRITE(4,1)'7 7'
WRITE(4,1)'8 8'
WRITE(4,1)'C '
WRITE(4,1)'MATERIAL'
WRITE(4,1)'MATE.NUMB E NU'
WRITE(4,1)'20 110000 0.35'
```

C

C

```
RETURN
END
```

C

```
C END PABLO1
```

C

```
SUBROUTINE RES1(ISHOR,NN1)
```

```
      INTEGER I,ISHOR,NN1
C
C THIS SUBROUTINE INPOSES CONSTRAINTS ON THE MODEL OF STEP
C WITH 1/3 OF THE TRANSITION RADIUS
C
      WRITE(4,1)'RESTRAINTS'
      WRITE(4,1)'NODE.NUMB DIRECTION'
1     FORMAT(80A)
C
      DO 10 I=NN1-2*ISHOR,NN1
          WRITE(4,2)I,0
2         FORMAT(I6,1X,I6)
10    CONTINUE
C
      RETURN
      END
C
C END RES1
C
      SUBROUTINE LOA1(XT,YT,NST,XP,ISHOR,NPPS)
      INTEGER NST,ISHOR,NPPS,I
      REAL D1,D2,F1,F2,XP,X,Y,PI
      DIMENSION XT(73,30),YT(73,30)
C
C THIS SUBROUTINE CALCULATES LOADS FOR STEP WITH 1/3 OF
C TRANSITION RADIUS
C
      PI=4.0*ATAN(1.0)
      X=XT(1,NST)
      Y=YT(1,NST)
      D1=SQRT(X**2+Y**2)
C
      X=XT((NPPS-1)/2+1,NST)
      Y=YT((NPPS-1)/2+1,NST)
      D2=SQRT(X**2+Y**2)
C
      F1=-0.5/D1
      F2=0.5/D2
      IF(XP.LE.0.0)THEN
          F1=-F1
          F2=-F2
      END IF
C
      WRITE(4,1)'LOADS'
      WRITE(4,1)'NODE.NUMB DIRE.OF.LOAD VALU.OF.LOAD'
1     FORMAT(80A)
C
      WRITE(4,2)1,3,F1
          I=(NPPS-1)/2+1
          WRITE(4,2)I,3,F2
C
2     FORMAT(I6,1X,I6,1X,E15.7)
C
      WRITE(4,1)'END.OF.DATA'
      RETURN
      END
C
C END LOA1
C
      SUBROUTINE GEOM2(XT,YT,NAME,NST,RAD,ISHOR,NPPS,NN2)
      CHARACTER NAME*10
      INTEGER I,J,K,NST,ISHOR,NPPS,INT,NN2
```

```
REAL PI,RAD,AL,X,Y,Z  
DIMENSION XT(73,30),YT(73,30)
```

```
C  
C THIS SUBROUTINE DEFINES NODES FOR STEP WITH 2/3 OF THE  
C TRANSITION RADIUS
```

```
C  
PI=4.0*ATAN(1.0)  
INT=(NPPS-1)/ISHOR  
WRITE(5,1)'TITLE COSF2 - STEP PROT ',NAME  
WRITE(5,3)'C STEP NUMBER ',NST  
3 FORMAT(A14,I6)  
WRITE(5,1)'CONTROL'  
WRITE(5,1)'FULL.CONTROL'  
WRITE(5,1)'PHASE=1,2,4,6,7,9'  
WRITE(5,1)'CLEAR.FILES'  
WRITE(5,1)'CONTROL.END'
```

```
C  
WRITE(5,1)'NODES'  
WRITE(5,1)'NODE.NUMB X Y Z'  
1 FORMAT(80A)  
C
```

```
J=0  
WRITE(5,1)'C C FIRST CONTOUR, EDGE'  
DO 10 I=1,ISHOR  
J=J+1  
K=1+(I-1)*INT  
WRITE(5,2)J,XT(K,NST),YT(K,NST),0.0  
2 FORMAT(I5,1X,E15.7,1X,E15.7,1X,E15.7)  
10 CONTINUE  
C
```

```
AL=XT(1,NST)/SQRT(XT(1,NST)**2+YT(1,NST)**2)  
IF(AL.GE.1.0)THEN  
AL=0.0  
ELSE  
AL=ACOS(AL)  
END IF  
C
```

```
WRITE(5,1)'C FIRST CONTOUR , 1ST INSIDE'  
DO 15 I=1,ISHOR  
J=J+1  
K=1+(I-1)*INT  
X=XT(K,NST)-RAD*COS((I-1)*PI/12+AL)/2  
Y=YT(K,NST)-RAD*SIN((I-1)*PI/12+AL)/2  
WRITE(5,2)J,X,Y,0.0  
15 CONTINUE  
C
```

```
WRITE(5,1)'C FIRST CONTOUR , 2ND INSIDE'  
DO 20 I=1,ISHOR  
J=J+1  
K=1+(I-1)*INT  
X=(XT(K,NST)-RAD*COS((I-1)*PI/12+AL)/2)/2  
Y=(YT(K,NST)-RAD*SIN((I-1)*PI/12+AL)/2)/2  
WRITE(5,2)J,X,Y,0.0  
20 CONTINUE  
WRITE(5,1)'C MIDPOINT'  
J=J+1  
WRITE(5,2)J,0.0,0.0,0.0  
C
```

```
C  
WRITE(5,1)'C SECOND CONTOUR, EDGE'  
DO 30 I=1,ISHOR  
J=J+1
```

```
      K=1+(I-1)*INT
      WRITE(5,2)J,XT(K,NST),YT(K,NST),8.0
30  CONTINUE
C
      WRITE(5,1)'C SECOND CONTOUR, 1ST INSIDE'
      DO 35 I=1,ISHOR
        J=J+1
        K=1+(I-1)*INT
        X=XT(K,NST)-RAD*COS((I-1)*PI/12+AL)/2
        Y=YT(K,NST)-RAD*SIN((I-1)*PI/12+AL)/2
        WRITE(5,2)J,X,Y,8.0
35  CONTINUE
C
      WRITE(5,1)'C SECOND CONTOUR, 2ND INSIDE'
      DO 40 I=1,ISHOR
        J=J+1
        K=1+(I-1)*INT
        X=(XT(K,NST)-RAD*COS((I-1)*PI/12+AL)/2)/2
        Y=(YT(K,NST)-RAD*SIN((I-1)*PI/12+AL)/2)/2
        WRITE(5,2)J,X,Y,8.0
40  CONTINUE
      WRITE(5,1)'C SECOND CONTOUR, MIDPOINT'
      J=J+1
      WRITE(5,2)J,0.0,0.0,8.0
C
C
      WRITE(5,1)'C THIRD CONTOUR, STEP'
      DO 50 I=1,ISHOR
        J=J+1
        K=1+(I-1)*INT
        X=XT(K,NST)+RAD*(1-COS(PI/6))*COS((I-1)*PI/12+AL)
        Y=YT(K,NST)+RAD*(1-COS(PI/6))*SIN((I-1)*PI/12+AL)
        Z=8.0+RAD*SIN(PI/6)
        WRITE(5,2)J,X,Y,Z
50  CONTINUE
C
      WRITE(5,1)'C THIRD CONTOUR, 1ST INSIDE'
      DO 55 I=1,ISHOR
        J=J+1
        K=1+(I-1)*INT
        X=XT(K,NST)-RAD*COS((I-1)*PI/12+AL)/2
        Y=YT(K,NST)-RAD*SIN((I-1)*PI/12+AL)/2
        Z=8.0+RAD*SIN(PI/INT)
        WRITE(5,2)J,XT(K,NST)-RAD*COS((I-1)*PI/12+AL)/2
1, YT(K,NST)-RAD*SIN((I-1)*PI/12+AL)/2
2, 8.0+RAD*SIN(PI/INT)
55  CONTINUE
C
      WRITE(5,1)'C THIRD CONTOUR, 2ND INSIDE'
      DO 60 I=1,ISHOR
        J=J+1
        K=1+(I-1)*INT
        X=(XT(K,NST)-RAD*COS((I-1)*PI/12+AL)/2)/2
        Y=(YT(K,NST)-RAD*SIN((I-1)*PI/12+AL)/2)/2
        Z=8.0+RAD*SIN(PI/3)
        WRITE(5,2)J,X,Y,Z
60  CONTINUE
      WRITE(5,1)'C THIRD CONTOUR, MIDPOINT'
      J=J+1
      Z=8.0+RAD*SIN(PI/3)
      WRITE(5,2)J,0.0,0.0,Z
C
```

```
WRITE(5,1)'C FOURTH CONTOUR, STEP'  
DO 70 I=1,ISHOR  
  J=J+1  
  K=1+(I-1)*INT  
  X=XT(K,NST)+RAD*(1-COS(PI/3))*COS((I-1)*PI/12+AL)  
  Y=YT(K,NST)+RAD*(1-COS(PI/3))*SIN((I-1)*PI/12+AL)  
  Z=8.0+RAD*SIN(PI/3)  
  WRITE(5,2)J,X,Y,Z  
70 CONTINUE  
C  
WRITE(5,1)'C FOURTH CONTOUR, 1ST INSIDE'  
DO 75 I=1,ISHOR  
  J=J+1  
  K=1+(I-1)*INT  
  X=XT(K,NST)-RAD*COS((I-1)*PI/12+AL)/2  
  Y=YT(K,NST)-RAD*SIN((I-1)*PI/12+AL)/2  
  Z=8.0+RAD*SIN(PI/3)  
  WRITE(5,2)J,X,Y,Z  
75 CONTINUE  
C  
WRITE(5,1)'C FOURTH CONTOUR, 2ND INSIDE'  
DO 80 I=1,ISHOR  
  J=J+1  
  K=1+(I-1)*INT  
  X=(XT(K,NST)-RAD*COS((I-1)*PI/12+AL)/2)/2  
  Y=(YT(K,NST)-RAD*SIN((I-1)*PI/12+AL)/2)/2  
  Z=8.0+RAD*SIN(PI/3)  
  WRITE(5,2)J,X,Y,Z  
80 CONTINUE  
WRITE(5,1)'C FOURTH CONTOUR, MIDPOINT'  
  J=J+1  
  Z=8.0+RAD*SIN(PI/3)  
  WRITE(5,2)J,0.0,0.0,Z  
C  
WRITE(5,1)'C FIFTH CONTOUR, EDGE'  
DO 90 I=1,ISHOR  
  J=J+1  
  K=1+(I-1)*INT  
  X=XT(K,NST)+RAD*(1-COS(PI/3))*COS((I-1)*PI/12+AL)  
  Y=YT(K,NST)+RAD*(1-COS(PI/3))*SIN((I-1)*PI/12+AL)  
  Z=8.0+RAD*SIN(PI/3)  
  WRITE(5,2)J,X,Y,Z  
90 CONTINUE  
C  
WRITE(5,1)'C FIFTH CONTOUR, 1ST INSIDE'  
DO 95 I=1,ISHOR  
  J=J+1  
  K=1+(I-1)*INT  
  X=XT(K,NST)-RAD*COS((I-1)*PI/12+AL)/2  
  Y=YT(K,NST)-RAD*SIN((I-1)*PI/12+AL)/2  
  Z=16.0+RAD*SIN(PI/3)  
  WRITE(5,2)J,X,Y,Z  
95 CONTINUE  
C  
WRITE(5,1)'C FIFTH CONTOUR, 2ND INSIDE'  
DO 100 I=1,ISHOR  
  J=J+1  
  K=1+(I-1)*INT  
  X=(XT(K,NST)-RAD*COS((I-1)*PI/12+AL)/2)/2  
  Y=(YT(K,NST)-RAD*SIN((I-1)*PI/12+AL)/2)/2  
  Z=16.0+RAD*SIN(PI/3)  
  WRITE(5,2)J,X,Y,Z
```

```
100 CONTINUE
WRITE(5,1)'C FITH CONTOUR, MIDPOINT'
J=J+1
Z=16.0+RAD*SIN(PI/3)
WRITE(5,2)J,0.0,0.0,Z
C
NN2=J
C
RETURN
END
C
C END GEOM2
C
C
SUBROUTINE PABLO2(ISHOR)
INTEGER I,J,K,ISHOR
INTEGER N1,N2,N5,EL,TYP,PROP
INTEGER*4 ETYP
DIMENSION EL(20)
C
C THIS SUBROUTINE DEFINES PAFBLOCKS (ELEMENTS) FOR STEP WITH
C 2/3 OF TRANSITION RADIUS
C
WRITE(5,1)'PAFBLOCKCS'
WRITE(5,1)'BLOCK.NUMB TYPE ELEM.TYPE PROP N1 N2 N5 TOPO'
1 FORMAT(80A)
C
WRITE(5,1)'C FIRST OUTSIDE'
J=0
N1=1
N2=1
N5=5
ETYP=37110
TYP=1
PROP=20
DO 10 I=1,ISHOR/2
EL(1)=1+(I-1)*2
EL(2)=1+MOD(I*2,ISHOR)
EL(3)=3*ISHOR+1+EL(1)
EL(4)=3*ISHOR+1+EL(2)
EL(5)=ISHOR+EL(1)
EL(6)=ISHOR+EL(2)
EL(7)=ISHOR+EL(3)
EL(8)=ISHOR+EL(4)
EL(9)=EL(1)+1
EL(10)=0
EL(11)=0
EL(12)=EL(3)+1
EL(13)=0
EL(14)=0
EL(15)=0
EL(16)=0
EL(17)=EL(5)+1
EL(18)=0
EL(19)=0
EL(20)=EL(7)+1
C
J=J+1
WRITE(5,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,20)
2 FORMAT(7(I6,1X)/* ',10(I5,1X)/* ',10(I5,1X))
10 CONTINUE
C
```

```
WRITE(5,1)'C FIRST INSIDE, 1ST'  
ETYP=37110  
TYP=1  
PROP=20  
DO 15 I=1, ISHOR/2  
  EL(1)=1+(I-1)*2+ISHOR  
  EL(2)=1+MOD(I*2, ISHOR)+ISHOR  
  EL(3)=3*ISHOR+1+EL(1)  
  EL(4)=3*ISHOR+1+EL(2)  
  EL(5)=ISHOR+EL(1)  
  EL(6)=ISHOR+EL(2)  
  EL(7)=ISHOR+EL(3)  
  EL(8)=ISHOR+EL(4)  
  EL(9)=EL(1)+1  
  EL(10)=0  
  EL(11)=0  
  EL(12)=EL(3)+1  
  EL(13)=0  
  EL(14)=0  
  EL(15)=0  
  EL(16)=0  
  EL(17)=EL(5)+1  
  EL(18)=0  
  EL(19)=0  
  EL(20)=EL(7)+1
```

C

```
  J=J+1  
  WRITE(5,2)J, TYP, ETYP, PROP, N1, N2, N5, (EL(K), K=1, 20)
```

15

```
CONTINUE
```

C

```
WRITE(5,1)'C FIRST INSIDE, 2ND'  
ETYP=37210  
TYP=4  
DO 20 I=1, ISHOR/2  
  EL(1)=3*ISHOR+1  
  EL(2)=2*ISHOR+1+(I-1)*2  
  EL(3)=2*ISHOR+1+MOD(I*2, ISHOR)  
  EL(4)=EL(1)+3*ISHOR+1  
  EL(5)=EL(2)+3*ISHOR+1  
  EL(6)=EL(3)+3*ISHOR+1  
  EL(7)=0  
  EL(8)=EL(2)+1  
  EL(9)=0  
  EL(10)=0  
  EL(11)=0  
  EL(12)=0  
  EL(13)=0  
  EL(14)=EL(5)+1  
  EL(15)=0
```

C

```
  J=J+1  
  WRITE(5,2)J, TYP, ETYP, PROP, N1, N2, N5, (EL(K), K=1, 15)
```

20

```
CONTINUE
```

C

```
WRITE(5,1)'C SECOND OUTSIDE'  
N5=1  
ETYP=37110  
TYP=1  
DO 30 I=1, ISHOR/2  
  EL(1)=1+(I-1)*2+3*ISHOR+1  
  EL(2)=1+MOD(I*2, ISHOR)+3*ISHOR+1
```

C

```
EL(3)=3*ISHOR+1+EL(1)
EL(4)=3*ISHOR+1+EL(2)
EL(5)=ISHOR+EL(1)
EL(6)=ISHOR+EL(2)
EL(7)=ISHOR+EL(3)
EL(8)=ISHOR+EL(4)
EL(9)=EL(1)+1
EL(10)=0
EL(11)=0
EL(12)=EL(3)+1
EL(13)=0
EL(14)=0
EL(15)=0
EL(16)=0
EL(17)=EL(5)+1
EL(18)=0
EL(19)=0
EL(20)=EL(7)+1
```

C

```
J=J+1
WRITE(5,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,20)
30 CONTINUE
```

C

```
WRITE(5,1)'C SECOND INSIDE, 1ST'
ETYP=37110
TYP=1
DO 35 I=1,ISHOR/2
  EL(1)=1+(I-1)*2+ISHOR+3*ISHOR+1
  EL(2)=1+MOD(I*2,ISHOR)+ISHOR+3*ISHOR+1
  EL(3)=3*ISHOR+1+EL(1)
  EL(4)=3*ISHOR+1+EL(2)
  EL(5)=ISHOR+EL(1)
  EL(6)=ISHOR+EL(2)
  EL(7)=ISHOR+EL(3)
  EL(8)=ISHOR+EL(4)
  EL(9)=EL(1)+1
  EL(10)=0
  EL(11)=0
  EL(12)=EL(3)+1
  EL(13)=0
  EL(14)=0
  EL(15)=0
  EL(16)=0
  EL(17)=EL(5)+1
  EL(18)=0
  EL(19)=0
  EL(20)=EL(7)+1
```

C

```
J=J+1
WRITE(5,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,20)
35 CONTINUE
```

C

```
WRITE(5,1)'C SECOND INSIDE, 2ND'
ETYP=37210
TYP=4
DO 40 I=1,ISHOR/2
  EL(1)=2*(3*ISHOR+1)
  EL(2)=2*ISHOR+1+(I-1)*2+3*ISHOR+1
  EL(3)=2*ISHOR+1+MOD(I*2,ISHOR)+3*ISHOR+1
  EL(4)=EL(1)+3*ISHOR+1
  EL(5)=EL(2)+3*ISHOR+1
  EL(6)=EL(3)+3*ISHOR+1
```

```
EL(7)=0
EL(8)=EL(2)+1
EL(9)=0
EL(10)=0
EL(11)=0
EL(12)=0
EL(13)=0
EL(14)=EL(5)+1
EL(15)=0
```

C

```
J=J+1
WRITE(5,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,15)
40 CONTINUE
```

C

```
WRITE(5,1)'C WEDGE IN STEP'
N5=1
ETYP=37210
TYP=4
DO 50 I=1,ISHOR/2
  EL(1)=2*(3*ISHOR+1)+1+(I-1)*2
  EL(2)=EL(1)+ISHOR
  EL(3)=3*(3*ISHOR+1)+1+(I-1)*2
  EL(4)=2*(3*ISHOR+1)+1+MOD(I*2,ISHOR)
  EL(5)=EL(4)+ISHOR
  EL(6)=3*(3*ISHOR+1)+1+MOD(I*2,ISHOR)
  EL(7)=0
  EL(8)=0
  EL(9)=0
  EL(10)=EL(1)+1
  EL(11)=EL(2)+1
  EL(12)=EL(3)+1
  EL(13)=0
  EL(14)=0
  EL(15)=0
```

C

```
J=J+1
WRITE(5,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,15)
50 CONTINUE
```

C

```
WRITE(5,1)'C THIRD OUTSIDE'
N5=5
ETYP=37110
TYP=1
DO 60 I=1,ISHOR/2
  EL(1)=1+(I-1)*2+3*(3*ISHOR+1)
  EL(2)=1+MOD(I*2,ISHOR)+3*(3*ISHOR+1)
  EL(3)=3*ISHOR+1+EL(1)
  EL(4)=3*ISHOR+1+EL(2)
  EL(5)=ISHOR+EL(1)
  EL(6)=ISHOR+EL(2)
  EL(7)=ISHOR+EL(3)
  EL(8)=ISHOR+EL(4)
  EL(9)=EL(1)+1
  EL(10)=0
  EL(11)=0
  EL(12)=EL(3)+1
  EL(13)=0
  EL(14)=0
  EL(15)=0
  EL(16)=0
  EL(17)=EL(5)+1
  EL(18)=0
```

```
      EL(19)=0
      EL(20)=EL(7)+1
C
      J=J+1
      WRITE(5,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,20)
60    CONTINUE
C
      WRITE(5,1)'C THIRD INSIDE, 1ST'
      ETYP=37110
      TYP=1
      DO 65 I=1,ISHOR/2
        EL(1)=1+(I-1)*2+ISHOR+3*(3*ISHOR+1)
        EL(2)=1+MOD(I*2,ISHOR)+ISHOR+3*(3*ISHOR+1)
        EL(3)=3*ISHOR+1+EL(1)
        EL(4)=3*ISHOR+1+EL(2)
        EL(5)=ISHOR+EL(1)
        EL(6)=ISHOR+EL(2)
        EL(7)=ISHOR+EL(3)
        EL(8)=ISHOR+EL(4)
        EL(9)=EL(1)+1
        EL(10)=0
        EL(11)=0
        EL(12)=EL(3)+1
        EL(13)=0
        EL(14)=0
        EL(15)=0
        EL(16)=0
        EL(17)=EL(5)+1
        EL(18)=0
        EL(19)=0
        EL(20)=EL(7)+1
C
      J=J+1
      WRITE(5,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,20)
65    CONTINUE
C
      WRITE(5,1)'C THIRD INSIDE, 2ND'
      ETYP=37210
      TYP=4
      DO 70 I=1,ISHOR/2
        EL(1)=4*(3*ISHOR+1)
        EL(2)=2*ISHOR+1+(I-1)*2+3*(3*ISHOR+1)
        EL(3)=2*ISHOR+1+MOD(I*2,ISHOR)+3*(3*ISHOR+1)
        EL(4)=EL(1)+3*ISHOR+1
        EL(5)=EL(2)+3*ISHOR+1
        EL(6)=EL(3)+3*ISHOR+1
        EL(7)=0
        EL(8)=EL(2)+1
        EL(9)=0
        EL(10)=0
        EL(11)=0
        EL(12)=0
        EL(13)=0
        EL(14)=EL(5)+1
        EL(15)=0
C
      J=J+1
      WRITE(5,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,15)
70    CONTINUE
C
      WRITE(5,1)'MESH'
```

```
WRITE(5,1)'REFE SPAC.LIST'  
WRITE(5,1)'1 1'  
WRITE(5,1)'2 2'  
WRITE(5,1)'3 3'  
WRITE(5,1)'4 4'  
WRITE(5,1)'5 5'  
WRITE(5,1)'6 6'  
WRITE(5,1)'7 7'  
WRITE(5,1)'8 8'  
WRITE(5,1)'C '  
WRITE(5,1)'MATERIAL'  
WRITE(5,1)'MATE.NUMB E NU'  
WRITE(5,1)'20 110000 0.35'  
  
C  
C  
    RETURN  
    END  
  
C  
C END PABLO2  
C  
    SUBROUTINE RES2(ISHOR,NN2)  
    INTEGER I,ISHOR,NN2  
  
C  
C THIS SUBROUTINE IMPOSES CONSTRAINTS ON THE MODEL OF STEP  
C WITH 2/3 OF TRANSITION RADIUS  
C  
    WRITE(5,1)'RESTRAINTS'  
    WRITE(5,1)'NODE.NUMB DIRECTION'  
1    FORMAT(80A)  
C  
    DO 10 I=NN2-3*ISHOR,NN2  
        WRITE(5,2)I,0  
2        FORMAT(I6,1X,I6)  
10    CONTINUE  
C  
    RETURN  
    END  
  
C  
C END RES2  
C  
    SUBROUTINE LOA2(XT,YT,NST,XP,ISHOR,NPPS)  
    INTEGER NST,ISHOR,NPPS,I  
    REAL D1,D2,F1,F2,XP,X,Y,PI  
    DIMENSION XT(73,30),YT(73,30)  
  
C  
C THIS SUBROUTINE CALCULATES LOAD FOR STEP WITH  
C 2/3 OF TRANSITION RADIUS  
C  
    PI=4.0*ATAN(1.0)  
    X=XT(1,NST)  
    Y=YT(1,NST)  
    D1=SQRT(X**2+Y**2)  
  
C  
    X=XT((NPPS-1)/2+1,NST)  
    Y=YT((NPPS-1)/2+1,NST)  
    D2=SQRT(X**2+Y**2)  
  
C  
C  
    F1=-0.5/D1  
    F2=0.5/D2  
    IF(XP.LE.0.0)THEN  
        F1=-F1
```

```
      F2=-F2
      END IF
C
      WRITE(5,1)'LOADS'
      WRITE(5,1)'NODE.NUMB DIRE.OF.LOAD VALU.OF.LOAD'
1      FORMAT(80A)
C
      WRITE(5,2)1,3,F1
      I=(NPPS-1)/2+1
      WRITE(5,2)I,3,F2
C
2      FORMAT(I6,1X,I6,1X,E15.7)
C
      WRITE(5,1)'END.OF.DATA'
      RETURN
      END
C
C END LOA2
C
      SUBROUTINE GEOM3(XT,YT,NAME,NST,RAD,ISHOR,NPPS,NN3)
      CHARACTER NAME*10
      INTEGER I,J,K,NST,ISHOR,NPPS,INT,NN3
      REAL PI,RAD,AL,X,Y,Z
      DIMENSION XT(73,30),YT(73,30)
C
C THIS SUBROUTINE DEFINES NODES FOR STEP WITH WHOLE
C TRANSITION RADIUS
C
      PI=4.0*ATAN(1.0)
      INT=(NPPS-1)/ISHOR
      WRITE(6,1)'TITLE COSF3 - STEP  PROT ',NAME
      WRITE(6,3)'C STEP NUMBER ',NST
3      FORMAT(A14,I6)
      WRITE(6,1)'CONTROL'
      WRITE(6,1)'FULL.CONTROL'
      WRITE(6,1)'PHASE=1,2,4,6,7,9'
      WRITE(6,1)'CLEAR.FILES'
      WRITE(6,1)'CONTROL.END'
C
      WRITE(6,1)'NODES'
      WRITE(6,1)'NODE.NUMB  X   Y   Z'
1      FORMAT(80A)
C
      AL=XT(1,NST)/SQRT(XT(1,NST)**2+YT(1,NST)**2)
      IF(AL.GE.1.0)THEN
          AL=0.0
      ELSE
          AL=ACOS(AL)
      END IF
C
      J=0
      WRITE(6,1)'C C FIRST CONTOUR, EDGE'
      DO 10 I=1,ISHOR
          J=J+1
          K=1+(I-1)*INT
          WRITE(6,2)J,XT(K,NST),YT(K,NST),0.0
2          FORMAT(I5,1X,E15.7,1X,E15.7,1X,E15.7)
10      CONTINUE
C
      WRITE(6,1)'C FIRST CONTOUR , 1ST INSIDE'
      DO 15 I=1,ISHOR
          J=J+1
```

```
K=1+(I-1)*INT
X=XT(K,NST)-RAD*COS((I-1)*PI/12+AL)/2
Y=YT(K,NST)-RAD*SIN((I-1)*PI/12+AL)/2
WRITE(6,2)J,X,Y,0.0
15 CONTINUE
C
WRITE(6,1)'C FIRST CONTOUR , 2ND INSIDE'
DO 20 I=1,ISHOR
  J=J+1
  K=1+(I-1)*INT
  X=(XT(K,NST)-RAD*COS((I-1)*PI/12+AL)/2)/2
  Y=(YT(K,NST)-RAD*SIN((I-1)*PI/12+AL)/2)/2
  WRITE(6,2)J,X,Y,0.0
20 CONTINUE
WRITE(6,1)'C MIDPOINT'
J=J+1
WRITE(6,2)J,0.0,0.0,0.0
C
C
WRITE(6,1)'C SECOND CONTOUR, EDGE'
DO 30 I=1,ISHOR
  J=J+1
  K=1+(I-1)*INT
  WRITE(6,2)J,XT(K,NST),YT(K,NST),8.0
30 CONTINUE
C
WRITE(6,1)'C SECOND CONTOUR, 1ST INSIDE'
DO 35 I=1,ISHOR
  J=J+1
  K=1+(I-1)*INT
  X=XT(K,NST)-RAD*COS((I-1)*PI/12+AL)/2
  Y=YT(K,NST)-RAD*SIN((I-1)*PI/12+AL)/2
  WRITE(6,2)J,X,Y,8.0
35 CONTINUE
C
WRITE(6,1)'C SECOND CONTOUR, 2ND INSIDE'
DO 40 I=1,ISHOR
  J=J+1
  K=1+(I-1)*INT
  X=(XT(K,NST)-RAD*COS((I-1)*PI/12+AL)/2)/2
  Y=(YT(K,NST)-RAD*SIN((I-1)*PI/12+AL)/2)/2
  WRITE(6,2)J,X,Y,8.0
40 CONTINUE
WRITE(6,1)'C SECOND CONTOUR, MIDPOINT'
J=J+1
WRITE(6,2)J,0.0,0.0,8.0
C
C
WRITE(6,1)'C THIRD CONTOUR, STEP'
C
DO 50 I=1,ISHOR
  J=J+1
  K=1+(I-1)*INT
  X=XT(K,NST)+RAD*(1-COS(PI/6))*COS((I-1)*PI/12+AL)
  Y=YT(K,NST)+RAD*(1-COS(PI/6))*SIN((I-1)*PI/12+AL)
  Z=8.0+RAD*SIN(PI/6)
  WRITE(6,2)J,X,Y,Z
50 CONTINUE
C
WRITE(6,1)'C THIRD CONTOUR, 1ST INSIDE'
DO 55 I=1,ISHOR
  J=J+1
```

```
K=1+(I-1)*INT
X=XT(K,NST)-RAD*COS((I-1)*PI/12+AL)/2
Y=YT(K,NST)-RAD*SIN((I-1)*PI/12+AL)/2
Z=8.0+RAD*SIN(PI/3)
WRITE(6,2)J,X,Y,Z
55 CONTINUE
C
WRITE(6,1)'C THIRD CONTOUR, 2ND INSIDE'
DO 60 I=1,ISHOR
  J=J+1
  K=1+(I-1)*INT
  X=(XT(K,NST)-RAD*COS((I-1)*PI/12+AL)/2)/2
  Y=(YT(K,NST)-RAD*SIN((I-1)*PI/12+AL)/2)/2
  Z=8.0+RAD*SIN(PI/3)
  WRITE(6,2)J,X,Y,Z
60 CONTINUE
WRITE(6,1)'C THIRD CONTOUR, MIDPOINT'
J=J+1
Z=8.0+RAD*SIN(PI/3)
WRITE(6,2)J,0.0,0.0,Z
C
WRITE(6,1)'C FOURTH CONTOUR, STEP'
DO 70 I=1,ISHOR
  J=J+1
  K=1+(I-1)*INT
  X=XT(K,NST)+RAD*(1-COS(PI/3))*COS((I-1)*PI/12+AL)
  Y=YT(K,NST)+RAD*(1-COS(PI/3))*SIN((I-1)*PI/12+AL)
  Z=8.0+RAD*SIN(PI/3)
  WRITE(6,2)J,X,Y,Z
70 CONTINUE
C
WRITE(6,1)'C FOURTH CONTOUR, 1ST INSIDE'
DO 75 I=1,ISHOR
  J=J+1
  K=1+(I-1)*INT
  Z=8.0+RAD*3/2
  WRITE(6,2)J,XT(K,NST),YT(K,NST),Z
75 CONTINUE
C
WRITE(6,1)'C FOURTH CONTOUR, 2ND INSIDE'
DO 78 I=1,ISHOR
  J=J+1
  K=1+(I-1)*INT
  X=XT(K,NST)-RAD*COS((I-1)*PI/12+AL)/2
  Y=YT(K,NST)-RAD*SIN((I-1)*PI/12+AL)/2
  Z=8.0+RAD*3/2
  WRITE(6,2)J,X,Y,Z
78 CONTINUE
C
WRITE(6,1)'C FOURTH CONTOUR, 3RD INSIDE'
DO 80 I=1,ISHOR
  J=J+1
  K=1+(I-1)*INT
  X=(XT(K,NST)-RAD*COS((I-1)*PI/12+AL)/2)/2
  Y=(YT(K,NST)-RAD*SIN((I-1)*PI/12+AL)/2)/2
  Z=8.0+RAD*3/2
  WRITE(6,2)J,X,Y,Z
80 CONTINUE
C
WRITE(6,1)'C FOURTH CONTOUR, MIDPOINT'
J=J+1
Z=8.0+RAD*3/2
```

```
WRITE(6,2)J,0.0,0.0,Z
C
WRITE(6,1)'C FOURTH CONTOUR, EXTRA'
DO 85 I=1,ISHOR
  J=J+1
  K=1+(I-1)*INT
  X=XT(K,NST)+RAD*COS((I-1)*PI/12+AL)
  Y=YT(K,NST)+RAD*SIN((I-1)*PI/12+AL)
  Z=8.0+RAD
  WRITE(6,2)J,X,Y,Z
85 CONTINUE
C
WRITE(6,1)'C FIFTH CONTOUR, EDGE'
DO 90 I=1,ISHOR
  J=J+1
  K=1+(I-1)*INT
  X=XT(K,NST)+RAD*COS((I-1)*PI/12+AL)
  Y=YT(K,NST)+RAD*SIN((I-1)*PI/12+AL)
  Z=8.0+RAD*3/2
  WRITE(6,2)J,X,Y,Z
90 CONTINUE
C
WRITE(6,1)'C FIFTH CONTOUR, 1ST INSIDE'
DO 92 I=1,ISHOR
  J=J+1
  K=1+(I-1)*INT
  Z=8.0+RAD*3/2
  WRITE(6,2)J,XT(K,NST),YT(K,NST),Z
92 CONTINUE
C
WRITE(6,1)'C FIFTH CONTOUR, 2ND INSIDE'
DO 95 I=1,ISHOR
  J=J+1
  K=1+(I-1)*INT
  X=XT(K,NST)-RAD*COS((I-1)*PI/12+AL)/2
  Y=YT(K,NST)-RAD*SIN((I-1)*PI/12+AL)/2
  Z=8.0+RAD*3/2
  WRITE(6,2)J,X,Y,Z
95 CONTINUE
C
WRITE(6,1)'C FIFTH CONTOUR, 3RD INSIDE'
DO 100 I=1,ISHOR
  J=J+1
  K=1+(I-1)*INT
  X=(XT(K,NST)-RAD*COS((I-1)*PI/12+AL)/2)/2
  Y=(YT(K,NST)-RAD*SIN((I-1)*PI/12+AL)/2)/2
  Z=8.0+RAD*3/2
  WRITE(6,2)J,X,Y,Z
100 CONTINUE
WRITE(6,1)'C FIFTH CONTOUR, MIDPOINT'
J=J+1
Z=8.0+RAD*3/2
WRITE(6,2)J,0.0,0.0,Z
C
WRITE(6,1)'C SIXTH CONTOUR, EDGE'
DO 110 I=1,ISHOR
  J=J+1
  K=1+(I-1)*INT
  X=XT(K,NST)+RAD*COS((I-1)*PI/12+AL)
  Y=YT(K,NST)+RAD*SIN((I-1)*PI/12+AL)
  Z=16.0+RAD*3/2
  WRITE(6,2)J,X,Y,Z
```

```
110 CONTINUE
C
WRITE(6,1)'C SIXTH CONTOUR, 1ST INSIDE'
DO 112 I=1,ISHOR
  J=J+1
  K=1+(I-1)*INT
  Z=16.0+RAD*3/2
  WRITE(6,2)J,XT(K,NST),YT(K,NST),Z
112 CONTINUE
C
WRITE(6,1)'C SIXTH CONTOUR, 2ND INSIDE'
DO 115 I=1,ISHOR
  J=J+1
  K=1+(I-1)*INT
  X=XT(K,NST)-RAD*COS((I-1)*PI/12+AL)/2
  Y=YT(K,NST)-RAD*SIN((I-1)*PI/12+AL)/2
  Z=16.0+RAD*3/2
  WRITE(6,2)J,X,Y,Z
115 CONTINUE
C
WRITE(6,1)'C SIXTH CONTOUR, 3RD INSIDE'
DO 120 I=1,ISHOR
  J=J+1
  K=1+(I-1)*INT
  X=(XT(K,NST)-RAD*COS((I-1)*PI/12+AL)/2)/2
  Y=(YT(K,NST)-RAD*SIN((I-1)*PI/12+AL)/2)/2
  Z=16.0+RAD*3/2
  WRITE(6,2)J,X,Y,Z
120 CONTINUE
WRITE(6,1)'C FIFTH CONTOUR, MIDPOINT'
J=J+1
Z=16.0+RAD*3/2
WRITE(6,2)J,0.0,0.0,Z
C
NN3=J
C
RETURN
END
C
C END GEOM3
C
C
SUBROUTINE PABLO3(ISHOR)
INTEGER I,J,K,ISHOR
INTEGER N1,N2,N5,EL,TYP,PROP
INTEGER*4 ETYP
DIMENSION EL(20)
C
C THIS SUBROUTINE DEFINES PAFBLOCKS (ELEMENTS) FOR STEP WITH
C WHOLE TRANSITION RADIUS
C
WRITE(6,1)'PAFBLOCKCKS'
WRITE(6,1)'BLOCK.NUMB TYPE ELEM.TYPE PROP N1 N2 N5 TOPO'
1 FORMAT(80A)
C
WRITE(6,1)'C FIRST OUTSIDE'
J=0
N1=1
N2=1
N5=5
ETYP=37110
TYP=1
```

```
PROP=20
DO 10 I=1,ISHOR/2
  EL(1)=1+(I-1)*2
  EL(2)=1+MOD(I*2,ISHOR)
  EL(3)=3*ISHOR+1+EL(1)
  EL(4)=3*ISHOR+1+EL(2)
  EL(5)=ISHOR+EL(1)
  EL(6)=ISHOR+EL(2)
  EL(7)=ISHOR+EL(3)
  EL(8)=ISHOR+EL(4)
  EL(9)=EL(1)+1
  EL(10)=0
  EL(11)=0
  EL(12)=EL(3)+1
  EL(13)=0
  EL(14)=0
  EL(15)=0
  EL(16)=0
  EL(17)=EL(5)+1
  EL(18)=0
  EL(19)=0
  EL(20)=EL(7)+1
C
  J=J+1
  WRITE(6,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,20)
2  FORMAT(7(I6,1X)/* ',10(I5,1X)/* ',10(I5,1X))
10 CONTINUE
C
WRITE(6,1)'C FIRST INSIDE, 1ST'
ETYP=37110
TYP=1
PROP=20
DO 15 I=1,ISHOR/2
  EL(1)=1+(I-1)*2+ISHOR
  EL(2)=1+MOD(I*2,ISHOR)+ISHOR
  EL(3)=3*ISHOR+1+EL(1)
  EL(4)=3*ISHOR+1+EL(2)
  EL(5)=ISHOR+EL(1)
  EL(6)=ISHOR+EL(2)
  EL(7)=ISHOR+EL(3)
  EL(8)=ISHOR+EL(4)
  EL(9)=EL(1)+1
  EL(10)=0
  EL(11)=0
  EL(12)=EL(3)+1
  EL(13)=0
  EL(14)=0
  EL(15)=0
  EL(16)=0
  EL(17)=EL(5)+1
  EL(18)=0
  EL(19)=0
  EL(20)=EL(7)+1
C
  J=J+1
  WRITE(6,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,20)
15 CONTINUE
C
WRITE(6,1)'C FIRST INSIDE, 2ND'
ETYP=37210
TYP=4
DO 20 I=1,ISHOR/2
```

```
EL(1)=3*ISHOR+1
EL(2)=2*ISHOR+1+(I-1)*2
EL(3)=2*ISHOR+1+MOD(I*2,ISHOR)
EL(4)=EL(1)+3*ISHOR+1
EL(5)=EL(2)+3*ISHOR+1
EL(6)=EL(3)+3*ISHOR+1
EL(7)=0
EL(8)=EL(2)+1
EL(9)=0
EL(10)=0
EL(11)=0
EL(12)=0
EL(13)=0
EL(14)=EL(5)+1
EL(15)=0
```

C

```
J=J+1
WRITE(6,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,15)
```

20

CONTINUE

C

C

```
WRITE(6,1)'C SECOND OUTSIDE'
```

```
N5=1
```

```
ETYP=37110
```

```
TYP=1
```

```
DO 30 I=1,ISHOR/2
```

```
EL(1)=1+(I-1)*2+3*ISHOR+1
```

```
EL(2)=1+MOD(I*2,ISHOR)+3*ISHOR+1
```

```
EL(3)=3*ISHOR+1+EL(1)
```

```
EL(4)=3*ISHOR+1+EL(2)
```

```
EL(5)=ISHOR+EL(1)
```

```
EL(6)=ISHOR+EL(2)
```

```
EL(7)=ISHOR+EL(3)
```

```
EL(8)=ISHOR+EL(4)
```

```
EL(9)=EL(1)+1
```

```
EL(10)=0
```

```
EL(11)=0
```

```
EL(12)=EL(3)+1
```

```
EL(13)=0
```

```
EL(14)=0
```

```
EL(15)=0
```

```
EL(16)=0
```

```
EL(17)=EL(5)+1
```

```
EL(18)=0
```

```
EL(19)=0
```

```
EL(20)=EL(7)+1
```

C

```
J=J+1
```

```
WRITE(6,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,20)
```

30

CONTINUE

C

```
WRITE(6,1)'C SECOND INSIDE, 1ST'
```

```
ETYP=37110
```

```
TYP=1
```

```
DO 35 I=1,ISHOR/2
```

```
EL(1)=1+(I-1)*2+ISHOR+3*ISHOR+1
```

```
EL(2)=1+MOD(I*2,ISHOR)+ISHOR+3*ISHOR+1
```

```
EL(3)=3*ISHOR+1+EL(1)
```

```
EL(4)=3*ISHOR+1+EL(2)
```

```
EL(5)=ISHOR+EL(1)
```

```
EL(6)=ISHOR+EL(2)
```

```
EL(7)=ISHOR+EL(3)
```

```
EL(8)=ISHOR+EL(4)
EL(9)=EL(1)+1
EL(10)=0
EL(11)=0
EL(12)=EL(3)+1
EL(13)=0
EL(14)=0
EL(15)=0
EL(16)=0
EL(17)=EL(5)+1
EL(18)=0
EL(19)=0
EL(20)=EL(7)+1
```

C

```
J=J+1
WRITE(6,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,20)
35 CONTINUE
```

C

```
WRITE(6,1)'C SECOND INSIDE, 2ND'
ETYP=37210
TYP=4
DO 40 I=1,ISHOR/2
  EL(1)=2*(3*ISHOR+1)
  EL(2)=2*ISHOR+1+(I-1)*2+3*ISHOR+1
  EL(3)=2*ISHOR+1+MOD(I*2,ISHOR)+3*ISHOR+1
  EL(4)=EL(1)+3*ISHOR+1
  EL(5)=EL(2)+3*ISHOR+1
  EL(6)=EL(3)+3*ISHOR+1
  EL(7)=0
  EL(8)=EL(2)+1
  EL(9)=0
  EL(10)=0
  EL(11)=0
  EL(12)=0
  EL(13)=0
  EL(14)=EL(5)+1
  EL(15)=0
```

C

```
J=J+1
WRITE(6,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,15)
40 CONTINUE
```

C

```
WRITE(6,1)'C THIRD OUTSIDE'
N5=1
ETYP=37110
TYP=1
DO 60 I=1,ISHOR/2
  EL(1)=1+(I-1)*2+2*(3*ISHOR+1)
  EL(2)=1+MOD(I*2,ISHOR)+2*(3*ISHOR+1)
  EL(3)=3*ISHOR+1+EL(1)
  EL(4)=3*ISHOR+1+EL(2)
  EL(5)=ISHOR+EL(1)
  EL(6)=ISHOR+EL(2)
  EL(7)=ISHOR+EL(3)
  EL(8)=ISHOR+EL(4)
  EL(9)=EL(1)+1
  EL(10)=0
  EL(11)=0
  EL(12)=EL(3)+1
  EL(13)=0
  EL(14)=0
  EL(15)=0
```

```
EL(16)=0
EL(17)=EL(5)+1
EL(18)=0
EL(19)=0
EL(20)=EL(7)+1

C
  J=J+1
  WRITE(6,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,20)
60 CONTINUE
C
  WRITE(6,1)'C THIRD INSIDE WEDGE'
  ETYP=37210
  TYP=4
  DO 62 I=1,ISHOR/2
    EL(1)=2*(3*ISHOR+1)+1+(I-1)*2+ISHOR
    EL(2)=3*(3*ISHOR+1)+1+(I-1)*2+2*ISHOR
    EL(3)=3*(3*ISHOR+1)+1+(I-1)*2+ISHOR
    EL(4)=2*(3*ISHOR+1)+1+MOD(I*2,ISHOR)+ISHOR
    EL(5)=3*(3*ISHOR+1)+1+MOD(I*2,ISHOR)+2*ISHOR
    EL(6)=3*(3*ISHOR+1)+1+MOD(I*2,ISHOR)+ISHOR
    EL(7)=0
    EL(8)=0
    EL(9)=0
    EL(10)=EL(1)+1
    EL(11)=EL(2)+1
    EL(12)=EL(3)+1

C
  J=J+1
  WRITE(6,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,15)
62 CONTINUE
C
  WRITE(6,1)'C THIRD INSIDE, 1ST'
  ETYP=37110
  TYP=1
  DO 65 I=1,ISHOR/2
    EL(1)=1+(I-1)*2+ISHOR+2*(3*ISHOR+1)
    EL(2)=1+MOD(I*2,ISHOR)+ISHOR+2*(3*ISHOR+1)
    EL(3)=4*ISHOR+1+EL(1)
    EL(4)=4*ISHOR+1+EL(2)
    EL(5)=ISHOR+EL(1)
    EL(6)=ISHOR+EL(2)
    EL(7)=ISHOR+EL(3)
    EL(8)=ISHOR+EL(4)
    EL(9)=EL(1)+1
    EL(10)=0
    EL(11)=0
    EL(12)=EL(3)+1
    EL(13)=0
    EL(14)=0
    EL(15)=0
    EL(16)=0
    EL(17)=EL(5)+1
    EL(18)=0
    EL(19)=0
    EL(20)=EL(7)+1

C
  J=J+1
  WRITE(6,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,20)
65 CONTINUE
C
  WRITE(6,1)'C THIRD INSIDE, 2ND'
  ETYP=37210
```

```
TYP=4
DO 70 I=1, ISHOR/2
  EL(1)=3*(3*ISHOR+1)
  EL(2)=2*ISHOR+1+(I-1)*2+2*(3*ISHOR+1)
  EL(3)=2*ISHOR+1+MOD(I*2, ISHOR)+2*(3*ISHOR+1)
  EL(4)=EL(1)+4*ISHOR+1
  EL(5)=EL(2)+4*ISHOR+1
  EL(6)=EL(3)+4*ISHOR+1
  EL(7)=0
  EL(8)=EL(2)+1
  EL(9)=0
  EL(10)=0
  EL(11)=0
  EL(12)=0
  EL(13)=0
  EL(14)=EL(5)+1
  EL(15)=0
```

C

```
  J=J+1
  WRITE(6,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,15)
70 CONTINUE
```

C

```
  WRITE(6,1)'C EXTRA IN STEP'
  ETYP=37110
  TYP=1
  DO 80 I=1, ISHOR/2
    EL(1)=3*(3*ISHOR+1)+4*ISHOR+1+1+(I-1)*2
    EL(2)=3*(3*ISHOR+1)+4*ISHOR+1+1+MOD(I*2, ISHOR)
    EL(3)=EL(1)+ISHOR
    EL(4)=EL(2)+ISHOR
    EL(5)=3*(3*ISHOR+1)+1+(I-1)*2
    EL(6)=3*(3*ISHOR+1)+1+MOD(I*2, ISHOR)
    EL(7)=EL(5)+ISHOR
    EL(8)=EL(6)+ISHOR
    EL(9)=EL(1)+1
    EL(10)=0
    EL(11)=0
    EL(12)=EL(3)+1
    EL(13)=0
    EL(14)=0
    EL(15)=0
    EL(16)=0
    EL(17)=EL(5)+1
    EL(18)=0
    EL(19)=0
    EL(20)=EL(7)+1
```

C

```
  J=J+1
  WRITE(6,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,20)
80 CONTINUE
```

C

```
  WRITE(6,1)'C FOURTH OUTSIDE'
  N5=5
  ETYP=37110
  TYP=1
  DO 90 I=1, ISHOR/2
    EL(1)=3*(3*ISHOR+1)+5*ISHOR+1+1+(I-1)*2
    EL(2)=3*(3*ISHOR+1)+5*ISHOR+1+1+MOD(I*2, ISHOR)
    EL(3)=4*ISHOR+1+EL(1)
    EL(4)=4*ISHOR+1+EL(2)
    EL(5)=ISHOR+EL(1)
    EL(6)=ISHOR+EL(2)
```

```
EL(7)=ISHOR+EL(3)
EL(8)=ISHOR+EL(4)
EL(9)=EL(1)+1
EL(10)=0
EL(11)=0
EL(12)=EL(3)+1
EL(13)=0
EL(14)=0
EL(15)=0
EL(16)=0
EL(17)=EL(5)+1
EL(18)=0
EL(19)=0
EL(20)=EL(7)+1
```

C

```
J=J+1
WRITE(6,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,20)
CONTINUE
```

90

C

```
WRITE(6,1)'C FOURTH 1ST INSIDE'
ETYP=37110
TYP=1
DO 100 I=1,ISHOR/2
  EL(1)=3*(3*ISHOR+1)+6*ISHOR+1+1+(I-1)*2
  EL(2)=3*(3*ISHOR+1)+6*ISHOR+1+1+MOD(I*2,ISHOR)
  EL(3)=4*ISHOR+1+EL(1)
  EL(4)=4*ISHOR+1+EL(2)
  EL(5)=ISHOR+EL(1)
  EL(6)=ISHOR+EL(2)
  EL(7)=ISHOR+EL(3)
  EL(8)=ISHOR+EL(4)
  EL(9)=EL(1)+1
  EL(10)=0
  EL(11)=0
  EL(12)=EL(3)+1
  EL(13)=0
  EL(14)=0
  EL(15)=0
  EL(16)=0
  EL(17)=EL(5)+1
  EL(18)=0
  EL(19)=0
  EL(20)=EL(7)+1
```

C

```
J=J+1
WRITE(6,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,20)
CONTINUE
```

100

C

```
WRITE(6,1)'C FOURTH 2ND INSIDE'
ETYP=37110
TYP=1
DO 110 I=1,ISHOR/2
  EL(1)=3*(3*ISHOR+1)+7*ISHOR+1+1+(I-1)*2
  EL(2)=3*(3*ISHOR+1)+7*ISHOR+1+1+MOD(I*2,ISHOR)
  EL(3)=4*ISHOR+1+EL(1)
  EL(4)=4*ISHOR+1+EL(2)
  EL(5)=ISHOR+EL(1)
  EL(6)=ISHOR+EL(2)
  EL(7)=ISHOR+EL(3)
  EL(8)=ISHOR+EL(4)
  EL(9)=EL(1)+1
  EL(10)=0
```

```
      EL(11)=0
      EL(12)=EL(3)+1
      EL(13)=0
      EL(14)=0
      EL(15)=0
      EL(16)=0
      EL(17)=EL(5)+1
      EL(18)=0
      EL(19)=0
      EL(20)=EL(7)+1
C
      J=J+1
      WRITE(6,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,20)
110  CONTINUE
C
      WRITE(6,1)'C FOURTH, 3RD INSIDE'
      ETYP=37210
      TYP=4
      DO 120 I=1,ISHOR/2
        EL(1)=3*(3*ISHOR+1)+5*ISHOR+1+4*ISHOR+1
        EL(2)=3*(3*ISHOR+1)+8*ISHOR+1+1+(I-1)*2
        EL(3)=3*(3*ISHOR+1)+8*ISHOR+1+1+MOD(I*2,ISHOR)
        EL(4)=EL(1)+4*ISHOR+1
        EL(5)=EL(2)+4*ISHOR+1
        EL(6)=EL(3)+4*ISHOR+1
        EL(7)=0
        EL(8)=EL(2)+1
        EL(9)=0
        EL(10)=0
        EL(11)=0
        EL(12)=0
        EL(13)=0
        EL(14)=EL(5)+1
        EL(15)=0
C
      J=J+1
      WRITE(6,2)J,TYP,ETYP,PROP,N1,N2,N5,(EL(K),K=1,15)
120  CONTINUE
C
C
      WRITE(6,1)'MESH'
      WRITE(6,1)'REFE SPAC.LIST'
      WRITE(6,1)'1 1'
      WRITE(6,1)'2 2'
      WRITE(6,1)'3 3'
      WRITE(6,1)'4 4'
      WRITE(6,1)'5 5'
      WRITE(6,1)'6 6'
      WRITE(6,1)'7 7'
      WRITE(6,1)'8 8'
      WRITE(6,1)'C '
      WRITE(6,1)'MATERIAL'
      WRITE(6,1)'MATE.NUMB E NU'
      WRITE(6,1)'20 110000 0.35'
C
C
      RETURN
      END
C
C END PABLO3
C
      SUBROUTINE RES3(ISHOR,NN3)
```

```
      INTEGER I, ISHOR, NN3
C
C THIS SUBROUTINE IMPOSES CONSTRAINTS ON THE MODEL OF STEP WITH
C WHOLE TRANSITION RADIUS
C
      WRITE(6,1) 'RESTRAINTS'
      WRITE(6,1) 'NODE.NUMB DIRECTION'
1     FORMAT(80A)
C
      DO 10 I=NN3-4*ISHOR, NN3
          WRITE(6,2) I, 0
2         FORMAT(I6,1X,I6)
10    CONTINUE
C
      RETURN
      END
C
C END RES3
C
      SUBROUTINE LOA3(XT, YT, NST, XP, ISHOR, NPPS)
      INTEGER NST, ISHOR, NPPS, I
      REAL D1, D2, F1, F2, XP, X, Y, PI
      DIMENSION XT(73,30), YT(73,30)
C
C THIS SUBROUTINE CALCULATES LOADS FOR STEP WITH WHOLE
C TRANSITION RADIUS
C
      PI=4.0*ATAN(1.0)
      X=XT(1, NST)
      Y=YT(1, NST)
      D1=SQRT(X**2+Y**2)
C
      X=XT((NPPS-1)/2+1, NST)
      Y=YT((NPPS-1)/2+1, NST)
      D2=SQRT(X**2+Y**2)
C
      F1=-0.5/D1
      F2=0.5/D2
      IF(XP.LE.0.0) THEN
          F1=-F1
          F2=-F2
      END IF
C
      WRITE(6,1) 'LOADS'
      WRITE(6,1) 'NODE.NUMB DIRE.OF.LOAD VALU.OF.LOAD'
1     FORMAT(80A)
C
      WRITE(6,2) 1, 3, F1
      I=(NPPS-1)/2+1
      WRITE(6,2) I, 3, F2
C
2     FORMAT(I6,1X,I6,1X,E15.7)
C
      WRITE(6,1) 'END.OF.DATA'
      RETURN
      END
C
C END LOA3
C
```

APPENDIX 3. Simple model. Program PROCO

Program PROCO

```
C PROGRAM FOR THE CALCULATION OF BENDING STRESSES IN PROSTHESES
C USING SIMPLE BENDING THEORY
C
C
C PROGRAM PROCO
C CHARACTER NAME*10
C INTEGER STEP,L1,L2,CCD,UEB,NPPS,NSCH
C INTEGER ICHO,LEVEL
C INTEGER M,I
C REAL M1,M2,INAX,INAY,INAXY,XP,YP,ZP,ZPN,XPN
C REAL DELC,BETA,P,RAD,D1,D2,PI,DUM,TORQ
C REAL ES,EC,DB
C DIMENSION NSCN(5),SCF(8,30,2)
C DIMENSION X(73,30),Y(73,30),Z(73,30),XO(73,30),YO(73,30),
C +XT(73,30),YT(73,30)
C DIMENSION XPL(30),YPL(30),ANG(30),CMID(30,3)
C DIMENSION INAX(30),INAY(30),INAXY(30),A(30,3),XBAR(30),YBAR(30)
C DIMENSION M1(30),M2(30)
C DIMENSION SSUM(73,30),FSUM(73,30)
C DIMENSION SMAX(30),SMIN(30),IMAX(30),MMAX(30),IMIN(30),MMIN(30)
C +,SFMAX(30),SFMIN(30),IFMIN(30),MFMIN(30),IFMAX(30),MFMAX(30)
C DIMENSION TMAX(30,3)
C
C
C READ DATA FROM THE GEOMETRY INPUT FILE AND FILE 'SCFDAT'
C WITH STRESS CONCENTRATION FACTORS
C
C CALL READAT(X,Y,Z,NSCN,XP,YP,ZP,STEP,L1,L2,UEB,CCD,NSCH,
C +NPPS,NAME,SCF)
C
C
C OPEN(9,FILE='STRESS')
3333 CONTINUE
C
C BETA: TILT ANGEL OF THE PROSTHESIS 10 DEGREES
C
C PI=4*ATAN(1.0)
C PRINT*, 'TILTANGLE OF PROSTHESIS IN DEG ? '
C READ(*,*)BETA
C BETA=BETA*PI/180
C
C P: LOAD OF THE PROSTHESIS IN NEWTONS
C
C PRINT*, 'ABSOLUTE VALUE OF THE LOAD IN [N] ? '
C READ(*,*)P
C
C RAD: VALUE OF THE TRANSITION RADIUS
C
C PRINT*, 'VALUE OF THE TRANSITION RADIUS [MM] ? '
C READ(*,*)RAD
C
C LEVEL: NUMBER OF THE CONTOUR AT EMBEDDING LEVEL
```

```
C
PRINT*, ' NUMBER OF CONTOUR AT THE EMBEDDING LEVEL ?'
READ(*,*)LEVEL
IF (LEVEL.GT.NSCN(4)) THEN
  LEVEL=NSCN(4)
END IF
IF (LEVEL.LT.0) THEN
  LEVEL=0
END IF

C
C
PRINT*, 'ESTEM = ? '
READ(*,*)ES
PRINT*, 'ECEMENT = ? '
READ(*,*)EC
PRINT*, 'DIAMETER OF EMBEDDING = ? '
READ(*,*)DB

C
C DEFINE NEW POINT COORDINATES AROUND CENTRE POINTS
C
  CALL SECT(X,Y,XO,YO,Z,NPPS,NSCN(4),CMID,ANG,XPL,YPL,XP,YP)
C
C CALCULATE COORDINATES OF CENTROIDS (POINTS OF GRAVITY) AND
C SECOND MOMENTS OF AREA ABOUT XX AND YY
C
  CALL CENTRO(NSCN(4),X,Y,NPPS,XBAR,YBAR,INAX,INAY,INAXY,XT,YT,
+XO,YO,A)
C
C
C CALCULATE APPLIED MOMENTS M1,M2 FOR PROSTHESIS WITHOUT EMBEDDING
C
  CALL MPROT(NSCN(4),XPL,YPL,ZP,P,XBAR,YBAR,Z,BETA,ANG,
+M1,M2,INAX,INAY,INAXY)
C
C CALCULATE MOMENTS FOR EMBEDDED PROSTHESIS
C
  CALL MPROEM(NSCN(4),LEVEL,XPL(LEVEL),P,XBAR(LEVEL),
+Z,BETA,ANG(LEVEL),M1,M2,INAX,INAY,X,Y,ES,EC,DB)
C
C
C CALCULATE STRESSES DUE TO MOMENTS AND SHEAR FORCE
C
  CALL COSTRE(NSCN(4),ANG,LEVEL,BETA,INAX,
+INAY,M1,M2,SSUM,A,P,XT,YT)
C
C CALCULATE STRESS CONCENTRATION FACTOR AND MULTIPLY STRESSES
C WITH THESE
C
  CALL CONCTR(NSCN(4),XBAR,YBAR,ANG,CMID,XO,YO,SSUM,FSUM,SCF,
+RAD)
C
C FIND MINIMUM AND MAXIMUM STRESSES AND FACTORED STRESSES ALONG
C EACH CONTOUR
C
  CALL SSORT(NSCN(4),NPPS,SSUM,FSUM,IMIN,MMIN,IMAX,MMAX,SMAX,
+SMIN,IFMIN,MFMIN,IFMAX,MFMAX,SFMAX,SFMIN)
C
C
WRITE(9,1000) ' ANALYSIS OF PROSTHESIS ',NAME
1000 FORMAT(80A)
C
PRINT*, ' ANALYSIS OF ',NAME
```

```
C
C
WRITE(9,1100)
WRITE(*,1100)
1100 FORMAT(// '          MAXIMUM AND MINIMUM STRESSES          '/')
WRITE(9,1200)
WRITE(*,1200)
1200 FORMAT('          STEP POINT MAXSTRESS  '/')
C
DO 10 M=1,NSCN(4)-1
WRITE(9,1300) MMAX(M),IMAX(M),SMAX(M)
WRITE(*,1300) MMAX(M),IMAX(M),SMAX(M)
1300 FORMAT(8X,2I5,F10.3)
10 CONTINUE
WRITE(9,1400)
WRITE(*,1400)
1400 FORMAT('          STEP POINT MINSTRESS  '/')
DO 20 M=1,NSCN(4)-1
WRITE(9,1300) MMIN(M),IMIN(M),SMIN(M)
WRITE(*,1300) MMIN(M),IMIN(M),SMIN(M)
20 CONTINUE
C
WRITE(9,1500)
WRITE(*,1500)
1500 FORMAT(// '          MAXIMUM AND MINIMUM FACTORED STRESSES  '/')
WRITE(9,1200)
WRITE(*,1200)
C
DO 30 M=1,NSCN(4)-1
WRITE(9,1300) MFMAX(M),IFMAX(M),SFMAX(M)
WRITE(*,1300) MFMAX(M),IFMAX(M),SFMAX(M)
30 CONTINUE
WRITE(9,1400)
WRITE(*,1400)
DO 40 M=1,NSCN(4)-1
WRITE(9,1300) MFMIN(M),IFMIN(M),SFMIN(M)
WRITE(*,1300) MFMIN(M),IFMIN(M),SFMIN(M)
40 CONTINUE
C
C
PRINT*, 'DEFAULTS FOR THIS RUN WERE:'
PRINT*, 'TILTANGLE      ',BETA*45/ATAN(1.0)
PRINT*, 'LOAD              ',P
PRINT*, 'RADIUS             ',RAD
PRINT*, 'EMB. LEVEL        ',LEVEL
C
WRITE(9,1000) ' '
WRITE(9,1000) '  LOAD          RADIUS          TILTANGLE          EMB.LEV '
WRITE(9,1000) ' '
WRITE(9,1700) P,RAD,BETA*45/ATAN(1.0),LEVEL
1700 FORMAT(F10.4,4X,F10.4,4X,F10.4,4X,I3)
C
C
C TORSION COMPUTATION
C
DO 56 M=1,NSCN(4)-1
CALL TORO(X,Y,M,TMAX)
C
C CALCULATE TORSION MOMENTS
C
TORQ=P*SIN(BETA)*(YP-CMID(M,2))
TMAX(M,2)=TMAX(M,2)*TORQ
```

```
C
56 CONTINUE
C
WRITE(9,1800)
WRITE(*,1800)
1800 FORMAT('/', STEP POINT TOR.STRESS '/')
DO 57 M=1,NSCN(4)-1
WRITE(9,1900)M,TMAX(M,1),TMAX(M,2)
WRITE(*,1900)M,TMAX(M,1),TMAX(M,2)
1900 FORMAT(4X,I5,4X,F10.3,4X,F10.3)
C
57 CONTINUE
C
C
C REDESIGN
C
C
C
PRINT*, 'REDESIGN OPTIONS'
PRINT*, ' 1 INCREASE CCD ANGLE'
PRINT*, ' 2 MAKE CONE SHORTER'
PRINT*, ' 3 NEW PARAMETERS'
PRINT*, ' 4 STOP'
PRINT*, 'ENTER OPTION NUMBER'
READ(*,*) ICHO
IF (ICHO.EQ.1) THEN
PRINT*, 'ENTER INCREASE IN CCD-ANGLE IN DEGREES'
READ(*,*) DELC
DELC=DELC*PI/180
ZPN=ABS(XP)*TAN((CCD-90)*PI/180)
DUM=ZP-ZPN
IF (XP.GT.0.0) THEN
XPN=XP*COS(DELC)-ZPN*SIN(DELC)
ZP=XP*SIN(DELC)+ZPN*COS(DELC)
ZP=ZP+DUM
ELSE
XPN=XP*COS(DELC)+ZPN*SIN(DELC)
ZP=-XP*SIN(DELC)+ZPN*COS(DELC)
ZP=ZP+DUM
END IF
XP=XPN
DO 50 I=1,NSCN(4)
XPL(I)=XP-CMID(I,1)
YPL(I)=YP-CMID(I,2)
D1=YPL(I)*COS(ANG(I))-XPL(I)*SIN(ANG(I))
D2=YPL(I)*SIN(ANG(I))+XPL(I)*COS(ANG(I))
XPL(I)=D2
YPL(I)=D1
50 CONTINUE
GOTO 3333
END IF
IF (ICHO.EQ.2) THEN
PRINT*, 'ENTER CHANGE IN THE CONE LENGHT IN MM'
READ(*,*) DELC
ZPN=ZP-DELC*SIN((180-CCD)*PI/180)
IF (XP.GT.0.0) THEN
XPN=XP-DELC*COS((180-CCD)*PI/180)
ELSE
XPN=XP+DELC*COS((180-CCD)*PI/180)
END IF
XP=XPN
ZP=ZPN
```

```
      DO 60 I=1,NSCN(4)
        XPL(I)=XP-CMID(I,1)
        YPL(I)=YP-CMID(I,2)
        D1=YPL(I)*COS(ANG(I))-XPL(I)*SIN(ANG(I))
        D2=YPL(I)*SIN(ANG(I))+XPL(I)*COS(ANG(I))
        XPL(I)=D2
        YPL(I)=D1
60     CONTINUE
      GOTO 3333
    END IF
  C
  IF(ICHO.EQ.3) THEN
    GOTO 3333
  END IF
  C
  C
  STOP
  END
  C
  C END MAIN PROGRAM
  C
  C
  C
  SUBROUTINE READAT(X,Y,Z,NSCN,XP,YP,ZP,STEP,L1,L2,UEB,CCD,NSCH,
+NPPS,NAME,SCF)
  CHARACTER NAME*10
  INTEGER STEP,NSCH,NPPS,CCD,L1,L2,UEB,I,J,M
  REAL XP,YP,ZP
  DIMENSION X(73,30),Y(73,30),Z(73,30)
  DIMENSION NSCN(5),SCF(8,30,2)
  C
  PRINT*,'NAME OF THE INPUT FILE'
  READ(*,55)NAME
55  FORMAT(A10)
  OPEN(2,FILE=NAME)
  READ(2,*)STEP
  DO 100 I=1,5
    READ(2,*) NSCN(I)
100  CONTINUE
  READ(2,*) NSCH
  READ(2,*) NPPS
  READ(2,*) CCD
  READ(2,*) L1
  READ(2,*) L2
  READ(2,*) UEB
  DO 110 I=1,NSCH
    DO 120 J=1,NPPS
      READ(2,*) X(J,I)
      READ(2,*) Y(J,I)
      READ(2,*) Z(J,I)
120  CONTINUE
110  CONTINUE
  C
  READ(2,*)XP
  READ(2,*)YP
  READ(2,*)ZP
  PRINT*,'CENTRE OF THE HEAD'
  PRINT*,XP,YP,ZP
  C
  CLOSE(2)
  C
  C READ DATA FROM SCFDAT: STRESS CONCENTRATION FACTORS
```

```
C
OPEN(3,FILE='SCFDAT')
DO 300 I=1,8
  DO 310 J=1,30
    READ(3,*) (SCF(I,J,M),M=1,2)
310  CONTINUE
300  CONTINUE
C
CLOSE(3)
C
RETURN
END
C
C END READAT
C
C
C
SUBROUTINE SECT(X,Y,XO,YO,Z,NPPS,NSCN4,CMID,ANG,XPL,YPL,XP,
+YP)
INTEGER I,J,K,NSCN4
REAL PI,X3,X1,X2,Y3,Y1,Y2,A1,A2,B1,B2,D1,D2,W,XP,YP
DIMENSION X(73,30),Y(73,30),Z(73,30),SEC(0:72,3),CMID(30,3)
DIMENSION XO(73,30),YO(73,30)
DIMENSION WEIG(73),ANG(30),XPL(30),YPL(30)
C
C
DO 100 I=1,NSCN4
  DO 110 J=1,NPPS
    SEC(J-1,1)=X(J,I)
    SEC(J-1,2)=Y(J,I)
    SEC(J-1,3)=Z(J,I)
    XO(J,I)=X(J,I)
    YO(J,I)=Y(J,I)
110  CONTINUE
C COMPUTING WEIGHTS
W=0.0
DO 130 J=0,NPPS-1
  D1=SQRT((SEC(J,1)-SEC(MOD(J+1,NPPS-1),1))**2+(SEC(J,2)-
+ SEC(MOD(J+1,NPPS-1),2))**2)
  D2=SQRT((SEC(J,1)-SEC(MOD(J+NPPS-2,NPPS-1),1))**2+(SEC(J,2)-
+ SEC(MOD(J+NPPS-2,NPPS-1),2))**2)
  WEIG(J+1)=(D1+D2)/2
  W=W+WEIG(J+1)
130  CONTINUE
C COMPUTE THE MIDPOINTS
DO 140 K=1,3
  CMID(I,K)=0.0
140  CONTINUE
DO 145 J=1,NPPS
  CMID(I,1)=WEIG(J)*SEC(J-1,1)+CMID(I,1)
  CMID(I,2)=WEIG(J)*SEC(J-1,2)+CMID(I,2)
145  CONTINUE
CMID(I,1)=CMID(I,1)/W
CMID(I,2)=CMID(I,2)/W
CMID(I,3)=SEC(1,3)
C
C FIND NEW POINTS ON THE CONTOUR IN 5 DEGREE STEPS
C AROUND CMIDS STARTING WITH THE POINT NO. 1
PI=4*ATAN(1.0)
SEC(0,1)=X(1,I)
SEC(0,2)=Y(1,I)
K=1
```

```
DO 210 J=0,NPPS-2
  X1=SEC(J,1)-CMID(I,1)
  Y1=SEC(J,2)-CMID(I,2)
  D1=SQRT(X1**2+Y1**2)
99  X2=X(MOD(K,NPPS)+1,I)-CMID(I,1)
  Y2=Y(MOD(K,NPPS)+1,I)-CMID(I,2)
  D2=SQRT(X2**2+Y2**2)
  IF((X1*X2+Y1*Y2)/(D1*D2)).GT.(COS(PI/36)))THEN
    K=K+1
    GOTO 99
  END IF
  X3=X1*COS(PI/36)-Y1*SIN(PI/36)
  Y3=X1*SIN(PI/36)+Y1*COS(PI/36)
  X3=X3+CMID(I,1)
  Y3=Y3+CMID(I,2)
  IF((ABS(X3-CMID(I,1)).GT.1E-12))THEN
    A1=(Y3-CMID(I,2))/(X3-CMID(I,1))
    B1=Y3-A1*X3
    IF((ABS(X(MOD(K,NPPS)+1,I)-SEC(J,1)).GT.1E-12))THEN
      A2=(Y(MOD(K,NPPS)+1,I)-SEC(J,2))/(X(MOD(K,NPPS)+1,I)
+      -SEC(J,1))
      B2=Y(MOD(K,NPPS)+1,I)-A2*X(MOD(K,NPPS)+1,I)
      SEC(J+1,1)=(B2-B1)/(A1-A2)
      SEC(J+1,2)=A1*SEC(J+1,1)+B1
    ELSE
      A2=0.0
      B2=Y(MOD(K,NPPS)+1,I)
      SEC(J+1,1)=(B2-B1)/A1
      SEC(J+1,2)=B2
    END IF
  ELSE
    A1=0.0
    B1=Y3
    IF((ABS(X(MOD(K,NPPS)+1,I)-SEC(J,1)).GT.1E-12))THEN
      A2=(Y(MOD(K,NPPS)+1,I)-SEC(J,2))/(X(MOD(K,NPPS)+1,I)
+      -SEC(J,1))
      B2=Y(MOD(K,NPPS)+1,I)-A2*X(MOD(K,NPPS)+1,I)
      SEC(J+1,1)=(B1-B2)/A2
      SEC(J+1,2)=B1
    ELSE
      SEC(J+1,1)=X(MOD(K,NPPS)+1,I)
      SEC(J+1,2)=Y(MOD(K,NPPS)+1,I)
    END IF
  END IF
210  CONTINUE
C  WRITE NEW POINTS
  DO 220 J=1,NPPS
    X(J,I)=SEC(J-1,1)-CMID(I,1)
    Y(J,I)=SEC(J-1,2)-CMID(I,2)
    XO(J,I)=XO(J,I)-CMID(I,1)
    YO(J,I)=YO(J,I)-CMID(I,2)
220  CONTINUE
C
  XPL(I)=XP-CMID(I,1)
  YPL(I)=YP-CMID(I,2)
C
C  ROTATE SO THAT THE FIRST POINT IS ON Y=0
C
C  CALCULATE ANGLE OF ROTATION ANG
C
  D1=X(1,I)/(SQRT(X(1,I)**2+Y(1,I)**2))
  D2=Y(1,I)/(SQRT(X(1,I)**2+Y(1,I)**2))
```

```
IF (D1.GE.0.) THEN
  IF (D2.GE.0.) THEN
    ANG(I)=ACOS(D1)
  ELSE
    ANG(I)=-ABS(ACOS(D1))
  END IF
ELSE
  IF (D2.GE.0.) THEN
    ANG(I)=ABS(ACOS(D1))
  ELSE
    ANG(I)=-ABS(ACOS(D1))
  END IF
END IF

C
C ROTATE BY ANG
C
DO 230 J=1,NPPS
  D1=Y(J,I)*COS(ANG(I))-X(J,I)*SIN(ANG(I))
  D2=Y(J,I)*SIN(ANG(I))+X(J,I)*COS(ANG(I))
  X(J,I)=D2
  Y(J,I)=D1
  D1=YO(J,I)*COS(ANG(I))-XO(J,I)*SIN(ANG(I))
  D2=YO(J,I)*SIN(ANG(I))+XO(J,I)*COS(ANG(I))
  XO(J,I)=D2
  YO(J,I)=D1
230 CONTINUE
C
C NEW COORDINATES OF THE CENTR OF THE HEAD: XPL, YPL
C
  D1=YPL(I)*COS(ANG(I))-XPL(I)*SIN(ANG(I))
  D2=YPL(I)*SIN(ANG(I))+XPL(I)*COS(ANG(I))
  XPL(I)=D2
  YPL(I)=D1
C
100 CONTINUE
RETURN
END
C
C END SECT
C
C
C
C
SUBROUTINE CENTRO(NSCN4,X,Y,NPPS,XBAR,YBAR,INAX,INAY,INAXY,XT,
+YT,XO,YO,A)
  INTEGER NSCN4,NPPS
  INTEGER I,II,J,M
  REAL DELX,B,YMIN,YMAX,H1,H2,X1,X2,Y1,Y2,A1,A2,IX1,IX2,IY1,IY2
  REAL IXY1,IXY2,IXX,IYY,IXYXY,INAX,INAY,INAXY
  DIMENSION X(73,30),Y(73,30),XBAR(30),YBAR(30),INAX(30),INAY(30)
+,INAXY(30),XT(73,30),YT(73,30),XO(73,30),YO(73,30)
  DIMENSION A(30,3),AX(30,3),AY(30,3),IXX(30,3),IYY(30,3),
+IXYXY(30,3),XMAX(4,30),IPOINT(4,30)
C
C FIND MAXIMUM X FOR EACH QUADRANT
C
C
DO 10 M=1,NSCN4
  I=0
  DO 11 II=1,4
    XMAX(II,M)=0.
  DO 12 J=1,18
    I=I+1
```

```
        IF(ABS(X(I,M)).GT.ABS(XMAX(II,M))) THEN
          XMAX(II,M)=X(I,M)
          IPOINT(II,M)=I
        END IF
12      CONTINUE
11      CONTINUE
10      CONTINUE
C
C LOOP ON NUMBER OF STEPS
C
      DO 20 M=1,NSCN4
C
C LOOP ON NUMBER OF POINTS AROUND PERIPHERY OF STEP
C
C CALCULATION OF STRIP PROPERTIES
C
      DO 21 I=1,NPPS-1
        DELX=ABS(X(I+1,M)-X(I,M))
        B=DELX
C
C 'NEGATIVE' AREAS OF CROSS-SECTION
C
        IF(I.LT.19) THEN
          IF((X(I,M).LT.XMAX(1,M)).AND.(I.LT.IPOINT(1,M))) THEN
            B=-DELX
          END IF
        END IF
        IF((I.GT.19).AND.(I.LT.37)) THEN
          IF((ABS(X(I,M)).LT.ABS(XMAX(2,M))).AND.(I.GT.IPOINT(2,M))) THEN
            B=-DELX
          END IF
        END IF
        IF((I.GT.37).AND.(I.LT.55)) THEN
          IF((ABS(X(I,M)).LT.ABS(XMAX(3,M))).AND.(I.LT.IPOINT(3,M))) THEN
            B=-DELX
          END IF
        END IF
        IF(I.GT.55) THEN
          IF((X(I,M).LT.XMAX(4,M)).AND.(I.GT.IPOINT(4,M))) THEN
            B=-DELX
          END IF
        END IF
        IF((ABS(Y(I,M)).LT.ABS(Y(I+1,M))) THEN
          YMIN=Y(I,M)
          YMAX=Y(I+1,M)
        ELSE
          YMIN=Y(I+1,M)
          YMAX=Y(I,M)
        END IF
        H1=ABS(YMIN)
        H2=ABS(YMAX)
        X1=(X(I,M)+X(I+1,M))/2.
        Y1=YMIN/2.
        Y2=YMAX/2.
        A1=B*H1
        A2=B*H2
        X2=X1
        IX1=(B*H1**3)/3.
        IX2=(B*H2**3)/3.
        IY1=(H1*B**3)/12. + A1*X1**2
        IY2=(H2*B**3)/12. + A2*X2**2
        IXY1=A1*X1*Y1
```

```
IXY2=A2*X2*Y2
C
C CALCULATION OF STEP PROPERTIES
C
  A(M,1)=A(M,1)+A1
  A(M,2)=A(M,2)+A2
  AX(M,1)=AX(M,1)+A1*X1
  AX(M,2)=AX(M,2)+A2*X2
  AY(M,1)=AY(M,1)+A1*Y1
  AY(M,2)=AY(M,2)+A2*Y2
  IXX(M,1)=IXX(M,1)+IX1
  IXX(M,2)=IXX(M,2)+IX2
  IYY(M,1)=IYY(M,1)+IY1
  IYY(M,2)=IYY(M,2)+IY2
  IXYXY(M,1)=IXYXY(M,1)+IXY1
  IXYXY(M,2)=IXYXY(M,2)+IXY2
21  CONTINUE
C
C AVERAGE MAX AND MIN PROPERTIES
C
  A(M,3)=(A(M,1)+A(M,2))/2.
  AX(M,3)=(AX(M,1)+AX(M,2))/2.
  AY(M,3)=(AY(M,1)+AY(M,2))/2.
  IXX(M,3)=(IXX(M,1)+IXX(M,2))/2.
  IYY(M,3)=(IYY(M,1)+IYY(M,2))/2.
  IXYXY(M,3)=(IXYXY(M,1)+IXYXY(M,2))/2.
C
C CENTROID POSITION
C
  XBAR(M)=AX(M,3)/A(M,3)
  YBAR(M)=AY(M,3)/A(M,3)
C
C NOMINAL MOMENTS OF AREA
C
  INAX(M)=IXX(M,3)-A(M,3)*YBAR(M)**2
  INAY(M)=IYY(M,3)-A(M,3)*XBAR(M)**2
  INAXY(M)=IXYXY(M,3)-A(M,3)*XBAR(M)*YBAR(M)
20  CONTINUE
C
C POINT COORDINATES ABOUT PRINCIPAL AXES
C
  DO 30 M=1,NSCN4
    DO 31 I=1,NPPS
      XT(I,M)=XO(I,M)-XBAR(M)
      YT(I,M)=YO(I,M)-YBAR(M)
31  CONTINUE
30  CONTINUE
C
  RETURN
  END
C
C END CENTRO
C
C
C
C
  SUBROUTINE MPROT(NSCN4,XPL,YPL,ZP,P,XBAR,YBAR,Z,BETA,
+ANG,M1,M2,INAX,INAY,INAXY)
  INTEGER NSCN4,M
  REAL ZP,P,BETA,M1,M2,INAX,INAY,INAXY
  REAL MX,MY,XL,YL,ZL
  DIMENSION XPL(30),YPL(30),XBAR(30),YBAR(30),Z(73,30),
+ANG(30),M1(30),M2(30),INAX(30),INAY(30),INAXY(30)
```

```

C
DO 10 M=1,NSCN4
  XL=XPL(M)-XBAR(M)
  YL=YPL(M)-YBAR(M)
  ZL=ZP-Z(1,M)
C
  IF(XL.LT.0.0) THEN
    XL=XL*COS(BETA)+ZL*SIN(BETA)*COS(ANG(M))
    YL=-YL*COS(BETA)+ZL*SIN(BETA)*SIN(ANG(M))
  ELSE
    XL=XL*COS(BETA)-ZL*SIN(BETA)*COS(ANG(M))
    YL=-YL*COS(BETA)-ZL*SIN(BETA)*SIN(ANG(M))
  END IF
C
  MX=P*YL
  MY=P*XL
C
  M1(M)=(MX+INAXY(M)*MY/INAY(M))/(1-INAXY(M)**2/INAX(M)/INAY(M))
  M2(M)=(MY+INAXY(M)*MX/INAX(M))/(1-INAXY(M)**2/INAX(M)/INAY(M))
10 CONTINUE
C
  RETURN
  END
C
C END MPROT
C
C
SUBROUTINE MPROEM(NSCN4,LEVEL,XPLLEV,P,
+XBARLV,Z,BETA,ANGLEV,M1,M2,INAX,INAY,X,Y,ES,EC,DB)
  INTEGER NSCN4,LEVEL,M
  REAL XPLLEV,P,XBARLV,BETA,M1,M2,ES,EC,DB
  REAL INAX,INAY,ANGLEV
  REAL SX,SY,XL,YL,ZL
  DIMENSION Z(73,30),X(73,30),Y(73,30)
  DIMENSION M1(30),M2(30),INAX(30),INAY(30),INAXY(30)
C
C FINITE DIFFERENCE METHOD FOR BEAMS ON EL. FOUNDATOIN
C
  IF(LEVEL.GT.0) THEN
    XL=XPLLEV-XBARLV
    DO 10 M=1,LEVEL
C
      IF(XL.LT.0.0) THEN
        SX=P*SIN(BETA)*COS(ANGLEV)
        SY=P*SIN(BETA)*SIN(ANGLEV)
      ELSE
        SX=-P*SIN(BETA)*COS(ANGLEV)
        SY=-P*SIN(BETA)*SIN(ANGLEV)
      END IF
      CALL ELBEAM(X,Y,Z,LEVEL,INAX,INAY,M1,M2,SX,SY,ES,EC,DB)
10 CONTINUE
    END IF
C
  RETURN
  END
C
C END MPROEM
C
C
SUBROUTINE COSTRE(NSCN4,ANG,LEVEL,BETA,
+INAX,INAY,M1,M2,SSUM,A,P,XT,YT)
  INTEGER NSCN4,LEVEL,M,I

```

```
REAL P,BETA,M1,M2,INAX,INAY
DIMENSION ANG(30),INAX(30),INAY(30),M1(30),M2(30)
DIMENSION SSUM(73,30),A(30,3),XT(73,30),YT(73,30)
DIMENSION S1(73,30),S2(73,30),SL(30)

C
C STRESSES DUE TO M1 AND M2 SEPARATELY
C
DO 10 M=1,NSCN4
DO 20 I=1,72
IF (M.GE.LEVEL) THEN
S1(I,M)=M1(M)*YT(I,M)/INAX(M)
S2(I,M)=-M2(M)*XT(I,M)/INAY(M)
SL(M)=-P/A(M,3)*COS(BETA)
SSUM(I,M)=S1(I,M)+S2(I,M)+SL(M)
ELSE
S1(I,M)=M1(M)*YT(I,M)/INAX(M)
S2(I,M)=-M2(M)*XT(I,M)/INAY(M)
SL(M)=0.0
SSUM(I,M)=S1(I,M)+S2(I,M)+SL(M)
END IF
20 CONTINUE
10 CONTINUE
RETURN
END

C
C END COSTRE
C
C
C
C
SUBROUTINE CONCTR(NSCN4,XBAR,YBAR,ANG,CMID,XO,YO,
+SSUM,FSUM,SCF,RAD)
INTEGER NSCN4
INTEGER M,I,MSTEP,IPNT
REAL XCEN,YCEN,RAT1,RAT2,DMIN,DMAX,K,RAD
DIMENSION XBAR(30),YBAR(30),ANG(30),CMID(30,3),SCF(8,30,2)
DIMENSION XO(73,30),YO(73,30),SSUM(73,30),FSUM(73,30)
DIMENSION C1(73,30),C2(73,30),K(73,30)

C
DO 10 M=1,NSCN4-1
XCEN=XBAR(M)*COS(ANG(M))-YBAR(M)*SIN(ANG(M))
YCEN=XBAR(M)*SIN(ANG(M))+YBAR(M)*COS(ANG(M))
XCEN=XCEN+CMID(M,1)
YCEN=YCEN+CMID(M,2)
DO 20 I=1,72
C1(I,M+1)=XO(I,M+1)*COS(ANG(M+1))-YO(I,M+1)*SIN(ANG(M+1))
C2(I,M+1)=XO(I,M+1)*SIN(ANG(M+1))+YO(I,M+1)*COS(ANG(M+1))
C1(I,M)=XO(I,M)*COS(ANG(M))-YO(I,M)*SIN(ANG(M))
C2(I,M)=XO(I,M)*SIN(ANG(M))+YO(I,M)*COS(ANG(M))
C1(I,M+1)=C1(I,M+1)+CMID(M+1,1)
C2(I,M+1)=C2(I,M+1)+CMID(M+1,2)
C1(I,M)=C1(I,M)+CMID(M,1)
C2(I,M)=C2(I,M)+CMID(M,2)

C
DMAX=2.0*SQRT((C1(I,M+1)-XCEN)**2+(C2(I,M+1)-YCEN)**2)
DMIN=2.0*SQRT((C1(I,M)-XCEN)**2+(C2(I,M)-YCEN)**2)
RAT1=DMAX/DMIN
RAT2=RAD/DMIN

C
IPNT=I
MSTEP=M
CALL SCFINT(RAT1,RAT2,IPNT,MSTEP,K,SCF)
FSUM(I,M)=K(I,M)*SSUM(I,M)
```

```
20 CONTINUE
10 CONTINUE
RETURN
END
C
C END CONCTR
C
C
SUBROUTINE SSORT(NSCN4,NPPS,SSUM,FSUM,IMIN,MMIN,IMAX,MMAX,SMAX,
+SMIN,IFMIN,MFMIN,IFMAX,MFMAX,SFMAX,SFMIN)
INTEGER NSCN4,NPPS,M,I
REAL LOW,HIGH
DIMENSION SSUM(73,30),FSUM(73,30)
DIMENSION IMIN(30),MMIN(30),IMAX(30),MMAX(30),SMAX(30),SMIN(30)
DIMENSION IFMIN(30),MFMIN(30),IFMAX(30),MFMAX(30),SFMAX(30),
+SFIN(30)
C
C MAXIMUM AND MINIMUM STRESSES
C
HIGH=0.
LOW=0.
DO 11 M=1,NSCN4-1
IMIN(M)=1
MMIN(M)=M
IMAX(M)=1
MMAX(M)=M
SMAX(M)=SSUM(1,M)
SMIN(M)=SSUM(1,M)
DO 12 I=1,NPPS-1
IF(SSUM(I,M).LT.SMIN(M)) THEN
SMIN(M)=SSUM(I,M)
IMIN(M)=I
END IF
IF(SSUM(I,M).GT.SMAX(M)) THEN
SMAX(M)=SSUM(I,M)
IMAX(M)=I
END IF
12 CONTINUE
IF(SMAX(M).GT.HIGH) THEN
HIGH=SMAX(M)
END IF
IF(SMIN(M).LT.LOW) THEN
LOW=SMIN(M)
END IF
11 CONTINUE
C
C MAXIMUM AND MINIMUM FACTORED STRESSES
C
HIGH=0.
LOW=0.
DO 15 M=1,NSCN4-1
IFMIN(M)=1
IFMAX(M)=1
MFMIN(M)=M
MFMAX(M)=M
SFMAX(M)=FSUM(1,M)
SFMIN(M)=FSUM(1,M)
DO 16 I=1,NPPS-1
IF(FSUM(I,M).LT.SFMIN(M)) THEN
SFMIN(M)=FSUM(I,M)
IFMIN(M)=I
END IF
```

```
      IF(FSUM(I,M).GT.SFMAX(M)) THEN
        SFMAX(M)=FSUM(I,M)
        IFMAX(M)=I
      END IF
16  CONTINUE
      IF(SFMAX(M).GT.HIGH) THEN
        HIGH=SFMAX(M)
      END IF
      IF(SFMIN(M).LT.LOW) THEN
        LOW=SFMIN(M)
      END IF
15  CONTINUE
C
      RETURN
      END
C
C  END SSORT
C
C
C
C
      SUBROUTINE TORO(X,Y,M,TMAX)
      INTEGER M,FAULT
      DIMENSION X(73,30),Y(73,30),TMAX(30,2)
C
C  FINITE ELEMENT STRESS ANALYSIS
C  TORSION OF A BAR WITH NONCIRCULAR CROSS SECTION
C  ADOPTED FROM
C  'ENGINEERING STRESS ANALYSIS'
C  BY D.N.FENNER (ELLIS HORWOOD 1987)
C
      CALL SPEC(X,Y,M)
      CALL ACTIVE
      CALL BWIDTH
      CALL ASSEM
      CALL SOLVE(FAULT)
      IF(FAULT.GT.0) GOTO 10
      CALL STRESS
      CALL OUTPUT(M,TMAX)
10  RETURN
      END
C
C
C
      SUBROUTINE SPEC(X,Y,M)
C
C  PROBLEM SPECIFICATION
C
      INTEGER I,M,K
      DIMENSION X(73,30),Y(73,30)
C
      COMMON/ELEM/IETYPE,NOE,IJ(100,3),MAT(100),NODN,NONE,NODE,NOST
      COMMON/NODE/NONS,XY(100,2),NOCO
      COMMON/EQNS/NODS,NOEQ,IBW,IDA(100,6),SS(200,50),FS(200)
      COMMON/DBCS/NOPD,IPD(50,2),PD(50)
      COMMON/MATS/NOPROP,NOSET,EDAT(5,5)
C  IETYPE: ELEMENT TYPE
C  NOE: NUMBER OF ELEMENTS IN THE SYSTEM
C  IJ(IE,NE): NODAL POINT NE FOR ELEMENT IE
C  MAT(IE): MATERIAL SET NUMBER FOR ELEMENT IE
C  NODN: NUMBER OF NODAL DEGREES OF FREEDOM
C  NONE: NUMBER OF NODES PER ELEMENT
C  NODE: NUMBER OF ELEMENT DEGREES OF FREEDOM
```

C NOST: NUMBER OF ELEMENT STRESS COMPONENTS
C NONS: NUMBER OF NODES IN THE SYSTEM
C XY(NS,ICO): COORDINATE ICO FOR NODAL POINT NS
C NOCO: NUMBER OF COORDINATES DEFINING ELEMENT GEOMETRY
C NODS: NUMBER OF SYSTEM DEGREES OF FREEDOM
C NOEQ: NUMBER OF ACTIVE EQUATIONS
C IBW: SEMI-BANDWIDTH OF SYSTEM STIFFNESS MATRIX
C IDA(NS,IDN): ACTIVE EQATION NUMBER CORRESPONDING TO DEGREE OF
C FREEDOM IDN OF NODE NS
C SS(IRE,ICE): SYSTEM STIFFNESS, AND ELEMENT STRESSES:
C SS(IRS,ICS), SYSTEM STIFFNESS COEFFICIENT;
C SS(IE,IST), STRESS COMPONENT IST FOR ELEMENT IE.
C FS(IDS): PRESCRIBED FORCE FOR SYSTEM DEGREE OF FREEDOM IDS
C NOPD: NUMBER OF PRESCRIBED DISPLACEMENTS
C IPD: POINTERS FOR DISPLACEMENT BOUNDARY CONDITION IBC:
C IPD(IBC,1),NODE; IPD(IBC,2), DEGREE OF FREEDOM
C PD(IBC): PRESCRIBED DISPLACEMENT FOR BOUNDARY CONDITION IBC
C NOPROP: NUMBER OF PROPERTIES PER SET OF MATERIAL DATA
C NOSET: NUMBER OF SETS OF MATERIAL DATA
C EDAT(IPROP,ISET): MATERIAL PROPERTY IPROP FOR DATA SET ISET

C
IETYPE=5
NODN=1
NONE=3
NOCO=2
NOST=2
NOPROP=0
NODE=NODN*NONE

C
C DEFINE NODES

C
NONS=61

C
DO 10 I=1,24
XY(I,1)=X(1+(I-1)*3,M)
XY(I,2)=Y(1+(I-1)*3,M)

10 CONTINUE

C
DO 20 I=1,18
XY(I+24,1)=X(1+(I-1)*4,M)*.75
XY(I+24,2)=Y(1+(I-1)*4,M)*.75

20 CONTINUE

C
DO 30 I=1,12
XY(I+42,1)=X(1+(I-1)*6,M)*.5
XY(I+42,2)=Y(1+(I-1)*6,M)*.5

30 CONTINUE

C
DO 35 I=1,6
XY(I+54,1)=X(1+(I-1)*12,M)*.25
XY(I+54,2)=Y(1+(I-1)*12,M)*.25

35 CONTINUE

C
XY(61,1)=0
XY(61,2)=0

C
C DEFINE ELEMENTS

C
NOE=96

C
K=0

```
DO 40 I=1,24
  IJ(I,1)=I
  IJ(I,2)=MOD(I,24)+1
  IJ(I,3)=24+I+K
  IF(MOD(I,4).EQ.0)THEN
    K=K-1
  END IF
  IF(I.EQ.24)THEN
    IJ(I,3)=25
  END IF
40 CONTINUE
C
K=0
DO 50 I=1,18
  IJ(24+I,1)=MOD(I+K,24)+1
  IF(MOD(I,3).EQ.0)THEN
    K=K+1
  END IF
  IJ(24+I,2)=MOD(I,18)+25
  IJ(24+I,3)=24+I
50 CONTINUE
C
K=0
DO 55 I=1,18
  IJ(42+I,1)=24+I
  IJ(42+I,2)=MOD(I,18)+25
  IJ(42+I,3)=42+I+K
  IF(MOD(I,3).EQ.0)THEN
    K=K-1
  END IF
  IF(I.EQ.18)THEN
    IJ(I+42,3)=43
  END IF
55 CONTINUE
C
K=0
DO 60 I=1,12
  IJ(I+60,1)=MOD(I+K,18)+25
  IF(MOD(I,2).EQ.0)THEN
    K=K+1
  END IF
  IJ(I+60,2)=MOD(I,12)+43
  IJ(I+60,3)=42+I
60 CONTINUE
C
K=0
DO 65 I=1,12
  IJ(I+72,1)=42+I
  IJ(I+72,2)=MOD(I,12)+43
  IJ(I+72,3)=54+I+K
  IF(MOD(I,2).EQ.0)THEN
    K=K-1
  END IF
  IF(I.EQ.12)THEN
    IJ(I+72,3)=55
  END IF
65 CONTINUE
C
K=0
DO 70 I=1,6
  IJ(I+84,1)=MOD(I+K,12)+43
  K=K+1
```

```
      IJ(I+84,2)=MOD(I,6)+55
      IJ(I+84,3)=54+I
70    CONTINUE
C
      DO 80 I=1,6
      IJ(90+I,1)=I+54
      IJ(90+I,2)=MOD(I,6)+55
      IJ(90+I,3)=61
80    CONTINUE
C
C
      NODS=NONS*NODN
C MATERIAL DATA
      NOSET=0
      DO 90 I=1,NOE
      MAT(I)=0
90    CONTINUE
C BOUNDARY CONDITIONS
      NOPD=1
      IPD(1,1)=61
      IPD(1,2)=1
      PD(1)=0
C
C
      RETURN
      END
C
C
C
      SUBROUTINE ACTIVE
C IDENTIFY ACTIVE EQUATIONS
      INTEGER NS, IDN, IBC
      COMMON/ELEM/IETYPE, NOE, IJ(100,3), MAT(100), NODN, NONE, NODE, NOST
      COMMON/NODE/NONS, XY(100,2), NOCO
      COMMON/EQNS/NODS, NOEQ, IBW, IDA(100,6), SS(200,50), FS(200)
      COMMON/DBCS/NOPD, IPD(50,2), PD(50)
C NS: SYSTEM NODE(=1,.....,NONS)
C IDN: NODAL DEGREE OF FREEDOM(=1,....,NODN)
C IBC: BOUNDARY CONDITION NUMBER
C
      DO 10 NS=1,NONS
      DO 15 IDN=1,NODN
      IDA(NS, IDN)=1
15    CONTINUE
10    CONTINUE
      DO 20 IBC=1,NOPD
      IF(ABS(PD(IBC)).GT.0.000001) GO TO 20
      NS=IPD(IBC,1)
      IDN=IPD(IBC,2)
      IDA(NS, IDN)=0
20    CONTINUE
      NOEQ=0
      DO 30 NS=1,NONS
      DO 30 IDN=1,NODN
      IF(IDA(NS, IDN).LT.0.000001) GOTO 30
      NOEQ=NOEQ+1
      IDA(NS, IDN)=NOEQ
30    CONTINUE
      RETURN
      END
C
C
```

```
C
SUBROUTINE BWIDTH
C CALCULATE SEMI-BANDWIDTH
INTEGER IE,NE,NS,IDN,IDE,IRE,IRS,ICE,ICS
COMMON/ELEM/IETYPE,NOE,IJ(100,3),MAT(100),NODN,NONE,NODE,NOST
COMMON/EQNS/NODS,NOEQ,IBW,IDA(100,6),SS(200,50),FS(200)
DIMENSION IRC(6)
C IE: ELEMENT NUMBER (=1,...,NOE)
C NE: ELEMENT NODE (=1,...,NONE)
C IDE: ELEMENT DEGREE OF FREEDOM (=1,...,NODE)
C IRE: ROW POSITION IN ELEMENT STIFFNESS MATRIX
C IRS: ROW POSITION IN SYSTEM STIFFNESS MATRIX
C ICE: COLUMN POSITION IN ELEMENT STIFFNESS MATRIX
C ICS: COLUMN POSITION IN SYSTEM STIFFNESS MATRIX
C IRC(IDE): ROW OR COLUMN POSITION IN SYSTEM MATRIX EQUIVALENT
C TO ROW OR COLUMN POSITION IDE IN ELEMENT STIFFNESS
C MATRIX
C
```

```
IBW=0
DO 40 IE=1,NOE
DO 10 NE=1,NONE
NS=IJ(IE,NE)
DO 15 IDN=1,NODN
IDE=NODN*(NE-1)+IDN
IRC(IDE)=IDA(NS,IDN)
15 CONTINUE
10 CONTINUE
DO 30 IRE=1,NODE
IRS=IRC(IRE)
IF(IRS.LT.0.000001) GOTO 30
DO 20 ICE=1,NODE
ICS=IRC(ICE)-IRS+1
IF(ICS.LT.1) GO TO 20
IBW=MAX(IBW,ICS)
20 CONTINUE
30 CONTINUE
40 CONTINUE
RETURN
END
```

```
C
C
C
```

```
SUBROUTINE ASSEM
C ASSEMBLE EQUILIBRIUM EQUATIONS
COMMON/ELEM/IETYPE,NOE,IJ(100,3),MAT(100),NODN,NONE,NODE,NOST
COMMON/EQNS/NODS,NOEQ,IBW,IDA(100,6),SS(200,50),FS(200)
COMMON/DBCS/NOPD,IPD(50,2),PD(50)
INTEGER IRS,ICS,IE,IDE,NE,NS,IDN,IRE,ICE,IBC,IDS
DIMENSION IRC(6),SE(6,6),FE(6)
C IDS: SYSTEM DEGREE OF FREEDOM (=1,...,NODS)
C SE(IRE,ICE): STIFFNESS COEFFICIENT IN ROW IRE AND COLUMN ICE OF
C ELEMENT STIFFNESS MATRIX
C FE(IDE): PRESCRIBED FORCE FOR ELEMENT DEGREE OF FREEDOM IDE
C
C ZERO ARRAYS
DO 10 IRS=1,NOEQ
FS(IRS)=0.
DO 15 ICS=1,IBW
SS(IRS,ICS)=0.
15 CONTINUE
10 CONTINUE
C SUM OVER ALL ELEMENTS IN SYSTEM
```

```
DO 50 IE=1,NOE
DO 16 IDE=1,NODE
  FE(IDE)=0.
16  CONTINUE
  CALL ELEMNT(IE,SE,FE)
  DO 20 NE=1,NONE
    NS=IJ(IE,NE)
    DO 25 IDN=1,NODN
      IDE=NODN*(NE-1)+IDN
      IRC(IDE)=IDA(NS,IDN)
25  CONTINUE
20  CONTINUE
  DO 40 IRE=1,NODE
    IRS=IRC(IRE)
    IF(IRS.EQ.0) GOTO 40
    FS(IRS)=FS(IRS)+FE(IRE)
    DO 30 ICE=1,NODE
      ICS=IRC(ICE)-IRS+1
      IF(ICS.LT.1) GOTO 30
      SS(IRS,ICS)=SS(IRS,ICS)+SE(IRE,ICE)
30  CONTINUE
40  CONTINUE
50  CONTINUE
C DISPLACEMENT BOUNDARY CONDITIONS
IF(NOEQ.GT.(NODS-NOPD)) THEN
DO 70 IBC=1,NOPD
  IF(ABS(PD(IBC)).LT.1E-12) GOTO 70
  NS=IPD(IBC,1)
  IDN=IPD(IBC,2)
  IDS=IDA(NS,IDN)
  SS(IDS,1)=SS(IDS,1)*1.E20
  FS(IDS)=PD(IBC)*SS(IDS,1)
70  CONTINUE
ENDIF
RETURN
END

C
C
C
  SUBROUTINE SOLVE(FAULT)
C SOLVE SET OF BANDED SYMMETRIC EQUILIBRIUM EQUATIONS
C USING GAUSSIAN ELIMINATION
  COMMON/EQNS/NODS,NOEQ,IBW,IDA(100,6),SS(200,50),FS(200)
  INTEGER IEQ,I,IR,IC,FAULT
  REAL R,CN
  DIMENSION DS(200)
C IEQ: ACTIVE EQUATION NUMBER (=1,...,NOEQ)
C I: FORWARD REDUCTION STEP NUMBER
C IR: ROW POSITION IN SYSTEM STIFFNESS MATRIX
C IC: COLUMN POSITION IN SYSTEM STIFFNESS MATRIX
C R: ELIMINATION RATIO FOR FORWARD REDUCTION
C DS: ARRAY STORING DIAGONAL COEFFICIENTS OF SYSTEM MATRIX
C
  FAULT=0
C
C STORE DIAGONAL COEFFICIENTS
C
  DO 10 IEQ=1,NOEQ
    DS(IEQ)=SS(IEQ,1)
10  CONTINUE
C FORWARD REDUCTION
DO 50 I=1,NOEQ-1
```

```
DO 40 IR=I+1,I+IBW-1
  IF(ABS(SS(I,IR-I+1)).LT.1E-12) GO TO 40
  R=SS(I,IR-I+1)/SS(I,1)
  DO 20 IC=IR,I+IBW-1
    IF(IC.GT.NOEQ) GO TO 30
    IF(ABS(SS(I,IC-I+1)).LT.1E-12) GO TO 20
    SS(IR,IC-IR+1)=SS(IR,IC-IR+1)-R*SS(I,IC-I+1)
20  CONTINUE
30  IF(ABS(FS(I)).LT.1E-12) GO TO 40
    FS(IR)=FS(IR)-R*FS(I)
40  CONTINUE
    CN=SS(I+1,1)/DS(I+1)
    IF(CN.LT.1E-3) GOTO 80
50  CONTINUE
C BACK SUBSTITUTION
  FS(NOEQ)=FS(NOEQ)/SS(NOEQ,1)
  DO 70 IR=NOEQ-1,1,-1
    DO 60 IC=IR+1,IR+IBW-1
      IF(IC.GT.NOEQ) GO TO 70
      IF(ABS(SS(IR,IC-IR+1)).LT.1E-12.OR.ABS(FS(IC)).LT.1E-12) GOTO 60
      FS(IR)=FS(IR)-SS(IR,IC-IR+1)*FS(IC)
60  CONTINUE
      FS(IR)=FS(IR)/SS(IR,1)
70  CONTINUE
    CALL RENUM
    RETURN
80  WRITE(9,600)
600  FORMAT(//' ***** ILL-CONDITIONED EQUATIONS ***** ')
    FAULT=1
    RETURN
  END
```

C
C
C

```
      SUBROUTINE RENUM
C  RENUMBER DISPLACEMENTS
      COMMON/ELEM/IETYPE,NOE,IJ(100,3),MAT(100),NODN,NONE,NODE,NOST
      COMMON/EQNS/NODS,NOEQ,IBW,IDA(100,6),SS(200,50),FS(200)
      COMMON/NODE/NONS,XY(100,2),NOCO
      INTEGER NS,IDN,IDS
```

C

```
      DO 10 NS=NONS,1,-1
        DO 15 IDN=NODN,1,-1
          IDS=NODN*(NS-1)+IDN
          IF(IDA(NS,IDN).EQ.0) THEN
            FS(IDS)=0.
          ELSE
            FS(IDS)=FS(IDA(NS,IDN))
          ENDIF
15  CONTINUE
10  CONTINUE
      RETURN
      END
```

C
C
C

```
      SUBROUTINE OUTPUT(M,TMAX)
      INTEGER M,IE,I
      REAL TAU
      DIMENSION TMAX(30,2),ARRAY(24)
      COMMON/EQNS/NODS,NOEQ,IBW,IDA(100,6),SS(200,50),FS(200)
```

C

C STRESSES IN SURFACE ELEMENTS DUE TO A TORQUE EQUAL TO 1

```
C
DO 10 IE=1,24
  ARRAY(IE)=SQRT(SS(IE,1)**2+SS(IE,2)**2)
  ARRAY(IE)=ARRAY(IE)/SS(1,3)
10 CONTINUE
  TMAX(M,1)=1
  TMAX(M,2)=ARRAY(1)
  TAU=ARRAY(1)
  DO 20 I=1,23
    IF (ARRAY(I).GT.TAU) THEN
      TAU=ARRAY(I)
      TMAX(M,1)=(I-1)*3+1
      TMAX(M,2)=TAU
    END IF
20 CONTINUE
RETURN
END
```

C
C
C

```
      SUBROUTINE ELEMNT(IE,SE,FE)
C EQUILIBRIUM EQUATIONS FOR NONCIRCULAR SHAFT ELEMENT
COMMON/ELEM/IETYPE,NOE,IJ(100,3),MAT(100),NODN,NONE,NODE,NOST
COMMON/NODE/NONS,XY(100,2),NOCO
COMMON/MATS/NOPROP,NOSET,EDAT(5,5)
INTEGER I,J,K
REAL AI,AJ,AK,AREA,BI,BJ,BK,CI,CJ,CK,XC,YC
DIMENSION SE(6,6),FE(6)
```

```
C ELEMENT STIFFNESS MATRIX [SE]
I=IJ(IE,1)
J=IJ(IE,2)
K=IJ(IE,3)
AI=XY(J,1)*XY(K,2)-XY(K,1)*XY(J,2)
AJ=XY(K,1)*XY(I,2)-XY(I,1)*XY(K,2)
AK=XY(I,1)*XY(J,2)-XY(J,1)*XY(I,2)
AREA=.5*(AI+AJ+AK)
BI=XY(J,2)-XY(K,2)
BJ=XY(K,2)-XY(I,2)
BK=XY(I,2)-XY(J,2)
CI=XY(K,1)-XY(J,1)
CJ=XY(I,1)-XY(K,1)
CK=XY(J,1)-XY(I,1)
SE(1,1)=(BI*BI+CI*CI)/(4.*AREA)
SE(1,2)=(BI*BJ+CI*CJ)/(4.*AREA)
SE(1,3)=(BI*BK+CI*CK)/(4.*AREA)
SE(2,2)=(BJ*BJ+CJ*CJ)/(4.*AREA)
SE(2,3)=(BJ*BK+CJ*CK)/(4.*AREA)
SE(3,3)=(BK*BK+CK*CK)/(4.*AREA)
SE(2,1)=SE(1,2)
SE(3,1)=SE(1,3)
SE(3,2)=SE(2,3)
```

```
C MATRIX [FE]
XC=(XY(I,1)+XY(J,1)+XY(K,1))/3.
YC=(XY(I,2)+XY(J,2)+XY(K,2))/3.
FE(1)=(YC*BI-XC*CI)/2.
FE(2)=(YC*BJ-XC*CJ)/2.
FE(3)=(YC*BK-XC*CK)/2.
RETURN
END
```

C
C

```
C
SUBROUTINE STRESS
C STRESSES AND TORSIONAL CONSTANT FOR NONCIRCULAR
COMMON/EQNS/NODS,NOEQ,IBW,IDA(100,6),SS(200,50),FS(200)
COMMON/ELEM/IETYPE,NOE,IJ(100,3),MAT(100),NODN,NONE,NODE,NOST
COMMON/NODE/NONS,XY(100,2),NOCO
COMMON/MATS/NOPROP,NOSET,EDAT(5,5)
INTEGER IE,I,J,K
REAL XI,XJ,XK,YI,YJ,YK,XC,YC,AI,AJ,AK,AREA,BI,BJ,BK,CI,CJ,CK
REAL F1,F2
```

```
C
SS(1,3)=0.
DO 10 IE=1,NOE
I=IJ(IE,1)
J=IJ(IE,2)
K=IJ(IE,3)
XI=XY(I,1)
XJ=XY(J,1)
XK=XY(K,1)
YI=XY(I,2)
YJ=XY(J,2)
YK=XY(K,2)
XC=(XI+XJ+XK)/3.
YC=(YI+YJ+YK)/3.
AI=XJ*YK-XK*YJ
AJ=XK*YI-XI*YK
AK=XI*YJ-XJ*YI
AREA=.5*(AI+AJ+AK)
BI=YJ-YK
BJ=YK-YI
BK=YI-YJ
CI=XK-XJ
CJ=XI-XK
CK=XJ-XI
```

```
C TORSIONAL CONSTANT
F1=((XC*CI-YC*BI)*FS(I)+(XC*CJ-YC*BJ)*FS(J)+
* (XC*CK-YC*BK)*FS(K))/2.
F2=AREA/6.*(XI*XI+XJ*XJ+XK*XK+YI*YI+YJ*YJ+YK*YK+XI*XJ+XJ*XK+
* XK*XI+YI*YJ+YJ*YK+YK*YI)
SS(1,3)=SS(1,3)+F1+F2
```

```
C ELEMENT STRESSES
C SS(IE,1)=TAUYZ; SS(IE,2)=TAUZX
SS(IE,1)=1./(2.*AREA)*(CI*FS(I)+CJ*FS(J)+CK*FS(K))+XC
SS(IE,2)=1./(2.*AREA)*(BI*FS(I)+BJ*FS(J)+BK*FS(K))-YC
10 CONTINUE
RETURN
END
```

```
C
C
C END TORO
```

```
C
SUBROUTINE ELBEAM(X,Y,Z,LEVEL,INAX,INAY,MX,MY,SX,SY,ES,EC,DB)
INTEGER FLAG,LEVEL,LDIV
REAL B,XRES,D,ES,EC,DB
REAL INAX,INAY,KN,HN,X,Y,Z,MX,MY,SX,SY,IN
DIMENSION X(73,30),Y(73,30),Z(73,30),INAX(30),INAY(30)
DIMENSION MX(30),MY(30),XRES(100),COEF(100,100)
DIMENSION IN(100),KN(100),HN(100),IPIVOT(100),B(100),D(100)
```

```
C
LDIV=Z(1,LEVEL)/2
C ES=2000
C EC=2000
```

```
C      DB=60
C
C      FLAG=1
      CALL PARAM(X,Y,Z,LDIV,KN,HN,IN,INAY,FLAG,EC,DB)
      CALL MATRIX(IN,KN,HN,COEF,LDIV+1,ES,MY(LEVEL),SX,B)
      CALL FACTOR(COEF,IPIVOT,D,LDIV+1)
      CALL SUBST(COEF,B,XRES,IPIVOT,LDIV+1)
      CALL MOMENT(MY,SX,XRES,LEVEL,LDIV,HN,Z,ES,IN)
C
C
C      FLAG=0
      CALL PARAM(X,Y,Z,LDIV,KN,HN,IN,INAX,FLAG,EC,DB)
      CALL MATRIX(IN,KN,HN,COEF,LDIV+1,ES,MX(LEVEL),SY,B)
      CALL FACTOR(COEF,IPIVOT,D,LDIV+1)
      CALL SUBST(COEF,B,XRES,IPIVOT,LDIV+1)
      CALL MOMENT(MX,SY,XRES,LEVEL,LDIV,HN,Z,ES,IN)
C
C      CALCULATE STRESSES
C
C      RETURN
      END
C
C      END ELBEAM
C
C      SUBROUTINE PARAM(X,Y,Z,LEVEL,KN,HN,IN,INA,FLAG,EC,DB)
      INTEGER I,K,L,LEVEL,FLAG
      REAL X,Y,Z,KN,HN,IN,INA,DB,EC,DS,HSUM
      DIMENSION X(73,30),Y(73,30),Z(73,30),INA(30)
      DIMENSION IN(100),KN(100),HN(100)
C
C      PREAPERING THE PARAMETERS FOR THE CALCULATION
      DB - BONE DIAMETER (60 MM)
      EC - CEMENT ELASTICITY
      KN - STIFFNESSES OF THE CEMENT RINGS
C
      K=FLAG*18
C
      HN(1)=2
      IN(1)=INA(1)
      DS=SQRT(X(1+K,1)**2+Y(1+K,1)**2)+SQRT(X(37+K,1)**2+Y(37+K,1)**2)
      DS=DS/DB
C
C      COMPUTATION OF THE STIFFNESS ACCORDING TO THE APPROXIMATE
      FORMULA DEVELOPED BY HUISKES
C
      KN(1)=EC*1.9*1.2*(0.24+DS/(1-DS))
      L=1
      HSUM=0.0
C
      DO 10 I=1,LEVEL
         HN(I+1)=2
         HSUM=HSUM+1
         IF(HSUM.GT.Z(1,L)) THEN
            L=L+1
         END IF
         IN(I+1)=INA(L)
         DS=SQRT(X(1+K,L)**2+Y(1+K,L)**2)+SQRT(X(37+K,L)**2+Y(37+K,L)**2)
         DS=DS/DB
         KN(I+1)=EC*1.9*1.2*(0.24+DS/(1-DS))
10      CONTINUE
      RETURN
```

```
END
C
C END PARAM
C
SUBROUTINE MATRIX(IN,KN,HN,COEF,N,ES,M,S,B)
C SUBROUTINE CALCULATES THE MATRIX FOR THE SOLUTION
C OF THE BEAM ON ELASTIC FOUNDATION WITH FINITE
C DIFFERENCE METHOD
C
INTEGER I,J,K,N
REAL IN,KN,M,S,HN,ES,R
DIMENSION IN(100),KN(100),HN(10),COEF(100,100),B(100)
C
C MATRIX COEF INCLUDES THE COEFFICIENTS FOR THE DISPLACEMENTS
C STARTING WITH THE POINT N TO 1. THE LAST RAW IS THE SHEAR
C FORCE S AND MOMENT M VECTOR
C
C ES ELASTICITY MODULUS OF THE STEM
C
C ZEROIZE THE MATRIX COEF
C
DO 10 I=1,100
  B(I)=0.0
  DO 20 J=1,100
    COEF(I,J)=0.0
20 CONTINUE
10 CONTINUE
C
C FIRST LINE IN COEF
C
COEF(1,1)=1+KN(1)*HN(1)**4/ES/IN(1)/2
COEF(1,2)=-2
COEF(1,3)=1
B(1)=0.0
C
C SECOND LINE IN COEF
C
COEF(2,N)=KN(N)*HN(N)/2/KN(1)/HN(1)
COEF(2,1)=0.5
B(2)=S/KN(1)/HN(1)
DO 30 I=2,N-1
  COEF(2,I)=KN(N-I+1)*HN(N-I+1)/KN(1)/HN(1)
30 CONTINUE
C
C COMPUTE REST OF THE MATRIX COEF
C
K=1
DO 40 I=3,N
  R=0.0
  DO 50 J=K,N
    IF(J.EQ.K)THEN
      COEF(I,J)=1
    END IF
    IF(J.EQ.K+1)THEN
      COEF(I,J)=-2
    END IF
    IF(J.EQ.K+2)THEN
      R=R+HN(J)
    IF(J.EQ.N)THEN
      COEF(I,J)=1+KN(J)*HN(J)**4/ES/IN(J)/2
    ELSE
      COEF(I,J)=1+KN(J)*HN(J)**4/ES/IN(J)
```

```
      END IF
      END IF
      IF (J.GT.K+2) THEN
        R=R+HN(J)
        IF (J.EQ.N) THEN
          COEF(I,J)=KN(J)*HN(J)**3/ES/IN(J)*R/2
        ELSE
          COEF(I,J)=KN(J)*HN(J)**3/ES/IN(J)*R
        END IF
      COEF(I,J)=0.0
    END IF
50  CONTINUE
    K=K+1
    B(I)=(S*R+M)*HN(N)**2/ES/IN(N)
40  CONTINUE
C
    RETURN
    END
C
C  END MATRIX
C
SUBROUTINE FACTOR(COEF,IPIVOT,D,N)
GAUSS REDUCTION WITH PARTIAL PIVOTING
C
C  INTEGER I,IPIVOT,NM1,N,J,K,KP1,IP,IPK
C  REAL D,ROWMAX,COLMAX,AWIKOV,RATIO
C  DIMENSION COEF(100,100),IPIVOT(100),D(100)
C
C  INITIALIZE IPIVOT,D
C
DO 10 I=1,N
  IPIVOT(I)=I
  ROWMAX=0.0
  DO 9 J=1,N
    ROWMAX=AMAX1(ROWMAX,ABS(COEF(I,J)))
9  CONTINUE
  IF(ROWMAX.LT.1E-10)GOTO 999
  D(I)=ROWMAX
10 CONTINUE
C
C  GAUSS ELIMINATION WITH SCALED PARTIAL PIVOTING
C
NM1=N-1
IF(NM1.EQ.0)RETURN
DO 20 K=1,NM1
  J=K
  KP1=K+1
  IP=IPIVOT(K)
  COLMAX=ABS(COEF(IP,K))/D(IP)
  DO 11 I=KP1,N
    IP=IPIVOT(I)
    AWIKOV=ABS(COEF(IP,K))/D(IP)
    IF(AWIKOV.LE.COLMAX) GOTO 11
    COLMAX=AWIKOV
  J=I
11 CONTINUE
C
  IF(COLMAX.EQ.0.0) GOTO 999
C
  IPK=IPIVOT(J)
  IPIVOT(J)=IPIVOT(K)
  IPIVOT(K)=IPK
```

```
C      DO 19 I=KP1,N
      IP=IPIVOT(I)
      COEF(IP,K)=COEF(IP,K)/COEF(IP,K)
      RATIO=-COEF(IP,K)
C
      DO 18 J=KP1,N
      COEF(IP,J)=RATIO*COEF(IPK,J)+COEF(IP,J)
18     CONTINUE
19     CONTINUE
20     CONTINUE
C
      IF(COEF(IP,N).EQ.0.0) GOTO 999
      RETURN
999    PRINT*, 'MATRIX COEF IS SINGULAR'
      RETURN
      END
C
      END FACTOR
C
      SUBROUTINE SUBST(COEF,B,X,IPIVOT,N)
C
      FORWARD AND BACK SUBSTITUTION FOR GAUSS FACTOR
C
      INTEGER I,J,K,IPIVOT,N,IP,KM1,NP1MK,KP1
      REAL B,X,COEF,SUM
      DIMENSION COEF(100,100),B(100),X(100),IPIVOT(100)
C
      IF(N.GT.1) GOTO 10
      X(1)=B(1)/COEF(1,1)
      RETURN
C
10     IP=IPIVOT(1)
      X(1)=B(IP)
      DO 15 K=2,N
      IP=IPIVOT(K)
      KM1=K-1
      SUM=0.0
      DO 14 J=1,KM1
      SUM=COEF(IP,J)*X(J)+SUM
14     CONTINUE
      X(K)=B(IP)-SUM
15     CONTINUE
C
      X(N)=X(N)/COEF(IP,N)
      K=N
      DO 20 NP1MK=2,N
      KP1=K
      K=K-1
      IP=IPIVOT(K)
      SUM=0.0
      DO 19 J=KP1,N
      SUM=COEF(IP,J)*X(J)+SUM
19     CONTINUE
      X(K)=(X(K)-SUM)/COEF(IP,K)
20     CONTINUE
C
      RETURN
      END
C
      END SUBST
C
```

```
SUBROUTINE MOMENT(M,S,X,LEVEL,N,HN,Z,ES,IN)
INTEGER I,N,L,LEVEL
REAL M,S,X,HN,R,MSUM,ES,IN
DIMENSION M(30),X(100),HN(100),Z(73,30),IN(100)
```

C

```
L=1
DO 10 I=2,N-1
  IF(ABS(I*HN(1)-Z(1,L)).LT.0.001)THEN
    M(L)=ES*IN(I)/HN(I)**2*(X(I+1)-2*X(I)+X(I-1))
    L=L+1
  END IF
```

10

```
CONTINUE
```

C

```
RETURN
END
```

C

```
END MOMENT
```

C

C

C

```
SUBROUTINE SCFINT(RAT1,RAT2,IPNT,MSTEP,K,SCF)
INTEGER IPNT,MSTEP,I,J,M
REAL K,RAT1,RAT2,A,B
DIMENSION SCF(8,30,2),K(73,30)
```

C

```
C FIND STRESS CONCENTRATION FACTORS
```

C

```
IF(RAT1.LE.1.01)THEN
  I=1
ELSEIF(RAT1.LE.1.02)THEN
  I=2
ELSEIF(RAT1.LE.1.05)THEN
  I=3
ELSEIF(RAT1.LE.1.1)THEN
  I=4
ELSEIF(RAT1.LE.1.2)THEN
  I=5
ELSEIF(RAT1.LE.1.5)THEN
  I=6
ELSEIF(RAT1.LE.2)THEN
  I=7
ELSEIF(RAT1.LE.3)THEN
  I=8
ELSE
  I=9
ENDIF
```

C

```
IF(RAT2.LE.0.01)THEN
  J=0
ELSEIF(RAT2.GT.0.3)THEN
  J=30
ELSE
  DO 100 M=1,30
    IF(RAT2.LE.(0.01+M*0.01))THEN
      J=M
      GOTO 110
    END IF
```

100

```
CONTINUE
```

110

```
CONTINUE
```

```
END IF
```

C

```
C LINEAR INTERPOLATION OF STRESS CONCENTRATION FACTORS
```

C

```
IF((I.EQ.9).OR.(J.EQ.0))THEN
  PRINT*,'***WARNING***'
  PRINT*,'STRESS CONCENTRATION FACTOR OUT OF'
  PRINT*,'INTERPOLATION RANGE'
  PRINT*,'SCF SET TO 4.5'
  PRINT*,'*****'
  K(IPNT,MSTEP)=4.5
  GOTO 300
END IF
IF(J.EQ.30)THEN
  K(IPNT,MSTEP)=SCF(I,J,2)
  GOTO 300
END IF
A=(SCF(I,J,1)-SCF(I,J+1,1))/(SCF(I,J,2)-SCF(I,J+1,2))
B=SCF(I,J,2)-A*SCF(I,J,1)
K(IPNT,MSTEP)=A*RAT2+B
300 RETURN
END
C
C END SCFINT
C
```

File containing values of stress concentration factors from the literature.

File SCFDAT

D/d = 1.01

<u>r/d</u>	<u>K_T</u>
0.010	1.637
0.020	1.437
0.030	1.352
0.040	1.311
0.050	1.285
0.060	1.273
0.070	1.258
0.080	1.247
0.090	1.245
0.100	1.237
0.110	1.236
0.120	1.229
0.130	1.226
0.140	1.224
0.150	1.223
0.160	1.222
0.170	1.220
0.180	1.220
0.190	1.219
0.200	1.218
0.210	1.216
0.220	1.211
0.230	1.211
0.240	1.208
0.250	1.206
0.260	1.205
0.270	1.203
0.280	1.204
0.290	1.203
0.300	1.203

D/d = 1.02

<u>r/d</u>	<u>K_T</u>
0.010	1.916
0.020	1.658
0.030	1.535
0.040	1.454
0.050	1.406
0.060	1.374
0.070	1.353
0.080	1.342
0.090	1.327
0.100	1.313
0.110	1.309
0.120	1.297
0.130	1.294
0.140	1.286
0.150	1.282
0.160	1.272
0.170	1.272
0.180	1.269
0.190	1.260

0.200	1.258
0.210	1.254
0.220	1.246
0.230	1.238
0.240	1.237
0.250	1.231
0.260	1.235
0.270	1.230
0.280	1.231
0.290	1.225
0.300	1.226

D/d = 1.05

<u>r/d</u>	<u>K_T</u>
0.010	2.415
0.020	2.033
0.030	1.835
0.040	1.731
0.050	1.658
0.060	1.596
0.070	1.551
0.080	1.515
0.090	1.498
0.100	1.470
0.110	1.452
0.120	1.435
0.130	1.420
0.140	1.404
0.150	1.389
0.160	1.373
0.170	1.365
0.180	1.351
0.190	1.342
0.200	1.333
0.210	1.324
0.220	1.315
0.230	1.303
0.240	1.299
0.250	1.292
0.260	1.283
0.270	1.275
0.280	1.272
0.290	1.269
0.300	1.270

D/d = 1.1

<u>r/d</u>	<u>K_T</u>
0.010	2.795
0.020	2.333
0.030	2.091
0.040	1.952
0.050	1.855
0.060	1.778
0.070	1.715
0.080	1.672
0.090	1.630
0.100	1.593
0.110	1.567
0.120	1.538
0.130	1.519

0.140	1.498
0.150	1.476
0.160	1.462
0.170	1.444
0.180	1.426
0.190	1.413
0.200	1.399
0.210	1.388
0.220	1.371
0.230	1.362
0.240	1.352
0.250	1.344
0.260	1.335
0.270	1.324
0.280	1.314
0.290	1.311
0.300	1.312

D/d = 1.2

<u>r/d</u>	<u>K_r</u>
0.010	3.258
0.020	2.698
0.030	2.389
0.040	2.199
0.050	2.057
0.060	1.949
0.070	1.860
0.080	1.792
0.090	1.738
0.100	1.691
0.110	1.654
0.120	1.621
0.130	1.593
0.140	1.569
0.150	1.542
0.160	1.519
0.170	1.497
0.180	1.475
0.190	1.452
0.200	1.439
0.210	1.423
0.220	1.412
0.230	1.392
0.240	1.382
0.250	1.369
0.260	1.360
0.270	1.355
0.280	1.351
0.290	1.342
0.300	1.340

D/d = 1.5

<u>r/d</u>	<u>K_r</u>
0.010	3.796
0.020	2.996
0.030	2.620
0.040	2.378
0.050	2.209
0.060	2.076
0.070	1.974

0.080	1.895
0.090	1.825
0.100	1.772
0.110	1.720
0.120	1.680
0.130	1.648
0.140	1.617
0.150	1.587
0.160	1.556
0.170	1.540
0.180	1.514
0.190	1.493
0.200	1.474
0.210	1.459
0.220	1.445
0.230	1.430
0.240	1.416
0.250	1.401
0.260	1.392
0.270	1.384
0.280	1.373
0.290	1.365
0.300	1.358

D/d = 2

<u>r/d</u>	<u>K_r</u>
0.010	3.997
0.020	3.134
0.030	2.755
0.040	2.515
0.050	2.333
0.060	2.194
0.070	2.078
0.080	1.983
0.090	1.909
0.100	1.846
0.110	1.792
0.120	1.739
0.130	1.695
0.140	1.657
0.150	1.628
0.160	1.596
0.170	1.564
0.180	1.541
0.190	1.518
0.200	1.503
0.210	1.481
0.220	1.462
0.230	1.447
0.240	1.431
0.250	1.413
0.260	1.403
0.270	1.392
0.280	1.382
0.290	1.379
0.300	1.368

D/d = 3

<u>r/d</u>	<u>K_r</u>
0.010	4.197

0.020	3.238
0.030	2.914
0.040	2.673
0.050	2.483
0.060	2.332
0.070	2.202
0.080	2.095
0.090	1.996
0.100	1.923
0.110	1.853
0.120	1.803
0.130	1.755
0.140	1.707
0.150	1.667
0.160	1.629
0.170	1.592
0.180	1.566
0.190	1.542
0.200	1.521
0.210	1.499
0.220	1.480
0.230	1.456
0.240	1.450
0.250	1.429
0.260	1.417
0.270	1.408
0.280	1.400
0.290	1.394
0.300	1.383

Example of the output from the program PROCOM. In this example, the elasticity modulus of the embedding was 32 times lower than that of the prosthesis.

File STRESS

ANALYSIS OF PROSTHESIS F076

LOAD	RADIUS	TILTANGLE	EMB.LEVEL
1000.00	2.0000	10.0000	12

MAXIMUM AND MINIMUM STRESSES

STEP POINT MAXSTRESS

1	7	4.042
2	3	5.834
3	6	6.375
4	5	5.796
5	6	6.475
6	3	6.231
7	66	1.815
8	39	9.796
9	38	33.303
10	38	55.817
11	36	81.379
12	36	82.798
13	37	70.156
14	34	61.552
15	37	50.578
16	31	43.583
17	35	35.193
18	36	25.136
19	34	18.817
20	32	14.501
21	31	12.144
22	31	8.848

STEP POINT MINSTRESS

1	43	-4.051
2	39	-5.863
3	39	-5.982
4	38	-5.376
5	38	-6.346
6	38	-5.862
7	28	-1.914
8	3	-10.693
9	4	-36.921
10	3	-64.270
11	2	-98.268
12	2	-118.033
13	3	-104.000
14	2	-94.758
15	2	-78.547
16	2	-68.641

17	2	-55.959
18	2	-38.503
19	1	-31.067
20	2	-24.962
21	2	-21.347
22	3	-15.947

MAXIMUM AND MINIMUM FACTORED STRESSES

STEP POINT MAXSTRESS

1	7	5.608
2	9	8.412
3	9	9.264
4	7	7.951
5	6	9.232
6	5	8.664
7	66	2.677
8	33	11.960
9	38	40.634
10	35	74.675
11	35	99.246
12	40	118.173
13	35	102.301
14	38	93.424
15	32	76.878
16	31	74.965
17	35	60.533
18	32	41.975
19	31	29.235
20	32	18.236
21	31	15.463
22	31	11.266

STEP POINT MINSTRESS

1	39	-5.027
2	39	-7.099
3	38	-7.380
4	38	-6.536
5	38	-7.743
6	38	-7.182
7	29	-2.375
8	6	-15.761
9	4	-56.934
10	2	-93.764
11	2	-149.262
12	2	-191.284
13	2	-150.292
14	2	-150.952
15	2	-125.127
16	2	-111.899
17	2	-100.294
18	2	-71.625
19	1	-60.559
20	2	-51.335
21	2	-43.900
22	3	-32.794

STEP	POINT	TOR. STRESS
1	61	10.815
2	61	9.028
3	61	7.670
4	64	5.285
5	61	4.256
6	58	4.379
7	58	3.405
8	58	3.001
9	58	2.604
10	58	2.431
11	58	2.429
12	58	2.898
13	58	3.359
14	58	3.302
15	58	2.648
16	58	2.401
17	58	2.700
18	58	2.051
19	58	1.876
20	58	1.002
21	58	0.689
22	55	0.300

APPENDIX 4. Program for Indexing of Diffraction Patterns

The camera constant method [110] was used for indexing diffraction patterns. In the first stage, the distances (r) of several spots are measured from the central spot. The camera constant of the electron microscope λ^*L , where λ is the wave length of the electrons and L the camera length, is divided by the values of r . The results are compared against a list of plane spacings (d). One of the spots is arbitrarily indexed for a given combination of (h,k,l) -indices corresponding to d . The remaining spots are indexed using rules of vector addition. The angles (α) between lines from the centre spot to the spots measured and the correct combination of the (h,k,l) -indices are checked using formulas for relevant crystal structures. In the second stage, the beam direction of the electrons (B) is determined. Having indexed two spots in the diffraction pattern, the corresponding reciprocal lattice vectors (g) can be computed. The beam direction can be then calculated from the vector product of the g vectors:

$$B = g_1 \wedge g_2$$

where B - beam direction,
 g_1, g_2 - reciprocal lattice vectors.

The beam direction is parallel to the zone axis $[u,v,w]$ of the reflecting planes.

The procedure outlined above works well in case of one phase material with known crystallographic structure. If different phases are present in the material and if they can have similar diffraction patterns, as in case of a titanium alloy, the indexing procedure becomes rather difficult. One way of avoiding the difficulties is to photograph several diffraction patterns with different beam directions, which is time consuming. A second way, is to plot theoretical diffraction patterns for different crystal structures and compare them with the experimental ones. The second method can be performed quickly on a computer. The computer program shown below performs two tasks: it searches for plane spacings and angles which would match experimental data in four different crystallographic systems, and it plots the respective diffraction patterns on the computer screen. The plotted diffraction pattern can then be immediately compared with the experimental one. A version of the program can be used for plotting theoretical diffraction patterns only by directly inputting (hkl) -indices. This version is not presented here, for it would not introduce any new information. As a concluding remark it should be pointed out that the use of the computer program significantly speed up and increased the accuracy of the indexing procedure.

Program DIFFRA

```
c   The program DIFFRA calculates theoretical diffraction
c   patterns which match the input data measured on a
c   experimentally obtained diffraction pattern for hexagonal,
c   cubic and orthorhombic crystal systems. The input data are:
c   r - distance in mm from the central spot to one of the
c   diffraction spots,
c   t - distance in mm from the central spot to a second
c   diffraction spot,
c   alpha - angle between vectors r and t in degrees.
c
c   The program asks several questions during it is ran. Two
c   files are produced on output: the file DIFOUT contains a
c   report of the last session and the file DRAWDAT includes
c   input data for the program DRAW which produces a graphical
c   representation of the calculated diffraction patterns.
c
c   The meanings of the variables in the program are as follows:
c   i,j,k - integer pointers
c   nfcc - number of planes in the fcc-array for face centred
c   cubic structure
c   nbcc - number of planes in the bcc-array for body centred
c   cubic structure
c   nhcp - number of planes in the hcp-array for hexagonal
c   structure
c   nort - number of planes in the ort-array for orthorhombic
c   structure
c   nr - identification number of the diffraction pattern
c   fccind, bccind, hcpind, ortind - arrays containing (hkl)-
c   indices of planes for comparison with fcc-, bcc-, hcp- and
c   ort-array
c   fcc, bcc, hcp, ort - arrays containing (hkl)-indices of all
c   possible planes according to cubic, hexagonal and orthorhombic
c   crystal symmetry
c   l - camera length of the microscope in mm
c   l1,l2 - lower and upper limit of the camera length
c   afcc - basis vector length of the fcc unit cell in Angstroem
c   abcc - basis vector length of the bcc unit cell in Angstroem
c   ahcp, chcp - basis vector lengths of the hcp unit cell
c   aort, bort, cort - basis vector lengths of the ort unit cell
c   lambda - wave length of the electrons in Angstroem
c   pi -  $\pi$ 
c   alpha1, alpha2, r1, r2, t1, t2 - lower and upper error
c   limits of alpha, r and t
c   erl, err, ert, era - measurement errors of l (mm), r and t
c   (%), alpha (degrees)
c   da, db, da1, da2, db1, db2 - plane spacings and their
c   limits calculated from r and t
c
c   program diffra
c
c   integer i,j,k,nfcc,nbcc,nhcp,nort,nr
c   integer*1 fccind(3,19),bccind(3,28),hcpind(4,25),
+ortind(3,100)
c   integer*1 fcc(700,3),bcc(700,3),hcp(700,3),ort(700,3)
c   real l,l1,l2,afcc,abcc,ahcp,chcp,aort,bort,cort,lambda,pi
c   real alpha,alpha1,alpha2,r,r1,r2,t,t1,t2
c   real erl,err,ert,era
c   real da,da1,da2,db,db1,db2
c   common /dat1/ fcc,bcc,hcp,ort,afcc,abcc,ahcp,chcp,alpha1,
```

```
*alpha2,da1,da2,db1,db2,alpha,nfcc,nbcc,nhcp,1,lambda,nr,  
*nort,aort,bort,cort  
data fccind /1,1,1,2,0,0,2,2,0,3,1,1,2,2,2,  
*4,0,0,3,3,3,4,2,0,4,2,2,5,1,1,3,3,3,4,4,0,  
*5,3,1,6,0,0,4,4,2,6,2,0,5,3,3,6,2,2,4,4,4/  
data bccind /1,1,0,2,0,0,2,1,1,2,2,0,3,1,0,2,2,2,3,2,1,4,0,0,  
*4,1,1,3,3,0,4,2,0,3,3,2,4,2,2,5,1,0,4,3,1,5,2,1,4,4,0,  
*5,3,0,4,3,3,6,0,0,4,4,2,6,1,1,5,3,2,6,2,0,5,4,1,6,2,2,6,3,1,  
*4,4,4/  
data hcpind /0,1,-1,0,0,0,0,2,0,1,-1,1,0,1,-1,2,  
*1,1,-2,0,0,1,-1,3,0,2,-2,0,1,1,-2,2,0,2,-2,1,  
*0,0,0,4,0,2,-2,2,0,1,-1,4,0,2,-2,3,1,2,-3,0,1,2,-3,1,  
*0,0,0,5,1,1,-2,4,1,2,-3,2,0,1,-1,5,0,2,-2,4,0,3,-3,0,  
*1,2,-3,3,0,3,-3,2,0,0,0,6,-1,2,-1,6/  
c data ortind /1,1,0,1,0,1,0,1,1,2,0,0,0,2,0,0,0,2,  
c *2,2,0,2,0,2,0,2,2,2,2,2,3,1,0,3,0,1,0,3,1,1,3,0,1,0,3,0,1,3,  
c *3,2,1,3,1,2,1,3,2,2,3,1,2,1,3,1,2,3,3,3,2,3,2,3,2,3,3,4,0,0,  
c *0,4,0,0,0,4,4,1,1,1,4,1,1,1,4,4,2,0,4,0,2,0,2,4,2,4,0,2,0,4,  
c *0,2,4,4,2,2,2,4,2,2,2,4,4,3,1,4,1,3,1,4,3,3,4,1,3,1,4,1,4,3,  
c *4,3,3,3,4,3,3,3,4,4,4,4,5,1,0,5,0,1,0,5,1,1,5,0,1,0,5,0,1,5,  
c *5,2,1,5,1,2,1,5,2,2,5,1,2,1,5,1,2,5,5,3,0,5,0,3,0,5,3,3,5,0,  
c *3,0,5,0,3,5,5,3,2,5,2,3,2,5,3,3,5,2,3,2,5,2,3,5/  
data ortind /1,0,0,0,1,0,0,0,1,1,1,0,1,0,1,0,1,1,2,0,0,0,2,0,  
*0,0,2,1,1,1,1,2,0,1,0,2,0,1,2,2,1,0,2,0,1,0,2,1,2,2,0,2,0,2,  
*2,1,1,1,2,1,1,1,2,  
*0,2,2,2,2,1,2,1,2,1,2,2,2,2,2,3,0,0,0,3,0,0,0,3,3,1,0,3,0,1,  
*0,3,1,1,3,0,1,0,3,0,1,3,3,1,1,1,3,1,1,1,3,3,2,1,3,1,2,1,3,2,  
*2,3,1,2,1,3,1,2,3,3,2,2,2,3,2,2,2,3,3,3,2,3,2,3,2,3,3,3,3,3,  
*4,0,0,0,4,0,0,0,4,4,1,0,4,0,1,0,4,1,1,4,0,1,0,4,0,1,4,4,1,1,  
*1,4,1,1,1,4,4,2,0,4,0,2,0,2,4,2,4,0,2,0,4,0,2,4,4,2,1,4,1,2,  
*1,4,2,2,4,1,2,1,4,1,2,4,4,2,2,2,4,2,2,2,4,4,3,0,4,0,3,0,4,3,  
*3,4,0,3,0,4,0,3,4,4,3,1,4,1,3,1,4,3,3,4,1,3,1,4,1,3,4,4,3,2,  
*4,2,3,2,4,3,3,4,2,3,2,4,2,3,4,4,3,3,3,4,3,3,3,4,4,4,4,4/  
c  
c pi=3.141592654  
c  
c Camera lengt in mm  
c l=755.3h  
c  
c Wave length in A for 100kV  
c lambda=.037  
c  
c Lattice parameter fcc martensite in A  
c afcc=4.5  
c  
c Lattice parameter bcc Ti in A  
c abcc=3.283  
c  
c Lattice parameters hcp Ti in A  
c ahcp=2.95  
c chcp=4.683  
c  
c Lattice parameters orthorhombic  
c aort=3.01  
c bort=4.9  
c cort=4.63  
c  
c Error limits  
c erl=5  
c err=5  
c ert=err  
c era=3
```

```
c
c   Zeroise arrays
do 10 i=1,700
  do 20 j=1,3
    fcc(i,j)=0
    bcc(i,j)=0
    hcp(i,j)=0
    ort(i,j)=0
20  continue
10  continue
c
c   Compute all possible plane indices for cubic, hexagonal and
c   orthorhombic system
c
call cubsym(fcc,fccind,19,nfcc,bcc,bccind,28,nbcc)
call hexsym(hcp,hcpind,25,nhcp,)
call ortsym(ort,ortind,100,nort,aort,bort,cort)
c
c   Open output files
c
open(3,file='b:difout')
open(4,file='b:drawdat')
c
c   Input of the diffr. pattern data
c
5  print*,'Photo number ?'
   read(*,*)nr
   print*,'Input the SHORTEST vector lenght in mm'
   print*,'A= ?'
   read(*,*)r
   print*,'Input the next shortest vector in anticlockwise'
   print*,'direction from the previous one in mm'
   print*,'B= ?'
   read(*,*)t
   print*,'Input the angle between A & B in degrees,'
   print*,'positive in anticlockwise direction'
   print*,'Alpha= ?'
   read(*,*)alpha
c
   print*,'Do you want to change settings ? (y=1,n=0)'
   read(*,*)i
   if(i.eq.1)then
     print*,'Default parameter:'
     print*,'Camera lenght in mm l=',l
     print*,'Wave length in A lambda=',lambda
     print*,'Lattice parameters in A :'
     print*,'fcc martensite afcc=',afcc
     print*,'bcc Ti          abcc=',abcc
     print*,'hcp Ti          ahcp=',ahcp
     print*,'                chcp=',chcp
     print*,'orthorhombic aort=',aort
     print*,'                bort=',bort
     print*,'                cort=',cort
     print*,' '
     print*,'Do you want to change the parameters ? (y=1,n=0)'
     read(*,*)i
     if(i.eq.1)then
       print*,'l= ? mm'
       read(*,*)l
       print*,'lambda= ? A'
       read(*,*)lambda
       print*,'afcc= ? A'
```

```
    read(*,*)afcc
    print*,'abcc= ? A'
    read(*,*)abcc
    print*,'ahcp= ? A'
    read(*,*)ahcp
    print*,'chcp= ? A'
    read(*,*)chcp
    print*,'aort= ? A'
    read(*,*)aort
    print*,'bort= ? A'
    read(*,*)bort
    print*,'cort= ? A'
    read(*,*)cort
end if
print*,'Do you want to change the error limits ? (y=1,n=0)'
read(*,*)i
if(i.eq.1)then
    print*,'erlength= ? mm           [erl=',erl,']'
    read(*,*)erl
    print*,'erradius= ? %           [err=',err,']'
    read(*,*)err
    print*,'erangle = ? deg        [era=',era,']'
    read(*,*)era
end if
end if
c
c   Compute error limits
c
    l1=1-erl
    l2=1+erl
    r1=r-err*r/100
    r2=r+err*r/100
    t1=t-ert*t/100
    t2=t+ert*t/100
    alpha1=alpha-era
    alpha2=alpha+era
c
c   Change degrees into radians
c
    alpha=alpha*pi/180
    alpha1=alpha1*pi/180
    alpha2=alpha2*pi/180
c
c   Computation of d spacing
c
    da1=l1*lambda/r2
    da2=l2*lambda/r1
    db1=l1*lambda/t2
    db2=l2*lambda/t1
c
c   Write report file
c
    write(3,*)
    write(3,*)' Photo Nr. = ',nr
    write(3,*)' _____'
    write(3,*)
c
c   Find planes which match the input data
c
    call fccpln(fccind)
    call bccpln(bccind)
    call hcppln(hcpind)
```

```
call ortpln(ortind)
c
print*, 'New data to be computed ? (yes=1,no=0)'
read(*,*)k
if(k.eq.1)goto 5
c
stop
end
c
c
c Subroutine CUBSYM creates all symmetrically possible plane
c indices (hkl) for cubic crystal system.
c ifcc,ibcc - number of (hkl)-indices in fccind and bccind to
c be permuted
c dum - dummy array
c
subroutine cubsym(fcc,fccind,ifcc,nfcc,bcc,bccind,ibcc,nbcc)
integer h,k,l,m,n,o,i,ii,jj,j,nfcc,nbcc,ifcc,ibcc
integer*1 fcc(700,3),bcc(700,3),dum(700,3)
integer*1 fccind(3,19),bccind(3,28)
c
c
c nfcc=0
c
c Symmetry operations in cubic system:
c face-centred cubic
c do 10 i=1,ifcc
c h=fccind(1,j)
c k=fccind(2,j)
c l=fccind(3,j)
c call stor(h,k,l,nfcc,fcc)
c
c m=-h
c n=k
c o=-l
c call stor(m,n,o,nfcc,fcc)
c
c m=-h
c n=-k
c o=l
c call stor(m,n,o,nfcc,fcc)
c
c m=h
c n=-k
c o=-l
c call stor(m,n,o,nfcc,fcc)
c
c m=k
c n=l
c o=h
c call stor(m,n,o,nfcc,fcc)
c
c m=-k
c n=l
c o=-h
c call stor(m,n,o,nfcc,fcc)
c
c m=-k
c n=-l
c o=h
c call stor(m,n,o,nfcc,fcc)
c
```

```
m=k
n=-l
o=-h
call stor(m,n,o,nfcc,fcc)
c
m=l
n=h
o=k
call stor(m,n,o,nfcc,fcc)
c
m=-l
n=h
o=-k
call stor(m,n,o,nfcc,fcc)
c
m=-l
n=-h
o=k
call stor(m,n,o,nfcc,fcc)
c
m=l
n=-h
o=-k
call stor(m,n,o,nfcc,fcc)
c
m=-l
n=-k
o=-h
call stor(m,n,o,nfcc,fcc)
c
m=l
n=-k
o=h
call stor(m,n,o,nfcc,fcc)
c
m=l
n=k
o=-h
call stor(m,n,o,nfcc,fcc)
c
m=-l
n=k
o=h
call stor(m,n,o,nfcc,fcc)
c
m=-h
n=-l
o=-k
call stor(m,n,o,nfcc,fcc)
c
m=h
n=-l
o=k
call stor(m,n,o,nfcc,fcc)
c
m=h
n=l
o=-k
call stor(m,n,o,nfcc,fcc)
c
m=-h
n=l
```

```
o=k
call stor(m,n,o,nfcc,fcc)
c
m=-k
n=-h
o=-l
call stor(m,n,o,nfcc,fcc)
c
m=k
n=-h
o=l
call stor(m,n,o,nfcc,fcc)
c
m=k
n=h
o=-l
call stor(m,n,o,nfcc,fcc)
c
m=-k
n=h
o=l
call stor(m,n,o,nfcc,fcc)
c
10 continue
c
c
c Symmetry operations in cubic system:
c body-centred cubic
c
c nbcc=0
c
c do 20 i=1,28
c   h=bccind(1,j)
c   k=bccind(2,j)
c   l=bccind(3,j)
c   call stor(h,k,l,nbcc,bcc)
c
c   m=-h
c   n=k
c   o=-l
c   call stor(m,n,o,nbcc,bcc)
c
c   m=-h
c   n=-k
c   o=l
c   call stor(m,n,o,nbcc,bcc)
c
c   m=h
c   n=-k
c   o=-l
c   call stor(m,n,o,nbcc,bcc)
c
c   m=k
c   n=l
c   o=h
c   call stor(m,n,o,nbcc,bcc)
c
c   m=-k
c   n=l
c   o=-h
c   call stor(m,n,o,nbcc,bcc)
c
```

m=-k
n=-l
o=h
call stor(m,n,o,nbcc,bcc)

c

m=k
n=-l
o=-h
call stor(m,n,o,nbcc,bcc)

c

m=l
n=h
o=k
call stor(m,n,o,nbcc,bcc)

c

m=-l
n=h
o=-k
call stor(m,n,o,nbcc,bcc)

c

m=-l
n=-h
o=k
call stor(m,n,o,nbcc,bcc)

c

m=l
n=-h
o=-k
call stor(m,n,o,nbcc,bcc)

c

m=-l
n=-k
o=-h
call stor(m,n,o,nbcc,bcc)

c

m=l
n=-k
o=h
call stor(m,n,o,nbcc,bcc)

c

m=l
n=k
o=-h
call stor(m,n,o,nbcc,bcc)

c

m=-l
n=k
o=h
call stor(m,n,o,nbcc,bcc)

c

m=-h
n=-l
o=-k
call stor(m,n,o,nbcc,bcc)

c

m=h
n=-l
o=k
call stor(m,n,o,nbcc,bcc)

c

m=h
n=l

```
o=-k
call stor(m,n,o,nbcc,bcc)
c
m=-h
n=l
o=k
call stor(m,n,o,nbcc,bcc)
c
m=-k
n=-h
o=-l
call stor(m,n,o,nbcc,bcc)
c
m=k
n=-h
o=l
call stor(m,n,o,nbcc,bcc)
c
m=k
n=h
o=-l
call stor(m,n,o,nbcc,bcc)
c
m=-k
n=h
o=l
call stor(m,n,o,nbcc,bcc)
c
20 continue
c
Delete repeated indices for fcc
c
jj=0
do 30 ii=1,nfcc
  h=fcc(ii,1)
  k=fcc(ii,2)
  l=fcc(ii,3)
  if((h.eq.0).and.(k.eq.0).and.(l.eq.0))goto 30
  do 40 j=ii+1,nfcc
    m=fcc(j,1)
    n=fcc(j,2)
    o=fcc(j,3)
    if((m.eq.0).and.(n.eq.0).and.(o.eq.0))goto 40
    if((h.eq.m).and.(k.eq.n).and.(l.eq.o))then
      fcc(j,1)=0
      fcc(j,2)=0
      fcc(j,3)=0
    end if
  40 continue
  jj=jj+1
  dum(jj,1)=h
  dum(jj,2)=k
  dum(jj,3)=l
30 continue
c
do 50 i=1,jj
  fcc(i,1)=dum(i,1)
  fcc(i,2)=dum(i,2)
  fcc(i,3)=dum(i,2)
50 continue
c
```

```
c      Number of (hkl)-indices in fcc-array
c
c      nfcc=jj
c
c      Delete repeated indices for bcc
c
c      jj=0
c      do 70 ii=1,nbcc
c          h=bcc(ii,1)
c          k=bcc(ii,2)
c          l=bcc(ii,3)
c          if((h.eq.0).and.(k.eq.0).and.(l.eq.0))goto 70
c          do 80 j=ii+1,nbcc
c              m=bcc(j,1)
c              n=bcc(j,2)
c              o=bcc(j,3)
c              if((m.eq.0).and.(n.eq.0).and.(o.eq.0))goto 80
c              if((h.eq.m).and.(k.eq.n).and.(l.eq.o))then
c                  bcc(j,1)=0
c                  bcc(j,2)=0
c                  bcc(j,3)=0
c              end if
c          continue
80      jj=jj+1
c          dum(jj,1)=h
c          dum(jj,2)=k
c          dum(jj,3)=l
70      continue
c
c      do 90 i=1,jj
c          bcc(i,1)=dum(i,1)
c          bcc(i,2)=dum(i,2)
c          bcc(i,3)=dum(i,3)
90      continue
c
c      Number of (hkl)-indices in bcc-array
c
c      nbcc=jj
c
c      stop
c
c
c      Subroutine HEXSYM creates all symmetrically possible plane
c      indices(hkl) for hexagonal crystal system.
c      ihcp - number of (hkl)-indices in hcpind-array to be
c      permuted
c      dum - dummy array
c
c      subroutine hexsym(hcp,hcpind,ihcp,nhcp)
c          integer ii,j,jj,nhcp,ihcp,h,k,i,l,m,n,o
c          integer*1 hcp(500,3),dum(500,3),hcpind(3,25)
c
c      Symmetry operations in hexagonal system
c
c      do 10 j=1,ihcp
c          h=hcpind(1,j)
c          k=hcpind(2,j)
c          l=hcpind(3,j)
c          i=-(h+k)
c          call stor(h,k,l,nhcp,hcp)
c
```

```
m=-i
n=-h
o=l
call stor(m,n,o,nhcp,hcp)
c
m=k
n=i
call stor(m,n,o,nhcp,hcp)
c
m=-h
n=-k
call stor(m,n,o,nhcp,hcp)
c
m=i
n=h
call stor(m,n,o,nhcp,hcp)
c
m=-k
n=-i
call stor(m,n,o,nhcp,hcp)
c
o=-l
m=h
n=i
call stor(m,n,o,nhcp,hcp)
c
m=k
n=h
call stor(m,n,o,nhcp,hcp)
c
m=i
n=k
call stor(m,n,o,nhcp,hcp)
c
m=-i
n=-k
call stor(m,n,o,nhcp,hcp)
c
m=-h
n=-i
call stor(m,n,o,nhcp,hcp)
c
m=-k
n=-h
call stor(m,n,o,nhcp,hcp)
c
10 continue
c
c Delete repeated (hkl)-indices
c
jj=0
do 30 ii=1,nhcp
  h=hcp(ii,1)
  k=hcp(ii,2)
  l=hcp(ii,3)
  if((h.eq.0).and.(k.eq.0).and.(l.eq.0))goto 30
  do 40 j=ii+1,nhcp
    m=hcp(j,1)
    n=hcp(j,2)
    o=hcp(j,3)
    if((m.eq.0).and.(n.eq.0).and.(o.eq.0))goto 40
    if((h.eq.m).and.(k.eq.n).and.(l.eq.o))then
```

```

        hcp(j,1)=0
        hcp(j,2)=0
        hcp(j,3)=0
    end if
40    continue
        jj=jj+1
        dum(jj,1)=h
        dum(jj,2)=k
        dum(jj,3)=l
30    continue
c
    do 50 i=1,jj
        hcp(i,1)=dum(i,1)
        hcp(i,2)=dum(i,2)
        hcp(i,3)=dum(i,3)
50    continue
c
c    Number of (hkl)-indices in hcp-array
c
c    nhcp=jj
c
c    stop
c
c
c    Subroutine ORTSYM creates all symmetrically possible plane
c    indices (hkl) for orthorhombic crystal system.
c    ihcp - number of (hkl)-indices in ortind-array to be
c    permuted
c    dum - dummy array
c
c    subroutine ortsym(ort,ortind,iort,nort,aort,bort,cort)
c    integer ii,j,jj,nort,iort,h,k,l,m,n,o
c    integer*1 ort(700,3),dum(700,3),ortind(3,100)
c    real d1,d2,aort,bort,cort,a,b,c
c
c    Symmetry operations in orthorhombic system
c
c    do 10 j=1,iort
c    h=ortind(1,j)
c    k=ortind(2,j)
c    l=ortind(3,j)
c    call stor(h,k,l,nort,ort)
c
c    m=h
c    n=-k
c    o=-l
c    call stor(m,n,o,nort,ort)
c
c    m=-h
c    n=k
c    o=-l
c    call stor(m,n,o,nort,ort)
c
c    m=-h
c    n=-k
c    o=l
c    call stor(m,n,o,nort,ort)
c
10    continue
c
c    Sorting of (hkl) according to the value of the spacing of
```

```
c   the planes d
c
    a=aort*aort
    b=bort*bort
    c=cort*cort
c
    do 25 ii=1,nort
d1=(ort(ii,1)**2)/a+(ort(ii,2)**2)/b+(ort(ii,3)**2)/c
    if(d1.lt.0.001)goto 25
    do 26 jj=ii,nort
d2=(ort(jj,1)**2)/a+(ort(jj,2)**2)/b+(ort(jj,3)**2)/c
    if(d2.lt.0.0001)goto 26
    if(d1.gt.d2)then
        h=ort(ii,1)
        k=ort(ii,2)
        l=ort(ii,3)
        ort(ii,1)=ort(jj,1)
        ort(ii,2)=ort(jj,2)
        ort(ii,3)=ort(jj,3)
        ort(jj,1)=h
        ort(jj,2)=k
        ort(jj,3)=l
        d1=d2
    end if
26    continue
25    continue
c
Delete repeated (hkl)-indices from ort-array
c
    jj=0
    do 30 ii=1,nort
        h=ort(ii,1)
        k=ort(ii,2)
        l=ort(ii,3)
        if((h.eq.0).and.(k.eq.0).and.(l.eq.0))goto 30
        do 40 j=ii+1,nort
            m=ort(j,1)
            n=ort(j,2)
            o=ort(j,3)
            if((m.eq.0).and.(n.eq.0).and.(o.eq.0))goto 40
            if((h.eq.m).and.(k.eq.n).and.(l.eq.o))then
                ort(j,1)=0
                ort(j,2)=0
                ort(j,3)=0
            end if
40        continue
            jj=jj+1
            dum(jj,1)=h
            dum(jj,2)=k
            dum(jj,3)=l
30    continue
c
    do 50 i=1,jj
        ort(i,1)=dum(i,1)
        ort(i,2)=dum(i,2)
        ort(i,3)=dum(i,2)
50    continue
c
Number of (hkl)-indices in ort-array
c
    nort=jj
c
```

```

      stop
c
c
c
c      Subroutine STOR writes the (hkl)-indices into an
c      appropriate array (fcc,bcc,hcp or ort).
c      STOR is called from CUBSYM, HEXSYM and ORTSYM
c      npl - number of the planes
c      array - name of the array
c
c      subroutine stor(h,k,l,npl,array)
c      integer h,k,l,npl
c      integer*1 array(700,3)
c
c      npl=npl+1
c      array(npl,1)=h
c      array(npl,2)=k
c      array(npl,3)=l
c
c      return
c      end
c
c
c      Subroutine FCCPLN finds if any of the (hkl)-indices match
c      the input data and then calculates all planes belonging to
c      the same zone. If a match is found, the (hkl)-indices of
c      the planes are written to the output file DRAWDAT.
c
c      The format of the data in DRAWDAT is as follows:
c      Integer number 1 indicates the fcc system
c      nr - identification number of the diffraction pattern
c      l,lambda,abcc - camera length, wave length and unit vector
c      nout - number of following integer triplets
c      first triplet u,v,w - zone axis
c      next triplets h,k,l - plane indices
c
c      subroutine fccpln(fccind)
c      integer i,ii,j,jj,h1,k1,l1,h2,k2,l2,h3,k3,l3,nplna,nplnb
c      integer zeiga(19),zeigb(19),nfcc,nbcc,nhcp,nort,nr
c      integer*1 fccind(3,19)
c      integer*1 fcc(700,3),bcc(700,3),hcp(700,3),ort(700,3)
c      integer out(200,3),nout
c      real d,da,db,cosab,u,v,w,u1,v1,w1
c      real afcc,abcc,ahcp,ahcp,aort,bort,cort,l,lambda
c      real alpha,alpha1,alpha2
c      real da1,da2,db1,db2
c      common /dat1/ fcc,bcc,hcp,ort,afcc,abcc,ahcp,ahcp,alpha1,
c      *alpha2,da1,da2,db1,db2,alpha,nfcc,nbcc,nhcp,l,lambda,nr,
c      *nort,aort,bort,cort
c
c      Zeroise pointer arrays
c
c      do 5 i=1,19
c          zeiga(i)=0
c          zeigb(i)=0
c      5 continue
c
c      Find matching planes
c
c      nplna=0
c      nplnb=0
c      do 10 i=1,19
```

```
h1=fccind(1,i)
k1=fccind(2,i)
l1=fccind(3,i)
d=(afcc**2)/(h1*h1+k1*k1+l1*l1)
d=sqrt(d)
if((d.ge.da1).and.(d.le.da2))then
  nplna=nplna+1
  zeiga(nplna)=i
  print*, 'OK for A !      d=',d
  write(3,*) 'OK for A !      d=',d
end if
if((d.ge.db1).and.(d.le.db2))then
  nplnb=nplnb+1
  zeigb(nplnb)=i
  print*, 'OK for B !      d=',d
  write(3,*) 'OK for B !      d=',d
end if
10 continue
c
c Write report file
c
if((nplna.eq.0).or.(nplnb.eq.0))then
  print*, '*****'
  print*, ' No planes found for fcc '
  print*, '*****'
  write(3,*) '*****'
  write(3,*) ' No planes found for fcc '
  write(3,*) '*****'
  return
end if
c
c Compute plane angles
c
do 20 i=1,nplna
  h1=fccind(1,zeiga(i))
  k1=fccind(2,zeiga(i))
  l1=fccind(3,zeiga(i))
  da=h1**2+k1**2+l1**2
  da=sqrt(da)
  do 30 ii=1,nplnb
    h2=fccind(1,zeigb(ii))
    k2=fccind(2,zeigb(ii))
    l2=fccind(3,zeigb(ii))
    db=h2**2+k2**2+l2**2
    db=sqrt(db)
    u1=0
    v1=0
    w1=0
    nout=0
    do 40 j=1,nfcc
      h2=fcc(j,1)
      k2=fcc(j,2)
      l2=fcc(j,3)
      if((h2.eq.0).and.(k2.eq.0).and.(l2.eq.0))goto 40
      d=h2**2+k2**2+l2**2
      d=sqrt(d)
      if((db.ge.(d-.01)).and.(db.le.(d+.01)))then
        cosab=(h1*h2+k1*k2+l1*l2)/(da*db)
        if(cosab.ge.1)then
          cosab=.999999
        end if
        if(cosab.le.-1)then
```

```
        cosab=-.999999
        end if
        cosab=acos(cosab)
        if((cosab.ge.alpha1).and.(cosab.le.alpha2))then
c
c      Find the zone axis
c
          u=k1*l2-l1*k2
          v=l1*h2-h1*l2
          w=h1*k2-k1*h2
          if((u*u+v*v+w*w).le.0.01)goto 40
          if((abs((u1**2+v1**2+w1**2)-(u*u+v*v+w*w))).ge.0.01)then
c
c      Write report file
c
          print*,'****'
          print*,'Found fcc:'
          print*,'Zone axis:      [' ,u,v,w,']'
          print*,'1st vector:    (' ,h1,k1,l1,')'
          print*,'2nd vector:    (' ,h2,k2,l2,')'
          write(3,*)'****'
          write(3,*)'Found fcc:'
          write(3,*)'Zone axis:      [' ,u,v,w,']'
          write(3,*)'1st vector:    (' ,h1,k1,l1,')'
          write(3,*)'2nd vector:    (' ,h2,k2,l2,')'
c
          nout=nout+1
          out(nout,1)=ifix(u)
          out(nout,2)=ifix(v)
          out(nout,3)=ifix(w)
          nout=nout+1
          out(nout,1)=h1
          out(nout,2)=k1
          out(nout,3)=l1
          nout=nout+1
          out(nout,1)=h2
          out(nout,2)=k2
          out(nout,3)=l2
c
c      Find planes belonging to the zone [u,v,w]
c
          do 50 jj=1,nfcc
            h3=fcc(jj,1)
            k3=fcc(jj,2)
            l3=fcc(jj,3)
            if((h3*h3+k3*k3+l3*l3).gt..01)then
              if((abs(h3*u+k3*v+l3*w)).le.0.01)then
                print*,'Next vector: (' ,h3,k3,l3,')'
                write(3,*)'Next vector: (' ,h3,k3,l3,')'
c
                nout=nout+1
                out(nout,1)=h3
                out(nout,2)=k3
                out(nout,3)=l3
c
                end if
              end if
            continue
50
c      Write output to the DRAWDAT file
c
          write(4,*)1
```

```

        write(4,*)nr
        write(4,*)l,lambda,afcc
        write(4,*)nout
        do 55 jj=1,nout
            write(4,*)(out(jj,jjj),jjj=1,3)
55      continue
        nout=0
c
        end if
        u1=u
        v1=v
        w1=w
        end if
        end if
40      continue
30      continue
20      continue
c
        return
        end
c
c
c      Subroutine BCCPLN finds if any of the (hkl)-indices match
c      the input data and then calculates all planes belonging to
c      the same zone.  If a match is found, the (hkl)-indices of
c      the planes are written to the output file DRAWDAT.
c
c      The format of the data in DRAWDAT is as follows:
c      Integer number 2 indicates the bcc system
c      nr - identification number of the diffraction pattern
c      l,lambda,abcc - camera length, wave length and unit vector
c      nout - number of following integer triplets
c      first triplet u,v,w - zone axis
c      next triplets h,k,l - plane indices
c
c      subroutine bccpln(bccind)
c      integer i,ii,j,jj,h1,k1,l1,h2,k2,l2,h3,k3,l3,nplna,nplnb
c      integer zeiga(28),zeigb(28),nfcc,nbcc,nhcp,nort
c      integer*1 bccind(3,28)
c      integer out(200,3),nout,nr
c      integer*1 fcc(700,3),bcc(700,3),hcp(700,3),ort(700,3)
c      real d,da,db,cosab,u,v,w,u1,v1,w1
c      real afcc,abcc,ahcp,chcp,aort,bort,cort,l,lambda
c      real alpha,alpha1,alpha2
c      real da1,da2,db1,db2
c      common /dat1/ fcc,bcc,hcp,ort,afcc,abcc,ahcp,chcp,alpha1,
c      *alpha2,da1,da2,db1,db2,alpha,nfcc,nbcc,nhcp,l,lambda,nr
c      *nort,aort,bort,cort
c
c      Zeroise pointer arrays
c
c      do 5 i=1,28
c          zeiga(i)=0
c          zeigb(i)=0
5      continue
c
c      Find matching planes
c
c      nplna=0
c      nplnb=0
c      do 10 i=1,28
c          h1=bccind(1,i)
```

```
k1=bccind(2,i)
l1=bccind(3,i)
d=(abcc**2)/(h1*h1+k1*k1+l1*l1)
d=sqrt(d)
if((d.ge.da1).and.(d.le.da2))then
  nplna=nplna+1
  zeiga(nplna)=i
  print*, 'OK for A !      d=',d
  write(3,*) 'OK for A !      d=',d
end if
if((d.ge.db1).and.(d.le.db2))then
  nplnb=nplnb+1
  zeigb(nplnb)=i
  print*, 'OK for B !      d=',d
  write(3,*) 'OK for B !      d=',d
end if
10 continue
c
c Write report file
c
if((nplna.eq.0).or.(nplnb.eq.0))then
  print*, '*****'
  print*, ' No planes found for bcc '
  print*, '*****'
  write(3,*) '*****'
  write(3,*) ' No planes found for bcc '
  write(3,*) '*****'
  return
end if
c
c Compute plane angles
c
do 20 i=1,nplna
  h1=bccind(1,zeiga(i))
  k1=bccind(2,zeiga(i))
  l1=bccind(3,zeiga(i))
  da=h1**2+k1**2+l1**2
  da=sqrt(da)
  do 30 ii=1,nplnb
    h2=bccind(1,zeigb(ii))
    k2=bccind(2,zeigb(ii))
    l2=bccind(3,zeigb(ii))
    db=h2**2+k2**2+l2**2
    db=sqrt(db)
    u1=0
    v1=0
    w1=0
    nout=0
    do 40 j=1,nbcc
      h2=bcc(j,1)
      k2=bcc(j,2)
      l2=bcc(j,3)
      if((h2.eq.0).and.(k2.eq.0).and.(l2.eq.0))goto 40
      d=h2**2+k2**2+l2**2
      d=sqrt(d)
      if((db.ge.(d-.01)).and.(db.le.(d+.01)))then
        cosab=(h1*h2+k1*k2+l1*l2)/(da*db)
        cosab=acos(cosab)
        if((cosab.ge.alpha1).and.(cosab.le.alpha2))then
c
c Find the zone axis
c
```

```
u=k1*l2-l1*k2
v=l1*h2-h1*l2
w=h1*k2-k1*h2
c
c
      if((u*u+v*v+w*w).le.0.01)goto 40
      if((abs((u1**2+v1**2+w1**2)-(u*u+v*v+w*w))).gt.0.01)then
c
c
Write report file
c
      print*,'****'
      print*,'Found bcc:'
      print*,'Zone axis:  [' ,u,v,w,']'
      print*,'1st vector: (' ,h1,k1,l1,')'
      print*,'2nd vector: (' ,h2,k2,l2,')'
      write(3,*)'****'
      write(3,*)'Found bcc:'
      write(3,*)'Zone axis:  [' ,u,v,w,']'
      write(3,*)'1st vector: (' ,h1,k1,l1,')'
      write(3,*)'2nd vector: (' ,h2,k2,l2,')'
c
c
      nout=nout+1
      out(nout,1)=ifix(u)
      out(nout,2)=ifix(v)
      out(nout,3)=ifix(w)
      nout=nout+1
      out(nout,1)=h1
      out(nout,2)=k1
      out(nout,3)=l1
      nout=nout+1
      out(nout,1)=h2
      out(nout,2)=k2
      out(nout,3)=l2
c
c
Find planes belonging to the zone [u,v,w]
c
      do 50 jj=1,nbcc
      h3=bcc(jj,1)
      k3=bcc(jj,2)
      l3=bcc(jj,3)
      if((h3*h3+k3*k3+l3*l3).gt..01)then
      if((abs(h3*u+k3*v+l3*w)).le.0.01)then
      print*,'Next vector: (' ,h3,k3,l3,')'
      write(3,*)'Next vector: (' ,h3,k3,l3,')'
c
      nout=nout+1
      out(nout,1)=h3
      out(nout,2)=k3
      out(nout,3)=l3
      end if
      end if
c
50      continue
c
Write DRAWDAT
c
      write(4,*)2
      write(4,*)nr
      write(4,*)l,lambd,abcc
      write(4,*)nout
      do 55 jj=1,nout
```



```
k1=hcpind(2,i)
i1=hcpind(3,i)
l1=hcpind(4,i)
d=(3*ahcp**2/2)/(h1*h1+k1*k1+i1*i1+l1*l1*(1/qphi))
d=sqrt(d)
if((d.ge.da1).and.(d.le.da2))then
  nplna=nplna+1
  zeiga(nplna)=i
  print*,'OK for A !      d=',d
  write(3,*)'OK for A !      d=',d
end if
if((d.ge.db1).and.(d.le.db2))then
  nplnb=nplnb+1
  zeigb(nplnb)=i
  print*,'OK for B !      d=',d
  write(3,*)'OK for B !      d=',d
end if
10 continue
c
c Write report file
c
if((nplna.eq.0).or.(nplnb.eq.0))then
  print*,'*****'
  print*,' No planes found for hcp '
  print*,'*****'
  write(3,*)'*****'
  write(3,*)' No planes found for hcp '
  write(3,*)'*****'
  return
end if
c
c Compute plane angles
c
do 20 i=1,nplna
  h1=hcpind(1,zeiga(i))
  k1=hcpind(2,zeiga(i))
  i1=hcpind(3,zeiga(i))
  l1=hcpind(4,zeiga(i))
  da=h1**2+k1**2+i1**2+(1/qphi)*l1**2
  da=sqrt(da)
  do 30 ii=1,nplnb
    h2=hcpind(1,zeigb(ii))
    k2=hcpind(2,zeigb(ii))
    i2=hcpind(3,zeigb(ii))
    l2=hcpind(4,zeigb(ii))
    db=h2**2+k2**2+i2**2+(1/qphi)*l2**2
    db=sqrt(db)
    u1=0
    v1=0
    t1=0
    w1=0
    nout=0
    do 40 j=1,nhcp
      h2=hcp(j,1)
      k2=hcp(j,2)
      i2=-(h2+k2)
      l2=hcp(j,3)
      if((h2.eq.0).and.(k2.eq.0).and.(l2.eq.0))goto 40
      d=h2**2+k2**2+i2**2+(1/qphi)*l2**2
      d=sqrt(d)
      if((db.ge.(d-.01)).and.(db.le.(d+.01)))then
        cosab=(h1*h2+k1*k2+i1*i2+(1/qphi)*l1*l2)/(da*db)
```

```
if(cosab.ge.1)then
  cosab=.999999
end if
if(cosab.le.-1)then
  cosab=-.999999
end if
cosab=acos(cosab)
if((cosab.ge.alpha1).and.(cosab.le.alpha2))then
c
c
c
  Find the zone axis

  u=12*(2*k1+h1)-11*(2*k2+h2)
  v=11*(2*h2+k2)-12*(2*h1+k1)
  w=3*(h1*k2-h2*k1)
  t=-(u+v)
  if((u*u+v*v+w*w).le.0.01)goto 40
if((abs((u1**2+v1**2+t1**2+w1**2)-(u*u+v*v+t*t+w*w))).gt.
*.01)then
c
c
c
  Write report file

  print*,'****'
  print*,'Found hcp:'
  print*,'Zone axis:  [' ,u,v,t,w,']'
  print*,'1st vector: (' ,h1,k1,i1,l1,')'
  print*,'2nd vector: (' ,h2,k2,i2,l2,')'
  write(3,*)'****'
  write(3,*)'Found hcp:'
  write(3,*)'Zone axis:  [' ,u,v,t,w,']'
  write(3,*)'1st vector: (' ,h1,k1,i1,l1,')'
  write(3,*)'2nd vector: (' ,h2,k2,i2,l2,')'
c
c
c
  nout=nout+1
  out(nout,1)=ifix(u)
  out(nout,2)=ifix(v)
  out(nout,3)=ifix(w)
  nout=nout+1
  out(nout,1)=h1
  out(nout,2)=k1
  out(nout,3)=l1
  nout=nout+1
  out(nout,1)=h2
  out(nout,2)=k2
  out(nout,3)=l2
c
c
c
  Find planes belonging to the zone [u,v,t,w]

  do 50 jj=1,nhcp
    h3=hcp(jj,1)
    k3=hcp(jj,2)
    i3=-(h3+k3)
    l3=hcp(jj,3)
    if((h3*h3+k3*k3+l3*l3).gt..01)then
      if((abs(h3*u+k3*v+i3*t+l3*w)).le.0.01)then
c
c
c
  Write report file

    write(3,*)'Next vector: (' ,h3,k3,i3,l3,')'
    print*,'Next vector: (' ,h3,k3,i3,l3,')'
c
c
  nout=nout+1
```

```

        out(nout,1)=h3
        out(nout,2)=k3
        out(nout,3)=l3
c
        end if
        end if
50      continue
c
c      Write DRAWDAT
c
        write(4,*)3
        write(4,*)nr
        write(4,*)l,lambda,ahcp,chcp
        write(4,*)nout
        do 55 jj=1,nout
          write(4,*)(out(jj,jjj),jjj=1,3)
55      continue
        nout=0
c
        end if
        u1=u
        v1=v
        t1=t
        w1=w
        end if
        end if
40      continue
30      continue
20      continue
c
      return
      end
c
c
c      Subroutine ORTPLN finds if any of the (hkl)-indices match
c      the input data and then calculates all planes belonging to
c      the same zone. If a match is found, the (hkl)-indices of
c      the planes are written to the output file DRAWDAT.
c
c      The format of the data in DRAWDAT is as follows:
c      Integer number 4 indicates the ort system
c      nr - identification number of the diffraction pattern
c      l,lambda,aort,bort,cort - camera length, wave length and
c      unit vectors
c      nout - number of following integer triplets
c      first triplet u,v,w - zone axis
c      next triplets h,k,l - plane indices
c
      subroutine ortpln(ortind)
      integer i,ii,j,jj,h1,k1,l1,h2,k2,l2,h3,k3,l3,nplna,nplnb
      integer zeiga(100),zeigb(100),nfcc,nbcc,nhcp,nort,nr
      integer*1 ortind(3,100)
      integer*1 fcc(700,3),bcc(700,3),hcp(700,3),ort(700,3)
      integer out(200,3),nout
      real d,da,db,cosab,u,v,w,u1,v1,w1
      real afcc,abcc,ahcp,chcp,aort,bort,cort,l,lambda
      real alpha,alpha1,alpha2
      real da1,da2,db1,db2
      common /dat1/ fcc,bcc,hcp,ort,afcc,abcc,ahcp,chcp,alpha1,
      *alpha2,da1,da2,db1,db2,alpha,nfcc,nbcc,nhcp,l,lambda,nr,
      *nort,aort,bort,cort
c
```

```
c Zeroise pointer arrays
c
do 5 i=1,100
  zeiga(i)=0
  zeigb(i)=0
5 continue
c
c Find matching planes
c
nplna=0
nplnb=0
do 10 i=1,100
  h1=ortind(1,i)
  k1=ortind(2,i)
  l1=ortind(3,i)
c   print*, 'Checking ort hkl',h1,k1,l1
c   write(3,*) 'Checking ort hkl',h1,k1,l1
  d=(aort*aort*bort*bort*cort*cort)/(h1*h1*bort*bort*cort*
*cort+k1*k1*cort*cort*aort*aort+l1*l1*aort*aort*bort*bort)
  d=sqrt(d)
  if((d.ge.da1).and.(d.le.da2))then
    nplna=nplna+1
    zeiga(nplna)=i
    print*, 'OK for A !      d=',d
    write(3,*) 'OK for A !      d=',d
  end if
  if((d.ge.db1).and.(d.le.db2))then
    nplnb=nplnb+1
    zeigb(nplnb)=i
    print*, 'OK for B !      d=',d
    write(3,*) 'OK for B !      d=',d
  end if
10 continue
c
c Write report file
c
if((nplna.eq.0).or.(nplnb.eq.0))then
  print*, '*****'
  print*, ' No planes found for ort '
  print*, '*****'
  write(3,*) '*****'
  write(3,*) ' No planes found for ort '
  write(3,*) '*****'
  return
end if
c
c Compute plane angles
c
do 20 i=1,nplna
  h1=ortind(1,zeiga(i))
  k1=ortind(2,zeiga(i))
  l1=ortind(3,zeiga(i))
  da=(aort*aort*bort*bort*cort*cort)/(h1*h1*bort*bort*cort*
*cort+k1*k1*cort*cort*aort*aort+l1*l1*aort*aort*bort*bort)
  da=sqrt(da)
  do 30 ii=1,nplnb
    h2=ortind(1,zeigb(ii))
    k2=ortind(2,zeigb(ii))
    l2=ortind(3,zeigb(ii))
    db=(aort*aort*bort*bort*cort*cort)/(h2*h2*bort*bort*cort*
*cort+k2*k2*cort*cort*aort*aort+l2*l2*aort*aort*bort*bort)
    db=sqrt(db)
```

```
u1=0
v1=0
w1=0
nout=0
do 40 j=1,nort
  h2=ort(j,1)
  k2=ort(j,2)
  l2=ort(j,3)
  if((h2.eq.0).and.(k2.eq.0).and.(l2.eq.0))goto 40
  d=(aort*aort*bort*bort*cort*cort)/(h2*h2*bort*bort*cort*
*cort+k2*k2*cort*cort*aort*aort+l2*l2*aort*aort*bort*bort)
  d=sqrt(d)
  if((db.ge.(d-.001)).and.(db.le.(d+.001)))then
    cosab=(h1*h2/aort/aort+k1*k2/bort/bort+l1*l2/cort/cort)*
*(da*db)
    if(cosab.ge.1)then
      cosab=.999999
    end if
    if(cosab.le.-1)then
      cosab=-.999999
    end if
    cosab=acos(cosab)
    if((cosab.ge.alpha1).and.(cosab.le.alpha2))then
c
c      Find the zone axis
c
      u=k1*l2-l1*k2
      v=l1*h2-h1*l2
      w=h1*k2-k1*h2
      if((u*u+v*v+w*w).le.0.01)goto 40
      if((abs((u1**2+v1**2+w1**2)-(u*u+v*v+w*w))).ge.0.01)then
c
c      Write report file
c
      print*,'****'
      print*,'Found ort:'
      print*,'Zone axis:  [' ,u,v,w,']'
      print*,'1st vector: (' ,h1,k1,l1,')'
      print*,'2nd vector: (' ,h2,k2,l2,')'
      write(3,*)'****'
      write(3,*)'Found ort:'
      write(3,*)'Zone axis:  [' ,u,v,w,']'
      write(3,*)'1st vector: (' ,h1,k1,l1,')'
      write(3,*)'2nd vector: (' ,h2,k2,l2,')'
c
      nout=nout+1
      out(nout,1)=ifix(u)
      out(nout,2)=ifix(v)
      out(nout,3)=ifix(w)
      nout=nout+1
      out(nout,1)=h1
      out(nout,2)=k1
      out(nout,3)=l1
      nout=nout+1
      out(nout,1)=h2
      out(nout,2)=k2
      out(nout,3)=l2
c
c      Find planes belonging to the zone [u,v,w]
c
      do 50 jj=1,nort
        h3=ort(jj,1)
```

```

      k3=ort(jj,2)
      l3=ort(jj,3)
      if((h3*h3+k3*k3+l3*l3).gt..01)then
        if((abs(h3*u+k3*v+l3*w)).le.0.01)then
          print*, 'Next vector: (' ,h3,k3,l3,')'
          write(3,*) 'Next vector: (' ,h3,k3,l3,')'
c
          nout=nout+1
          out(nout,1)=h3
          out(nout,2)=k3
          out(nout,3)=l3
c
          end if
          end if
50      continue
c
c      Write DRAWDAT
c
          write(4,*)4
          write(4,*)nr
          write(4,*)1,lambda,aort,bort,cort
          write(4,*)nout
          do 55 jj=1,nout
            write(4,*)(out(jj,jjj),jjj=1,3)
55      continue
          nout=0
c
          end if
          u1=u
          v1=v
          w1=w
          end if
          end if
40      continue
30      continue
20      continue
c
      return
      end
c
```

Program DRAW

C The program DRAW uses the file DRAWDAT created by the program
C DIFFRA and draws a diffraction pattern on a computer screen. This
C program is software and hardware dependent as it will run only on
C ATARI 1040ST computer under FORTRAN77.

C PROGRAM DRAW

C INTEGER AESRET, HANDLE, WKXYWH, DESKX, DESKY, DESKW, DESKH
C INTEGER WX, WY, WW, WH, DESKHA, MYWIND, WFNAME, NAMEP

C Clip rectangle:
C INTEGER*2 CLIPR(0:3)

C Variables for calculating pattern points:
C REAL A, B, XSCALE, YSCALE

C VDI parameter arrays:
C INTEGER*2 POINTS(0:256), WORKIN(0:10), WORKOU(0:56)

C Variables for computation
C INTEGER OUT(200,3), NOUT, NR, TYPE, I, HKL1(3), HKL2(3), UVW(3)
C REAL L, LAMBDA, ADIR, BDIR, CDIR, D11, D22, RPHI(200,2)

C Scale factors
C XSCALE=.321875
C YSCALE=.3075

C Read data from DROWDAT
C OPEN(4, FILE='B:DRAWDAT', STATUS='OLD')
13 READ(4, *, END=11) TYPE
C READ(4, *, END=11) NR

C Type of the crystal system:
C 1=fcc, 2=bcc, 3=hcp, 4=ort

C IF (TYPE.EQ.3) THEN
C READ(4, *, END=11) L, LAMBDA, ADIR, CDIR
C END IF
C IF (TYPE.EQ.4) THEN
C READ(4, *, END=11) L, LAMBDA, ADIR, BDIR, CDIR
C END IF
C IF ((TYPE.EQ.1).OR.(TYPE.EQ.2)) THEN
C READ(4, *, END=11) L, LAMBDA, ADIR
C END IF

C Read zone axis [u,v,w]
C
C READ(4, *, END=11) NOUT
C READ(4, *, END=11) (UVW(I), I=1,3)

C Read plane indices (h,k,l)

C DO 10 I=1, NOUT-1
C READ(4, *, END=11) (OUT(I, J), J=1,3)
10 CONTINUE

C GOTO 14
11 PRINT*, 'END OF FILE REACHED!'

C

```
C      Computation of the R and PHI coordinates
C
14     DO 20 I=1,3
        HKL1(I)=OUT(1,I)
20     CONTINUE
C
C      Hexagonal system
C
        IF (TYPE.EQ.3) THEN
C
            CDIR=(CDIR/ADIR)**2
            CDIR=(CDIR*2)/3
            D1=HKL1(1)**2+HKL1(2)**2+(HKL1(1)+HKL1(2))**2+
+ (1/CDIR)*HKL1(3)**2
            D11=D1*2/3/ADIR**2
            D11=SQRT(D11)
            D1=SQRT(D1)
            RPHI(1,1)=L*LAMBDA*D11
            RPHI(1,2)=0
C
            DO 30 I=2,NOUT-1
                DO 40 J=1,3
                    HKL2(J)=OUT(I,J)
40         CONTINUE
C
                D2=HKL2(1)**2+HKL2(2)**2+(HKL2(1)+HKL2(2))**2+
+ (1/CDIR)*HKL2(3)**2
                D22=D2*2/3/ADIR**2
                D22=SQRT(D22)
                D2=SQRT(D2)
C
                RPHI(I,1)=L*LAMBDA*D22
                RPHI(I,2)=(HKL1(1)*HKL2(1)+HKL1(2)*HKL2(2)+HKL1(3)*
+ HKL2(3)*(1/CDIR)+(HKL1(1)+HKL1(2))*(HKL2(1)+HKL2(2)))/D1/D2
                IF (RPHI(I,2).GE.1.0) THEN
                    RPHI(I,2)=.999999
                END IF
                IF (RPHI(I,2).LE.-1.0) THEN
                    RPHI(I,2)=-.999999
                END IF
                RPHI(I,2)=ACOS(RPHI(I,2))
30         CONTINUE
            END IF
C
C      Cubic system
C
        IF ((TYPE.EQ.1).OR.(TYPE.EQ.2)) THEN
C
            D1=HKL1(1)**2+HKL1(2)**2+HKL1(3)**2
            D11=D1/ADIR**2
            D11=SQRT(D11)
            D1=SQRT(D1)
            RPHI(1,1)=L*LAMBDA*D11
            RPHI(1,2)=0
C
            DO 50 I=2,NOUT-1
                DO 60 J=1,3
                    HKL2(J)=OUT(I,J)
60         CONTINUE
C
                D2=HKL2(1)**2+HKL2(2)**2+HKL2(3)**2
                D22=D2/ADIR**2
```

```
D22=SQRT(D22)
D2=SQRT(D2)
C
RPHI(I,1)=L*LAMBDA*D22
RPHI(I,2)=(HKL1(1)*HKL2(1)+HKL1(2)*HKL2(2)+HKL1(3)*
+HKL2(3))/D1/D2
IF(RPHI(I,2).GE.1.0)THEN
RPHI(I,2)=0.999999
END IF
IF(RPHI(I,2).LE.-1.0)THEN
RPHI(I,2)=-.999999
END IF
RPHI(I,2)=ACOS(RPHI(I,2))
50 CONTINUE
END IF
C
C Orthorhombic system
C
IF(TYPE.EQ.4)THEN
C
D1=(HKL1(1)**2)/ADIR/ADIR+(HKL1(2)**2)/BDIR/BDIR+
*(HKL1(3)**2)/CDIR/CDIR
D11=D1
D11=SQRT(D11)
D1=SQRT(D1)
RPHI(1,1)=L*LAMBDA*D11
RPHI(1,2)=0
C
DO 90 I=2,NOUT-1
DO 100 J=1,3
HKL2(J)=OUT(I,J)
100 CONTINUE
C
D2=(HKL2(1)**2)/ADIR/ADIR+(HKL2(3)**2)/CDIR/CDIR+
*(HKL2(2)**2)/BDIR/BDIR
D22=D2
D22=SQRT(D22)
D2=SQRT(D2)
C
RPHI(I,1)=L*LAMBDA*D22
RPHI(I,2)=(HKL1(1)*HKL2(1)/ADIR/ADIR+HKL1(3)*
+HKL2(3)/CDIR/CDIR+HKL1(2)*HKL2(2)/BDIR/BDIR)/(D1*D2)
IF(RPHI(I,2).GE.1.0)THEN
RPHI(I,2)=.999999
END IF
IF(RPHI(I,2).LE.-1.0)THEN
RPHI(I,2)=-.999999
END IF
RPHI(I,2)=ACOS(RPHI(I,2))
90 CONTINUE
END IF
C
C Calculate X,Y-coordinates
C
DO 70 I=0,256
POINTS(I)=0
70 CONTINUE
IF(NOUT.GT.62)THEN
NOUT=62
END IF
J=1
DO 80 I=1,NOUT-1
```

```
POINTS(I+J)=NINT((RPHI(I,1)/XSCALE)*COS(RPHI(I,2)))
POINTS(I+1+J)=NINT((RPHI(I,1)*SIN(RPHI(I,2))/YSCALE))
C
C Second set of coordinates because of centre of symmetry
C
POINTS(I+2+J)=-POINTS(I+J)
POINTS(I+3+J)=-POINTS(I+1+J)
J=J+3
80 CONTINUE
C
C Write data on screen
C
PRINT*, 'TYPE=', TYPE
PRINT*, 'PHOTO NR.=', NR
PRINT*, 'ZONE : '
WRITE(*,21) (UVW(I), I=1,3)
21 FORMAT(3I3)
PRINT*, '1ST HKL : '
WRITE(*,22) (HKL1(I), I=1,3)
22 FORMAT(3I3)
C
C Initiate graphics application
CALL APPLIN
C
C Open virtual workstation
HANDLE=0
DO 1 I=0,9
WORKIN(I)=1
1 CONTINUE
WORKIN(7) = 0
WORKIN(10) = 2
WORKIN(3)=3
CALL VOPNVW(WORKIN, HANDLE, WORKOU)
C
C Determine desktop window work area size
WKXYWH = 4
DESKHA = 0
CALL WINDGE(DESKHA, WKXYWH, DESKX, DESKY, DESKW, DESKH)
C
C Determine my window work area size
WW = DESKW/2
WH = DESKH
WX = DESKX+WW
WY = DESKY
C
C Create window half size
CALL WINDCR(1, WX, WY, WW, WH)
MYWIND = AESRET()
C
C Open the window
CALL WINDOP(MYWIND, WX, WY, WW, WH)
C
C Set clip rectangle to work area of window
CALL WINDGE(MYWIND, WKXYWH, WX, WY, WW, WH)
CLIPR(0) = WX
CLIPR(1) = WY
CLIPR(2) = WX+WW
CLIPR(3) = WY+WH
CALL VSCLIP(HANDLE, 1, CLIPR)
C
C Hide mouse while drawing
CALL GRAFMO(256, 0)
```

```
C
C   Fill rectangle with background (white)
CALL VRRECT(HANDLE, CLIPR)

C
C   Calculate coordinates
A=WX+WW/2
B=WY+WH/2
DO 5 I=0,254,2
POINTN(I)=POINTN(I)+A
5 POINTN(I+1)=POINTN(I+1)+B

C
C   Draw the pattern
CALL VPMARK(HANDLE, 127, POINTN)

C
C   Wait until keyboard
CALL EVNTKE

C
C   Show mouse after update
CALL GRAFMO(0,0)
CALL GRAFMO(257,0)

C
C   Close and delete window
CALL WINDCL(MYWIND)
CALL WINDDE(MYWIND)
CALL VCLRWK(HANDLE)
CALL VCLSVW(HANDLE)

C
C   Application exit
CALL APPLEX

C
PRINT*, 'NEW PATTERN ?           (Y=1,N=0) '
READ(*,*)I
IF(I.EQ.1)GOTO 13

C
STOP
END
```

